# Bachelor of Engineering in Food Technologt and Biochemical Engg. Examination, 2018 

(3rd Year, 2ndSemester)
Mass Transfer Operation - I
Time : Three hours
Full Marks : 100
( 50 marks for each Part)
Use a separate Answer-Script for each Part
PART - I
Any Three Questions from Q. No. 1-4 and Q. No. 5 is compulsory.
Q.No. 1.
a) With the help of concentration in the solid phase, which is expressed as $q$ [ kg absorbate (solute) / kg absorbent (solid) ], and in the fluid phase (gas or liquid) as C ( kg absorbate $/ \mathrm{m}^{3}$ fluid), define the following equation with a neat diagram of adsorption isotherm [ $q$ vs $C$ ]:
i) Henry's Isotherm Equation
iI) Freundlich Isotherm Equation
iii) Langmulr Isotherm Equation
b) Discuss the temperature effect on adsorption and desorption.
c) Explain the difference between absorbtion and adsorption.
Q.No.2.
a) Explain the Distribution Co-efficient for both the dilute and the concentrated solution.
b) With a help of an equilateral triangular co-ordinate, draw the equilibrium data of three component system and explaln all the Inhererit phases mass fraction and component percentage at major locations based on the triangular diagram.
c) With the region of ambivalence, the selection of the phase to be dispersed depends on various consideration. Explain those considerations briefly.
Q.No.3.

Differentlate between the following two operating lines (considering both mass balance and component balance ) :
Q.No.4.

$$
\begin{gathered}
y_{n+1}=\frac{L_{n} x_{n}}{V_{n+1}}+\frac{V_{1} y_{1}-L_{0} x_{0}}{V_{n+1}} \\
x_{n+1}=\frac{y_{n}}{1+\frac{V_{1}-L_{0}}{L_{n}}}+\frac{V_{1} x_{1}-L_{0} x_{0}}{L_{n}+V_{1}-L_{0}}
\end{gathered}
$$

a) Draw the following diagrams depicting the Feed, Solvent, Raffinate and Extract for both input and output of each stage, mentioning all details so as to make total material balance and component balance for the entire stages involved in the system.
i) Single Stage Extraction System
ii) Multistage Cross-current System
iii) Multstage Counter-current System
b) Prove the following equation ( considering the multistage cross-current System ):

$$
\begin{equation*}
x_{3}=\frac{x_{F}}{\left(\frac{R_{1}}{F}+\frac{E_{1} K}{F}\right)\left(\frac{R_{2}}{R_{1}}+\frac{E_{2} K}{R_{1}}\right)\left(\frac{R_{3}}{R_{2}}+\frac{E_{3} K}{R_{2}}\right)} \tag{04}
\end{equation*}
$$

Ref. No. Ex/ ETM.BE./KT.....3.35.......2018
Q.No.5. (Attempt any two questions)
a) It is desired to absorb $90 \%$ of the acetone in a gas containing $1.0 \mathrm{~mol} \%$ acetone in air in a counter - current stage tower. The total inlet gas flow to the tower is $30 \mathrm{kgmol} / \mathrm{h}$ and the total inlet pure water flow to be used to absorb the acetone is $90 \mathrm{kgmol} \mathrm{H}_{2} \mathrm{O} / \mathrm{h}$. the process is to operate isothermally at 300 K and a total pressure of $101.3 \mathrm{kP} \mathrm{P}_{\mathrm{A}}$. The equilibrium relation for the Acetone (A) in the gas-liquid is $\cdot y_{A}=2.53 x_{A}$. Determine the number of theoretical stages required for this separation.
b) Keeping all the parameters same as above, find the number of theoretical stages required for the purpose using Analytical Method and conclude your view on the subject using both the method, namely, Graphical method and Analytical method.
c) 150 kg of nicotine-water solution containing $1 \%$ nicotine is to be extracted with 250 kg of kerosene at $20^{\circ} \mathrm{C}$. Water and Kerosene are essentially immiscible in each other. Determine the percentage extraction of nicotine after one stage operation. At the dilute end of the system, the equilibrium relationship is $\gamma^{*}=0.798 X$ where $\gamma$ and $X$ are expressed as kg nicotine $/ \mