

**Name of the Examination: B. PHARMACY THIRD YEAR SECOND SEMESTER - 2019**  
**Subject : PHARMACEUTICAL ENGINEERING -I Time: Three hours**

**Full Marks:100**

**Answer any five questions taking at least two questions from each group.)**

**Group A**

**Q1. (a)(i) Derive the expression of Rate of heat flow by conduction through a metallic cylinder :**

(ii) A cylindrical pipe of negligible thickness containing a hot fluid at  $150^{\circ}\text{C}$  and having an outer diameter of 0.4 m is insulated with three layers of each 60 mm thick insulation of thermal conductivities of  $k_1=0.02, k_2=0.06, k_3=0.16 \text{ W/mK}$  (starting from inside). The outside surface temperature is  $30^{\circ}\text{C}$ . Determine (i) heat loss by conduction per unit length of pipe and, (ii) interface temperature of insulating layers.

(b) Calculate the overall heat transfer coefficients based on both inside and outside areas for the following cases .

Case (i): water at  $10^{\circ}\text{C}$  flowing in a condenser tube (inside diameter,  $D_i=0.62 \text{ inch}$ , thickness of tube = $0.065 \text{ inch}$ ) and saturated steam at  $105^{\circ}\text{C}$  condensing on the outside.

$$h_i=12 \text{ kW/m}^2 \cdot \text{C}, h_o=14 \text{ kW/m}^2 \cdot \text{C}, k_m=120 \text{ W/m} \cdot \text{C}$$

Case (ii) Benzene condensing at atmospheric pressure ( $80^{\circ}\text{C}$ ) on the outside wall of a steel pipe (outside diameter,  $D_o=1.315 \text{ inch}$ , thickness of tube = $0.133 \text{ inch}$ ) and air at  $15^{\circ}\text{C}$  flowing within the pipe at 6 m/s.  $h_i=20 \text{ kW/m}^2 \cdot \text{C}, h_o=1200 \text{ kW/m}^2 \cdot \text{C}$

$$\text{and } k_m=45 \text{ W/m} \cdot \text{C}$$

**Marks (3+5)+(6+6)**

**Q2. (a) An aqueous solution of  $\text{NaNO}_3$  (M.W.85) is fed to a continuous crystallizer at a rate of 5000 kg/hr. The solution is cooled from  $90$  to  $40^{\circ}\text{C}$ . The cooling agent is water. Loss of water from feed due to evaporation in the crystallizer is 3% of the feed solution. Determine the quantity of heat (kilo watt) that must be withdrawn by the cooling agent.**

**Data:**

Mass fraction of  $\text{NaNO}_3$  in feed ( $x_F$ ), mother ( $x_L$ ) liquor and crystal ( $x_c$ ) are 0.5763, 0.5111 and 0.5941 respectively.

Heat capacity of feed solution ( $c_p$ ) =  $2469.57 \text{ J/kg}^{\circ}\text{K}$  Latent heat ( $\lambda$ ) of vaporization of water  $2345000 \text{ J/kg}$

Heat of crystallization of  $\text{NaNO}_3$  ( $h_c$ ) =  $248235.3 \text{ J/kg}$ .

**Solve by mass balance technique.**

(b) A solution containing 23% by mass of sodium phosphate (MW 164) is cooled from 313 to 298 K in a Swenson Walker crystallizer to form crystals of  $\text{Na}_3\text{PO}_4 \cdot 12\text{H}_2\text{O}$ . The solubility of  $\text{Na}_3\text{PO}_4$  at temperature 298 K is 13.42%, and the rate of product formation is 0.063 per second. The mean heat capacity of the solution is 3.2 kJ/kg K and the heat of crystallization is 146.5 kJ/kg of crystal. If cooling water enters and leaves at 288 and 293 K respectively, and the overall heat transfer coefficient is 0.14 kW/m<sup>2</sup>K. What length of crystallizer is required? Area of heat transfer per one meter is one square meter.

**Solve by mass balance technique.**

**Marks 10+10**

Q3. (a) Discuss various effects of system geometry (shape factors) on power number ( $N_p$ ) or power requirement.

(b) A tank 1.2 m in diameter and 2 m high which is filled to a depth of 1.2 m with a liquid having a viscosity of 11 poise and a density of 800 kg/m<sup>3</sup>. An impellor of diameter 360 mm is installed in the tank 360 mm from the bottom. The agitator rotates at 800 rpm. What are the power requirement for agitating liquid in both **baffled** and **unbaffled** tanks fitted with (i) **propeller** ( $a=1.7, b=18$ ) and (ii) **turbine** ( $a=1, b=40$ ) type impellers? Solve by graphical plotting on log-log graph papers.

Data for Propeller impellor						Data for Turbine type impellor					
$N_{Re}$	250	400	$10^3$	$2*10^3$	$10^4$	$N_{Re}$	200	300	$10^3$	$3*10^3$	$10^4$
Unbaffled, $N_p$	0.95	0.9	0.8	0.7	0.6	Unbaffled, $N_p$	3.7	3.8	2.7	1.75	1.4
Baffled, $N_p$	0.95	0.9	0.9	0.9	0.9	Baffled, $N_p$	3.7	3.8	4.5	5.3	6

**Marks 4+8\*2**

Q4. Write short notes on any four of the following:

- (i) Meirs Supersaturation theory, (ii) caking of crystal during storage, (iii) 1-2 Heat exchanger,
- (iv) Vortex in liquid mixing, (v) Ribbon blender, (vi) Turbine impellor system.

**Marks 4\*5**

B. PHARMACEUTICAL TECHNOLOGY THIRD YEAR SECOND SEMESTER -2019

PHARMACEUTICAL ENGINEERING-II

TIME: 3 h

FULL MARKS: 100

ANSWER ANY FIVE QUESTIONS TAKING ATLEAST TWO FROM EACH GROUP

GROUP-B

(Use graph paper if required)

1. A 6% aqueous solution of a high molecular weight solute has to be concentrated to 35% in a forward-feed double effect evaporator at the rate of  $8000 \text{ kg.h}^{-1}$ . The feed temperature is  $40^\circ\text{C}$ . Saturated steam at  $4.5 \text{ kg.cm}^{-2}$  is available for heating. A vacuum of  $600 \text{ mm Hg}$  is maintained in the second effect. Calculate the area requirements, if calandria of equal area are used. The overall heat transfer coefficients are  $650$  and  $470 \text{ kcal.h}^{-1}\text{m}^{-2} \text{ }^\circ\text{C}^{-1}$  in the first and the last effect respectively. The specific heat of the concentrated liquor is  $0.84 \text{ kcal.kg}^{-1}\text{C}^{-1}$ . [20 marks]
2.
  - a. A material is crushed in a Blake jaw crusher such that the average size of particle is reduced from  $40 \text{ mm}$  to  $10 \text{ mm}$  with the consumption of energy of  $13.0 \text{ kW/(kg/s)}$ . What would be the consumption of energy needed to crush the same material of average size  $75 \text{ mm}$  to an average size of  $25 \text{ mm}$ :
    - a) assuming Rittinger's law applies?
    - b) assuming Kick's law applies?Which of these results would be regarded as being more reliable and why?
  - b. The screen analysis shown in the table-1 below, applies to a sample of crushed quartz. The density of the particle is  $3000 \text{ kg/m}^3$ , and the shape factor are  $a=1.5$ , and  $\Phi_s=0.6$ . for the material between 4-mesh and 200 mesh in particle size, calculate a)  $A_w$ , and  $N_w$   
b)  $\bar{D}_v$  c)  $v \bar{D}_s$  d)  $\bar{D}_w$  e)  $\bar{N}$ , for the 150/200 mesh increment. f) What fraction of the total number of particles is in the 150/200-mesh increment?
  - c. Write short on any three: a. Ball Mill, b. Roller Mill, c. Hammer Mill, d. Fluid Energy Mill.
  - d. If crushing rolls,  $1\text{m}$  in diameter, are set so that the crushing surfaces are  $12.5\text{mm}$  apart and the angle of nip is  $31^\circ$ , what is the maximum size of particle which should be fed to the rolls? If the actual capacity of the machine is 20 per cent of the theoretical, calculate the throughout in  $\text{kg/s}$  when running at  $3.0 \text{ Hz}$  if the working face of the rolls is  $0.4 \text{ m}$  long and the bulk density of the feed is  $2500 \text{ kg/m}^3$ . [5+10+3+2=20 marks]
3.
  - a. Answer any three  
Explain the advantages and disadvantages of the following:
    - i. Cyclone Separator
    - ii. Dynamic Scrubbers
    - iii. Short-Tube Vertical Evaporator
    - iv. Gasketed Plate Evaporator
  - b. Derive the design equation of filtration. Using Sperry correlation derive the condition at constant pressure and incompressible sludge. Drive the filtration time cycle.

- c. A quartz mixture having the screen analysis shown in the table-2 below is screened through a standard 10-mesh screen. The cumulative screen analysis of the overflow and underflow are also provided. Calculate the mass ratios of the overflow and underflow to feed and the overall effectiveness of the screen.

[ $4 \times 3 = 12 + 4 + 4 = 20$  marks]

4.

- a. An evaporator is used to concentrate 5000 kg/h of a 15% solution of NaOH in water entering at  $65^\circ\text{C}$  to a product of 55% solids. The pressure of the saturated steam used is 25 psia and the pressure in the vapour space of the evaporator is 12 kPa. The overall heat transfer coefficient is  $1600 \text{ W/m}^2 \cdot \text{K}$ . Calculate the steam used, the steam economy in kg vaporized/kg steam used, and the heating surface area in  $\text{km}^2$ .
- b. Design a liquid-liquid gravity separator which can handle a two phase liquid stream of  $0.5 \text{ m}^3/\text{min}$ . The feed contains 45% by volume of light phase and 55% by volume of a heavy phase. Densities of light ( $\rho_l$ ) and heavy phase ( $\rho_h$ ) are 900 and  $1150 \text{ kg/m}^3$  respectively. Required settling time of light phase is 5 min while the settling time for heavy phase is 4 min.

[ $10 + 10 = 20$  marks]

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Supplementary Data

Table-1

Mesh	Screen opening $D_{ps}$ , mm	Mass fraction retained, $x_p$	Average particle diameter in increment, $D_p$ , mm	Cumulative fraction smaller than $D_p$
4	4.699	0.0000	—	1.0000
6	3.327	0.0251	4.013	0.9749
8	2.362	0.1250	2.845	0.8499
10	1.651	0.3207	2.007	0.5292
14	1.168	0.2570	1.409	0.2722
20	0.833	0.1590	1.001	0.1132
28	0.589	0.0538	0.711	0.0594
35	0.417	0.0210	0.503	0.0384
48	0.295	0.0102	0.356	0.0282
65	0.208	0.0077	0.252	0.0205
100	0.147	0.0058	0.178	0.0147
150	0.104	0.0041	0.126	0.0106
200	0.074	0.0031	0.089	0.0075
Pan	—	0.0075	0.037	0.0000

Table-2

Mesh	$D_{ps}$ , mm	Cumulative fraction smaller than $D_p$		
		Feed	Overflow	Underflow
4	4.699	0	0	—
6	3.327	0.025	0.071	—
8	2.362	0.15	0.43	0
10	1.651	0.47	0.85	0.195
14	1.168	0.73	0.97	0.58
20	0.833	0.885	0.99	0.83
28	0.589	0.94	1.00	0.91
35	0.417	0.96	—	0.94
65	0.208	0.98	—	0.975
Pan	—	1.00	—	1.00

Table 3 Saturation Temperature Table for Steam in SI Units

T C	P kPa	v m³/kg	w kg/kg	T <sub>s</sub> °C	L <sub>s</sub> /L <sub>v</sub>	L <sub>s</sub> /w	L <sub>s</sub> /v						
0	0.6110	0.000095	205.94	205.93	0.9907	2500.02	2499.12	0.9901	2373.12	0.9893	0.9888	0.9885	0.9882
2	0.7056	0.000093	176.63	176.63	0.9748	2504.40	2495.15	0.9745	2377.48	0.9734	0.9731	0.9727	0.9725
4	0.8140	0.000093	157.04	157.04	17.5929	2508.40	2491.01	17.5901	2380.76	17.5817	0.9604	0.9611	0.9628
6	0.9357	0.000093	137.50	137.50	25.9279	2512.64	2487.72	25.9269	2383.90	25.9257	0.9508	0.9520	0.9513
8	1.0722	0.000093	120.82	120.82	34.2306	2516.52	2492.21	34.2305	2386.91	34.2252	0.9409	0.9515	0.9509
10	1.2232	0.000093	106.31	106.31	42.5897	2520.42	2477.13	42.5885	2389.84	42.5875	0.9308	0.9416	0.9418
12	1.4025	0.000093	93.74	93.74	50.9100	2524.16	2472.27	50.9146	2392.20	50.9120	0.9204	0.9312	0.9313
14	1.5985	0.000093	82.33	82.33	59.2401	2527.50	2473.86	59.2385	2395.31	59.2367	0.9102	0.9210	0.9209
16	1.8100	0.000093	73.33	73.33	67.5925	2531.55	2474.02	67.5907	2399.47	67.5871	0.9059	0.9111	0.9111
18	2.0363	0.000093	63.64	63.64	75.8337	2535.23	2479.34	75.8317	2401.01	75.8253	0.9078	0.9163	0.9163
20	2.3776	0.000093	57.80	57.80	84.2413	2538.86	2484.65	84.2400	2403.53	84.2393	0.9094	0.9200	0.9205
22	2.8311	0.000093	51.47	51.47	92.5447	2542.46	2489.34	92.5420	2408.43	92.5391	0.9247	0.9298	0.9298
24	3.3936	0.000093	45.90	45.90	100.8445	2546.06	2495.21	100.8432	2409.12	2408.28	0.9351	0.9381	0.9380
26	3.9604	0.000093	41.02	41.02	109.486	2549.65	2499.48	109.4853	2411.21	2402.65	0.9411	0.9326	0.9372
28	4.7336	0.000093	36.22	36.22	117.482	2553.23	2495.74	117.481	2414.19	2407.01	0.9492	0.9453	0.9474
30	5.2429	0.000093	32.52	32.52	125.301	2556.81	2491.06	125.3007	2417.17	2401.36	0.9556	0.9556	0.9584
32	5.7556	0.000093	29.57	29.57	134.336	2561.39	2496.25	134.331	2419.44	2435.71	0.9640	0.9446	0.9493
34	6.3101	0.000093	26.60	26.60	142.462	2563.96	2491.50	142.456	2422.52	2439.06	0.9613	0.9744	0.9831
36	6.9128	0.000093	23.96	23.96	150.860	2566.53	2496.24	150.854	2425.19	2424.40	0.9583	0.9351	0.9168
38	7.6235	0.000093	21.62	21.62	159.120	2571.09	2491.97	159.113	2427.84	2468.74	0.9452	0.9268	0.9112
40	8.3753	0.000093	19.54	19.54	167.452	2574.65	2497.20	167.441	2430.22	2463.08	0.9310	0.9395	0.9395
42	9.1676	0.000093	17.69	17.69	175.786	2578.20	2502.41	175.778	2483.13	2457.41	0.9282	0.9210	0.9126
44	9.9927	0.000093	16.04	16.04	184.123	2581.75	2497.63	184.114	2495.24	2429.13	0.9248	0.9183	0.9104
46	10.844	0.000093	14.58	14.58	192.463	2585.30	2498.33	192.452	2498.30	2436.04	0.9310	0.9401	0.9470
48	11.162	0.000093	13.23	13.23	200.805	2588.87	2503.92	200.794	2441.11	2429.35	0.9271	0.9125	0.9354
50	11.533	0.000093	12.05	12.05	209.150	2593.34	2503.19	209.137	2443.78	2434.65	0.9230	0.9075	0.9145
52	11.910	0.000093	10.98	10.98	217.498	2598.86	2502.36	217.484	2446.22	2422.95	0.9287	0.9110	0.9145

T C	P* Pa	v <sub>t</sub> m <sup>3</sup> /kg	v <sub>r</sub> m <sup>3</sup> /kg	v <sub>b</sub> m <sup>3</sup> /kg	v <sub>f</sub> m <sup>3</sup> /kg	v <sub>fg</sub> m <sup>3</sup> /kg	v <sub>lg</sub> m <sup>3</sup> /kg	v <sub>g</sub> m <sup>3</sup> /kg	v <sub>l</sub> m <sup>3</sup> /kg	v <sub>fg</sub> m <sup>3</sup> /kg	v <sub>lg</sub> m <sup>3</sup> /kg	v <sub>g</sub> m <sup>3</sup> /kg	v <sub>l</sub> m <sup>3</sup> /kg	T <sub>s</sub> K
54	14.993	0.001014	10.02	225.843	2199.36	2373.51	225.833	240.04	2203.21	0.7543	2.0091	7.2547		
56	16.507	0.001015	9.159	9.158	234.202	2602.35	2368.65	234.185	2451.66	0.7708	0.79757	7.1959		
58	18.143	0.001016	8.381	8.380	242.558	2606.34	2363.78	242.540	2454.27	2211.73	0.8051	7.9428	7.1377	
60	19.916	0.001017	7.679	7.678	250.918	2609.30	2158.39	250.898	2456.87	2105.97	0.8302	7.9104	7.0802	
62	21.834	0.001018	7.044	7.043	259.281	2613.26	2153.98	259.259	2459.46	2100.20	0.8552	7.8786	7.0234	
64	23.906	0.001019	6.470	6.469	267.647	2616.70	2149.05	267.623	2462.04	2194.41	0.88201	7.8472	6.9671	
66	26.144	0.001020	5.949	5.948	276.016	2620.13	2344.11	275.990	2454.01	2188.62	0.9048	7.8163	6.9115	
68	28.557	0.001021	5.476	5.475	284.389	2623.54	2330.15	284.360	2457.16	2162.80	0.9264	7.7839	6.9564	
70	31.156	0.001022	5.047	5.046	291.765	2626.94	2334.16	292.733	2469.71	2176.97	0.9539	7.7559	6.8020	
72	33.952	0.001024	4.656	4.655	301.144	2630.32	2329.18	301.109	2472.24	2171.13	0.9712	7.7363	6.7481	
74	36.957	0.001025	4.309	4.309	310.527	2633.09	2324.16	310.499	2474.76	2165.27	1.0034	7.6972	6.6948	
76	40.184	0.001026	3.976	3.975	317.913	2637.04	2319.13	317.872	2477.27	2159.40	1.0265	7.6586	6.6421	
78	43.645	0.001028	3.680	3.679	326.303	2640.37	2314.07	326.258	2479.76	2153.51	1.0505	7.6403	6.5809	
80	47.153	0.001029	3.409	3.408	334.686	2643.09	2306.90	334.658	2482.25	2147.60	1.0743	7.6123	6.5382	
82	51.322	0.001030	3.162	3.161	343.063	2646.99	2303.90	343.040	2484.72	2141.68	1.0986	7.5850	6.4970	
84	55.567	0.001032	2.935	2.934	351.444	2650.27	2308.78	351.427	2487.17	2135.74	1.1216	7.5579	6.4364	
86	60.102	0.001033	2.727	2.726	359.829	2653.53	2293.64	359.807	2490.92	2128.78	1.1450	7.5313	6.3862	
88	64.942	0.001034	2.537	2.536	368.308	2656.76	2288.47	368.280	2492.04	2121.80	1.1684	7.5050	6.3366	
90	70.104	0.001036	2.361	2.360	376.720	2660.01	2281.36	376.698	2494.46	2117.81	1.1916	7.4790	6.2874	
92	75.603	0.001037	2.200	2.199	385.117	2663.21	2278.03	385.099	2498.86	2111.80	1.2147	7.4534	6.2382	
94	81.457	0.001038	2.052	2.051	393.552	2666.40	2272.94	393.474	2498.25	2105.77	1.2377	7.4282	6.1905	
96	87.683	0.001040	1.915	1.914	401.984	2669.57	2277.58	401.893	2501.62	2099.73	1.2606	7.4033	6.1427	
98	94.299	0.001042	1.780	1.778	410.414	2672.73	2281.30	410.316	2503.98	2093.66	1.2833	7.3787	6.0954	
100	101.325	0.001043	1.673	1.672	418.849	2675.94	2286.99	418.743	2506.32	2087.57	1.3060	7.3545	6.0485	
102	108.778	0.001045	1.566	1.565	427.289	2678.55	2291.66	427.175	2508.64	2081.47	1.3285	7.3106	6.0020	
104	116.678	0.001046	1.466	1.465	435.733	2682.03	2301.30	435.611	2510.95	2075.34	1.3510	7.3070	5.9560	
106	125.047	0.001048	1.374	1.373	444.183	2685.09	2296.91	444.052	2513.25	2069.19	1.3733	7.2837	5.9103	
108	133.905	0.001050	1.289	1.288	452.638	2688.13	2315.49	452.498	2515.52	2063.03	1.3955	7.2606	5.8651	
110	143.773	0.001051	1.210	1.209	461.099	2691.14	2320.04	460.948	2517.78	2056.83	1.4177	7.2379	5.8203	

T	P <sub>c</sub>	v <sub>f</sub>	v <sub>b</sub>	v <sub>d</sub>	v <sub>e</sub>	v <sub>g</sub>	v <sub>h</sub>	v <sub>i</sub>	v <sub>j</sub>	v <sub>k</sub>	v <sub>l</sub>	v <sub>m</sub>	v <sub>n</sub>	v <sub>o</sub>	v <sub>p</sub>	v <sub>q</sub>	v <sub>r</sub>	v <sub>s</sub>	v <sub>t</sub>	
C	L <sub>12</sub>	middle	middle																	
112	153.173	0.001033	1.136	469.565	2694.12	2224.57	469.404	2520.03	2056.2	1.4397	7.2155	5.7758								
114	163.628	0.001035	1.098	478.038	2697.10	219.06	477.865	3522.5	2044.8	1.4616	7.1935	5.7118								
116	174.662	0.001037	1.004	486.516	2700.04	2113.52	486.311	1524.6	2038.12	1.4384	7.1715	5.6800								
118	186.297	0.001038	0.945331	495.001	2702.95	2207.95	494.804	2526.64	2031.84	1.5051	7.1498	5.6447								
120	198.559	0.001039	0.891572	503.993	2705.84	2202.35	503.282	1528.81	2026.53	1.5267	7.1285	5.6017								
122	211.972	0.001039	0.840501	0.833438	511.991	2708.70	2198.71	511.766	2530.96	2019.9	1.5483	7.1074	5.5591							
124	225.062	0.001040	0.792831	0.701917	520.495	2711.51	2191.9	520.257	2533.09	2019.4	1.5697	7.0885	5.5108							
126	239.354	0.001040	0.748448	0.747382	529.009	2714.34	2185.33	528.754	2535.19	2006.44	1.5910	7.0659	5.4749							
128	254.377	0.001048	0.706958	0.705890	537.530	2717.11	2179.58	537.258	2537.28	2000.02	1.6123	7.0455	5.4332							
130	270.156	0.001040	0.668182	0.667118	546.058	2719.86	2173.30	545.769	2533.97	1993.57	1.6334	7.0254	5.3919							
132	286.720	0.001077	0.631933	0.630880	551.505	2722.57	2167.93	551.287	2541.38	1987.69	1.6545	7.0054	5.3510							
134	304.097	0.001074	0.598007	0.598033	562.140	2725.25	2162.11	562.813	2543.40	1980.59	1.6754	6.9857	5.3108							
136	322.317	0.001076	0.566238	0.566162	571.693	2727.90	2156.21	571.347	2545.39	1974.05	1.6963	6.9662	5.2699							
138	341.408	0.001078	0.53566	0.535391	580.256	2730.52	2150.25	580.088	2547.36	1967.47	1.7171	6.9469	5.2358							
140	361.402	0.001080	0.508556	0.508476	588.828	2733.10	2144.27	588.418	2549.31	1960.87	1.7378	6.9279	5.1900							
142	382.328	0.001082	0.482365	0.482283	597.410	2735.65	2138.24	596.986	2551.23	1954.23	1.7585	6.9090	5.1505							
144	404.219	0.001084	0.457774	0.456930	606.002	2738.16	2132.16	605.584	2553.12	1947.55	1.7790	6.8903	5.1113							
146	427.106	0.001086	0.434672	0.433535	614.004	2740.64	2126.03	614.110	2554.98	1940.84	1.7995	6.9778	5.0723							
148	451.022	0.001089	0.412954	0.411865	623.217	2743.97	2119.96	622.766	2558.17	1913.62	1.8205	6.7395	4.9100							
150	476.000	0.001091	0.392524	0.391333	631.841	2745.47	2113.63	631.322	2558.63	1906.72	1.8406	6.7172	4.8800							
152	500.271	0.001093	0.373205	0.372202	640.470	2747.34	2107.03	640.938	2560.41	1900.41	1.8604	6.6904	4.7996							
154	529.277	0.001095	0.355186	0.355090	649.124	2750.16	2101.04	648.544	2563.17	1901.62	1.8806	6.7130	4.7118							
156	557.644	0.001096	0.338120	0.338120	657.783	2752.44	2094.66	657.170	2561.89	1898.77	1.9007	6.7300	4.6338							
158	587.212	0.001100	0.320226	0.320050	669.454	2754.98	2088.23	668.848	2565.58	1895.77	1.9206	6.7745	4.5600							
160	618.016	0.001102	0.306849	0.305747	675.138	2756.88	2081.74	674.457	2567.24	1892.76	1.9406	6.8130	4.4838							
162	650.002	0.001105	0.292510	0.291414	683.836	2759.04	2075.30	683.117	2568.87	1885.75	1.9604	6.7300	4.4100							
164	683.477	0.001107	0.278035	0.277878	692.546	2761.15	2068.60	691.790	2570.47	1878.68	1.9802	6.7130	4.3318							
166	718.210	0.001110	0.266105	0.265165	701.271	2763.22	2061.95	700.474	2571.01	1871.56	2.0000	6.6901	4.2662							
168	754.324	0.001112	0.254112	0.252950	710.010	2765.24	2055.23	709.171	2573.56	1864.39	2.0106	6.6794	4.1593							

T	P <sub>c</sub>	n <sub>1</sub>	n <sub>2</sub>	n <sub>3</sub>	n <sub>4</sub>	n <sub>5</sub>	n <sub>6</sub>	n <sub>7</sub>	n <sub>8</sub>	n <sub>9</sub>	n <sub>10</sub>	n <sub>11</sub>	n <sub>12</sub>	n <sub>13</sub>	n <sub>14</sub>	n <sub>15</sub>
170	791.970	0.000115	0.242680	0.241547	718.764	2767.22	2048.45	711.981	2570.06	1857.13	2.0302	6.64923	4.6226			
172	874.075	0.000117	0.113844	0.1130717	727.532	2769.15	2041.92	726.684	2570.52	1856.92	2.0303	6.6494	4.5876			
174	877.184	0.000120	0.221580	0.220461	716.316	2771.03	2034.71	735.340	2571.95	1842.61	2.0782	6.6301	4.5338			
176	937.436	0.000122	0.211855	0.210743	745.116	2772.57	2027.75	744.901	2573.41	1835.25	2.0976	6.6139	4.5162			
178	977.023	0.000125	0.202656	0.201531	753.931	2774.65	2020.72	752.835	2580.60	1827.84	2.1170	6.5978	4.4408			
180	1002.34	0.000126	0.193022	0.192704	761.764	2776.30	2013.62	761.634	2582.01	1830.38	2.1163	6.5818	4.4156			
182	1049.27	0.000130	0.185615	0.185004	771.613	2778.07	2006.46	770.427	2583.29	1818.71	2.1555	6.5660	4.4005			
184	1097.91	0.000133	0.177767	0.176634	780.480	2779.71	1969.23	779.236	2584.54	1806.30	2.1747	6.5502	4.3756			
186	1148.30	0.000136	0.170955	0.169159	789.364	2781.20	1991.93	788.001	2585.74	1767.82	2.1938	6.5346	4.3488			
188	1200.50	0.000139	0.163195	0.162057	798.266	2782.32	1984.56	795.899	2586.91	1790.01	2.2120	6.5191	4.3062			
190	1254.51	0.000141	0.156466	0.155304	807.167	2784.30	1977.11	805.555	2588.03	1781.28	2.2302	6.4729	4.2033			
192	1310.45	0.000144	0.150807	0.149622	816.117	2785.72	1969.60	814.227	2589.12	1774.49	2.2505	6.4383	4.1375			
194	1368.30	0.000147	0.143919	0.142772	825.906	2787.00	1952.01	823.516	2590.17	1766.05	2.2691	6.4017	4.0681			
196	1428.14	0.000150	0.136955	0.134654	837.007	2790.37	1932.06	832.422	2591.18	1751.75	2.2886	6.3776	4.0003			
198	1533.92	0.000152	0.127293	0.126157	842.875	2792.75	1910.80	850.286	2591.07	1742.18	2.3102	6.3479	3.9347			
200	1581.00	0.000155	0.119538	0.118415	848.163	2793.97	1905.61	841.345	2592.14	1736.95	2.3354	6.3101	3.8687			
202	1619.96	0.000159	0.112266	0.111106	851.123	2795.06	1903.80	850.555	2593.95	1724.71	2.3540	6.2540	3.9017			
204	1682.17	0.000163	0.104742	0.103690	870.164	2795.11	1922.92	868.222	2594.70	1716.55	2.3735	6.2350	3.8687			
206	1753.60	0.000167	0.099244	0.098533	875.905	2796.30	1932.00	877.217	2595.59	1715.18	2.3832	6.2013	3.8687			
208	1831.29	0.000170	0.096598	0.095490	915.928	2802.73	2095.11	1896.74	2596.35	1704.12	2.4007	6.1863	3.9017			
210	1906.30	0.000172	0.093369	0.092501	925.028	2803.40	1932.90	1905.95	2597.05	1694.97	2.4193	6.1778	3.8687			
212	1981.67	0.000176	0.089240	0.088320	934.250	2803.07	1940.22	1904.21	2597.24	1693.41	2.4377	6.1339	3.8687			
214	2066.46	0.000179	0.085160	0.084156	943.498	2803.73	1951.11	1906.74	2598.35	1704.12	2.4567	6.1268	3.8687			
216	2145.71	0.000182	0.081555	0.080793	952.772	2804.13	1947.45	940.741	2599.49	1671.88	2.4746	6.1177	3.7704			
218	2230.45	0.000186	0.078481	0.077485	960.272	2804.72	1958.95	949.899	2600.44	1650.54	2.5065	6.0973	3.7378			
220	2317.81	0.000190	0.075195	0.074193	969.028	2805.13	1967.46	1076.46	2601.84	1641.77	2.5418	6.0730	3.7053			
222	2407.50	0.000193	0.072579	0.071579	978.076	2805.53	1976.55	1086.46	2603.84	1631.3	2.5817	6.0210	3.6704			
224	2500.45	0.000197	0.069955	0.068955	987.076	2806.13	1985.65	1095.46	2605.84	1621.77	2.5918	6.0001	3.6704			
226	2595.84	0.000200	0.067320	0.067021	991.397	2801.21	1991.44	1169.74	968.281	1632.93	1.5660	6.2188	3.6728			

T C	P <sub>c</sub> kPa	v <sub>t</sub> m <sup>3</sup> /kg	v <sub>s</sub> m <sup>3</sup> /kg	v <sub>f</sub> m <sup>3</sup> /kg	v <sub>fg</sub> m <sup>3</sup> /kg	v <sub>g</sub> m <sup>3</sup> /kg	v <sub>l</sub> m <sup>3</sup> /kg	v <sub>lg</sub> m <sup>3</sup> /kg	v <sub>v</sub> m <sup>3</sup> /kg	v <sub>lv</sub> m <sup>3</sup> /kg	v <sub>l</sub> m <sup>3</sup> /kg	v <sub>fg</sub> m <sup>3</sup> /kg	v <sub>g</sub> m <sup>3</sup> /kg	v <sub>l</sub> m <sup>3</sup> /kg	v <sub>lg</sub> m <sup>3</sup> /kg
228	2684.01	0.001204	0.074220	0.073025	980.750	2801.50	1820.75	977.506	2601.53	1624.02	2.3541	6.2245	3.6404		
230	2795.02	0.001206	0.071555	0.070346	990.131	2801.50	1811.67	986.754	2601.50	1615.05	2.0823	6.2104	3.6081		
232	2898.94	0.001212	0.068091	0.067779	999.539	2802.06	1802.49	996.025	2602.03	1606.00	2.0604	6.1963	3.5759		
234	3005.81	0.001216	0.065552	0.065316	1008.93	2802.19	1793.23	1005.32	2602.21	1596.89	2.0534	6.1821	3.5437		
236	3115.69	0.001220	0.064174	0.062954	1018.44	2802.30	1783.85	1014.64	2602.35	1587.71	1.9594	6.1680	3.5116		
238	3228.65	0.001224	0.061911	0.060887	1027.94	2802.33	1774.39	1021.99	2602.44	1578.46	2.0474	6.1539	3.4795		
240	3344.74	0.001228	0.059739	0.058511	1037.46	2802.30	1764.94	1031.36	2602.49	1569.13	2.0323	6.1398	3.4475		
242	3464.02	0.001233	0.057654	0.056421	1047.02	2802.21	1755.19	1042.75	2602.49	1559.74	2.0192	6.1258	3.4155		
244	3586.55	0.001237	0.055651	0.054414	1056.61	2802.05	1745.53	1052.17	2602.15	1550.28	2.0021	6.1117	3.3836		
246	3712.39	0.001242	0.053727	0.052486	1065.23	2801.82	1735.93	1061.62	2602.36	1540.74	1.9789	6.0977	3.3517		
248	3841.61	0.001246	0.051878	0.050632	1075.89	2801.52	1725.63	1071.10	2602.23	1531.13	2.0738	6.0836	3.3199		
250	3974.26	0.001251	0.050100	0.048850	1085.58	2801.16	1715.38	1080.60	2602.05	1521.41	2.0815	6.0696	3.2880		
252	4110.40	0.001256	0.048331	0.047135	1095.30	2800.73	1705.43	1090.14	2601.82	1511.88	2.0793	6.0555	3.2562		
254	4250.11	0.001260	0.046747	0.045486	1105.06	2800.23	1695.17	1099.70	2601.55	1501.85	2.0370	6.0414	3.2245		
256	4393.44	0.001265	0.045164	0.043899	1114.85	2799.66	1684.81	1100.29	2601.23	1491.94	2.0346	6.0073	3.1927		
258	4540.47	0.001270	0.043661	0.042371	1124.69	2799.02	1674.34	1118.92	2600.87	1481.95	2.0223	6.0032	3.1610		
260	4691.15	0.001275	0.042175	0.040900	1134.56	2798.32	1663.76	1126.57	2600.45	1471.89	2.0099	5.9991	3.1293		
262	4845.85	0.001281	0.040753	0.039483	1144.47	2797.54	1653.06	1138.26	2600.01	1461.75	2.0074	5.9850	3.0976		
264	5004.33	0.001286	0.039443	0.038117	1154.42	2796.70	1642.26	1147.98	2599.51	1451.53	1.9650	5.9708	3.0659		
266	5166.78	0.001291	0.038093	0.036801	1164.41	2795.79	1631.38	1157.74	2598.97	1441.23	2.0225	5.9566	3.0342		
268	5333.25	0.001297	0.036819	0.035532	1174.44	2794.80	1620.36	1167.53	2598.38	1430.85	2.0099	5.9424	3.0023		
270	5503.82	0.001303	0.035622	0.034309	1184.52	2793.75	1609.23	1177.35	2597.75	1420.40	2.0074	5.9394	2.9708		
272	5672.56	0.001309	0.034437	0.033129	1194.64	2792.62	1597.98	1187.21	2597.07	1409.56	2.0048	5.9139	2.9391		
274	5857.53	0.001315	0.033304	0.031990	1204.81	2791.43	1586.62	1197.11	2596.35	1399.23	2.0021	5.8995	2.9074		
276	6040.80	0.001321	0.032211	0.030891	1215.03	2790.16	1575.13	1207.05	2595.58	1388.53	3.0094	5.8852	2.8757		
278	6223.47	0.001327	0.031157	0.029830	1225.29	2788.82	1563.53	1217.03	2594.76	1377.73	3.0067	5.8707	2.8440		
280	6420.58	0.001333	0.030158	0.028805	1235.61	2787.41	1551.80	1227.05	2593.91	1366.86	3.0040	5.8562	2.8123		
282	6617.23	0.001340	0.029155	0.027816	1245.98	2785.93	1539.95	1237.12	2593.01	1355.89	3.0012	5.8417	2.7805		
284	6818.48	0.001346	0.028206	0.026859	1256.40	2784.38	1527.98	1247.22	2592.06	1344.84	3.0084	5.8271	2.7488		

T	P <sub>c</sub>	V <sub>t</sub>	V <sub>r</sub>	V <sub>b</sub>	V <sub>a</sub>	V <sub>d</sub>	V <sub>e</sub>	V <sub>f</sub>	V <sub>g</sub>	V <sub>h</sub>	V <sub>i</sub>	V <sub>j</sub>	V <sub>k</sub>	V <sub>l</sub>	V <sub>m</sub>	V <sub>n</sub>	V <sub>o</sub>	V <sub>p</sub>	V <sub>q</sub>	V <sub>r</sub>
286	7024.42	0.001363	0.017588	0.025915	1266.88	2782.75	1515.87	1257.18	2611.07	1313.69	3.0955	5.8125	2.7170							
288	7235.11	0.001360	0.016602	0.025042	1277.42	2781.05	1503.64	1267.58	2590.03	1322.45	3.1126	5.7977	2.6852							
290	7450.65	0.001367	0.015445	0.024178	1283.01	2779.26	1491.27	1277.83	2538.96	1311.13	3.1296	5.7890	2.6533							
292	7661.10	0.001374	0.014717	0.023343	1295.67	2777.44	1478.77	1282.13	2537.83	1299.71	3.1166	5.7801	2.6315							
294	7886.54	0.001382	0.013917	0.022535	1309.39	2775.53	1486.14	1298.48	2586.07	1282.19	3.1635	5.7532	2.5896							
296	8127.07	0.001388	0.013142	0.021753	1220.18	2771.54	1453.36	1308.89	2535.46	1276.57	3.1804	5.7382	2.5578							
298	8358.76	0.001387	0.012393	0.020696	1311.03	2771.47	1440.44	1319.35	2584.20	1264.85	3.1972	5.7231	2.5259							
300	8583.60	0.001385	0.011669	0.019653	1341.95	2789.34	1427.38	1329.87	2582.91	1253.04	3.2139	5.7079	2.4940							
302	8805.96	0.001413	0.010667	0.015554	1352.95	2767.13	1414.16	1340.45	2581.57	1241.11	3.2106	5.6927	2.4621							
304	9011.63	0.001421	0.010238	0.018857	1364.04	2764.84	1400.80	1351.10	2580.18	1230.03	3.2472	5.6773	2.4302							
306	9358.81	0.001390	0.019531	0.018601	1375.19	2762.48	1387.29	1361.81	2578.76	1216.95	3.2616	5.6619	2.3982							
308	9621.53	0.001410	0.018995	0.017556	1386.43	2760.05	1373.62	1372.50	2577.29	1204.70	3.2860	5.6463	2.3664							
310	9890.03	0.001488	0.018379	0.016931	1397.76	2757.54	1359.78	1381.47	2575.77	1192.34	3.2962	5.6307	2.3345							
312	10164.34	0.001457	0.017782	0.016235	1409.17	2754.96	1445.79	1394.36	2574.22	1179.86	3.3123	5.6150	2.3027							
314	10444.32	0.001466	0.017303	0.015137	1420.68	2753.20	1331.62	1405.16	2572.62	1167.20	3.3282	5.5991	2.2709							
316	10780.34	0.001476	0.016643	0.015167	1432.28	2749.56	1317.22	1404.44	2570.92	1154.54	3.3439	5.5832	2.2393							
318	11022.41	0.001486	0.016100	0.014664	1443.98	2746.75	1302.77	1427.61	2569.30	1141.69	3.3584	5.5671	2.2077							
320	11300.63	0.001496	0.015373	0.014978	1455.79	2743.87	1288.08	1438.86	2567.57	1128.71	3.3746	5.5510	2.1764							
322	11626.06	0.001496	0.015663	0.015357	1467.71	2741.91	1273.20	1450.30	2565.80	1115.60	3.3805	5.5347	2.1452							
324	11935.86	0.001517	0.014568	0.014952	1479.74	2737.87	1258.13	1461.64	2563.90	1102.35	3.4041	5.5183	2.1142							
326	12251.07	0.001527	0.014086	0.012561	1491.88	2734.76	1244.87	1473.17	2562.13	1098.96	3.4182	5.5018	2.0886							
328	12576.82	0.001538	0.013623	0.012303	1504.15	2731.57	1227.41	1484.81	2560.24	1075.43	3.4318	5.4851	2.0553							
330	12907.21	0.001550	0.013171	0.011622	1516.55	2728.30	1211.75	1496.55	2558.20	1061.74	3.4448	5.4684	2.0235							
332	13244.33	0.001561	0.012733	0.011172	1529.09	2724.96	1195.87	1508.41	2556.31	1047.90	3.4571	5.4515	1.9944							
334	13585.29	0.001573	0.013033	0.010735	1541.76	2721.54	1179.78	1520.38	2554.28	1033.90	3.4685	5.4344	1.9659							
336	13909.20	0.001585	0.012611	0.010311	1554.57	2718.04	1165.46	1532.48	2552.21	1019.74	3.4788	5.4173	1.9384							
338	14230.16	0.001598	0.011496	0.009998	1567.54	2714.46	1146.92	1544.70	2550.10	1005.40	3.4879	5.4000	1.9121							
340	14563.20	0.001611	0.011068	0.009497	1580.67	2710.91	1130.14	1557.05	2547.94	990.89	3.4953	5.3825	1.8972							
342	15034.68	0.001624	0.010751	0.0099107	1593.96	2707.08	1113.11	1568.55	2545.74	976.19	3.3609	5.3649	1.8641							

T C	P <sub>at</sub> kPa	v <sub>t</sub> m <sup>3</sup> /kg	v <sub>c</sub> m <sup>3</sup> /kg	v <sub>d</sub> m <sup>3</sup> /kg	b <sub>t</sub> m <sup>3</sup> /kg	b <sub>c</sub> m <sup>3</sup> /kg	b <sub>d</sub> m <sup>3</sup> /kg	u <sub>t</sub> kJ/kg	u <sub>c</sub> kJ/kg	u <sub>d</sub> kJ/kg	s <sub>t</sub> kJ/kg K	s <sub>c</sub> kJ/kg K	s <sub>d</sub> kJ/kg K
344	15914.47	0.001637	0.010655	0.008728	1607.42	2703.26	1685.54	1582.19	2543.50	961.31	3.5040	5.3472	1.8433
346	15901.74	0.001651	0.010609	0.008359	1621.07	2699.38	1678.31	1594.98	2541.21	946.73	3.5040	5.3294	1.8254
348	16196.03	0.001655	0.008664	0.008000	1641.90	2695.41	1660.51	1607.93	2538.18	930.94	3.5002	5.3114	1.8111
350	16399.25	0.001679	0.008630	0.007650	1648.92	2691.36	1642.44	1621.05	2536.50	915.45	3.4915	5.2932	1.8017
352	17009.71	0.001694	0.008604	0.007111	1665.15	2687.24	1624.06	1634.34	2534.07	899.73	3.4764	5.2749	1.7985
354	17428.13	0.001709	0.008589	0.006980	1677.60	2683.03	1655.93	1647.81	2531.00	883.79	3.4528	5.2565	1.8036
356	17833.94	0.001724	0.008582	0.006538	1692.26	2678.75	986.48	1661.47	2529.09	867.61	3.4170	5.2378	1.8169
358	18286.36	0.001740	0.008584	0.006344	1707.16	2674.38	967.22	1675.33	2526.52	851.19	3.3676	5.2191	1.8315
360	18732.41	0.001756	0.008585	0.006039	1722.30	2669.91	947.64	1689.40	2523.91	834.51	3.3154	5.2002	1.9047
362	19183.91	0.001773	0.008574	0.005741	1737.69	2665.41	927.72	1703.63	2521.26	817.57	3.1918	5.1801	1.9863
364	19634.00	0.001790	0.007242	0.005452	1753.35	2660.81	907.45	1718.19	2518.55	800.36	3.0409	5.1610	2.1210
366	20112.81	0.001807	0.006937	0.005170	1769.28	2656.12	886.84	1732.93	2515.79	782.56	2.8150	5.1425	2.1276
368	20590.46	0.001825	0.006720	0.004895	1785.50	2651.35	865.85	1747.93	2512.99	765.06	2.4610	5.1230	2.6620
370	21077.08	0.001843	0.006570	0.004627	1810.03	2646.50	844.48	1763.17	2510.13	746.95	5.1033	5.1033	3.2451
372	21572.82	0.001862	0.006328	0.004366	1838.56	2641.57	822.71	1778.69	2507.22	728.53	0.5930	5.0835	4.4864
374	22077.11	0.001881	0.006193	0.004111	1866.02	2636.56	800.54	1794.49	2504.26	709.77	-19.7443	5.0635	24.3977

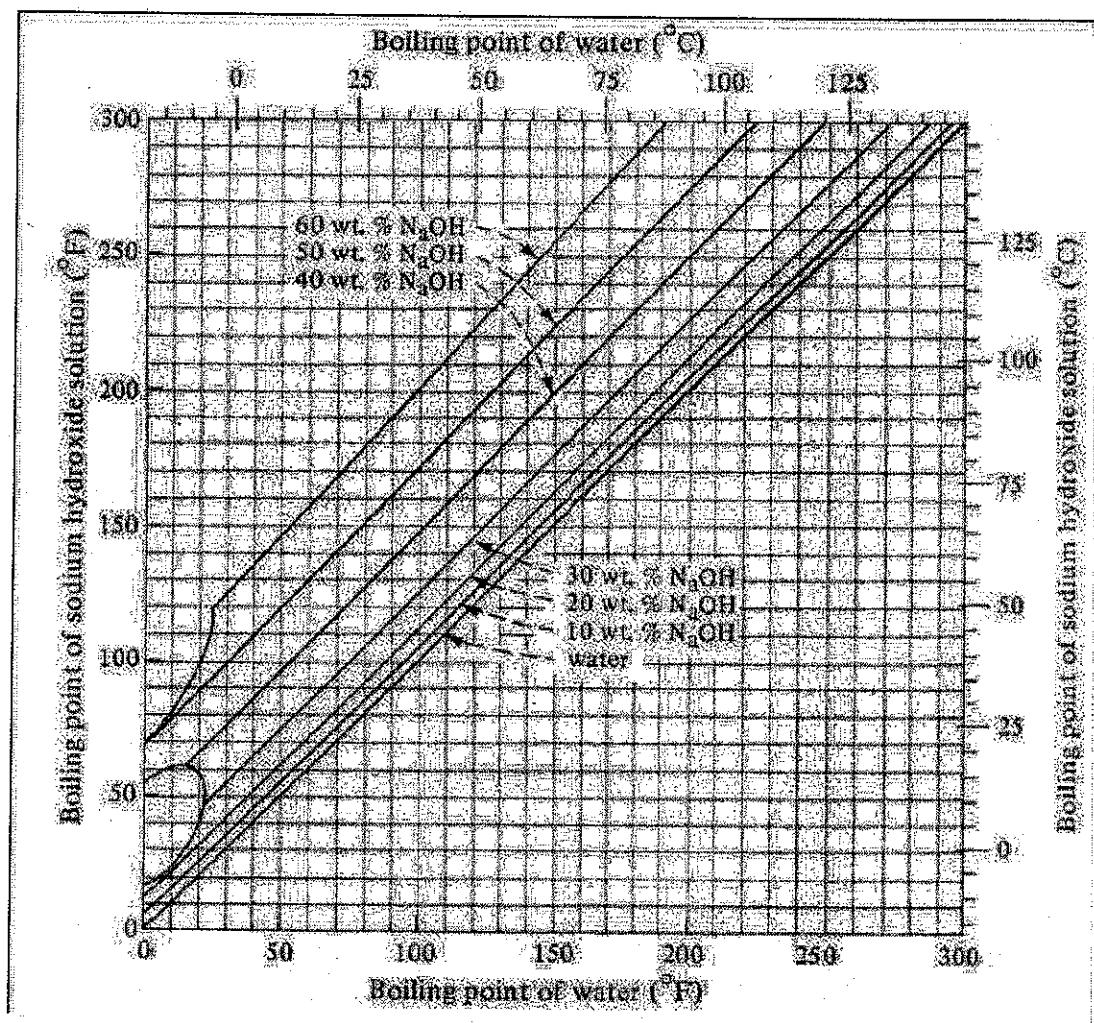


Figure. 1 Duhring lines for aqueous solutions of sodium hydroxide.

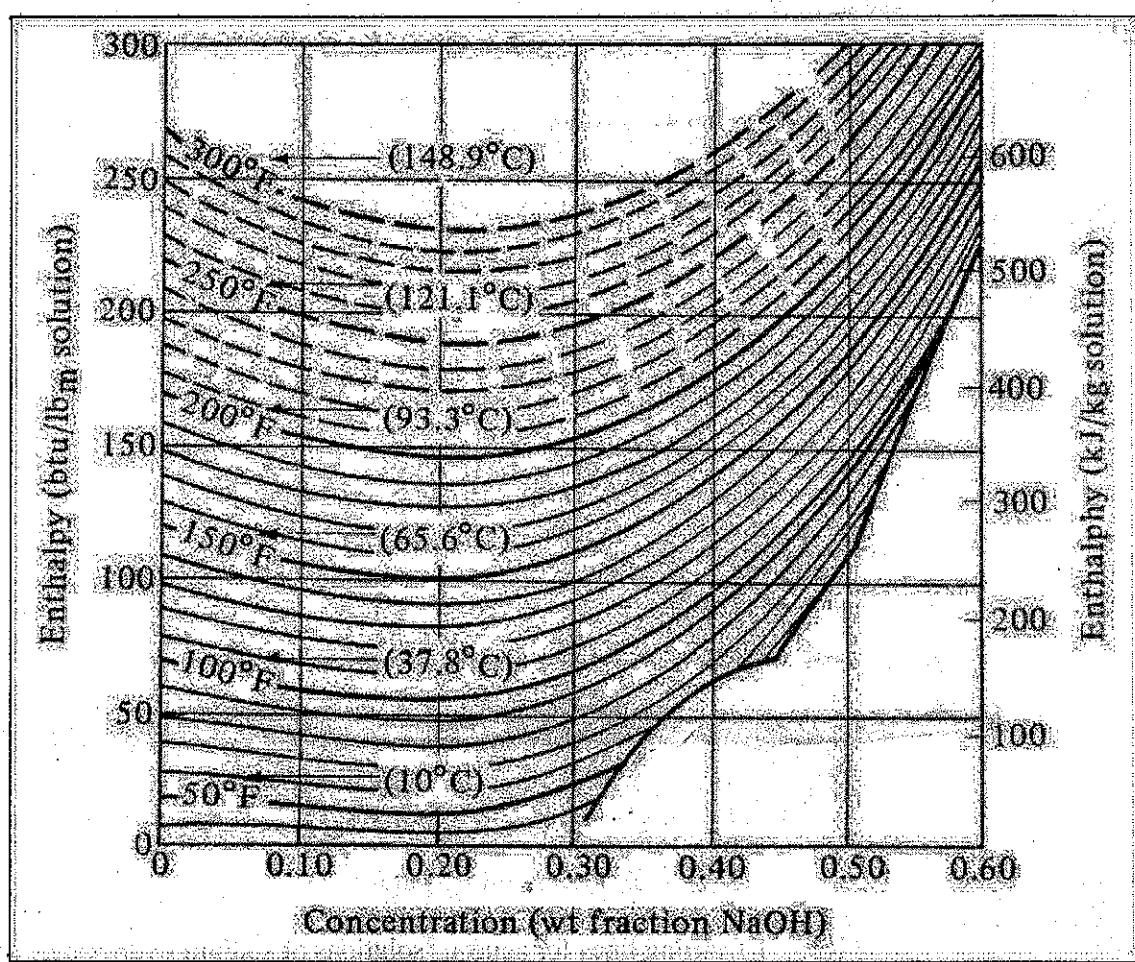


Figure.2 Enthalpy concentration chart for the system NaOH water.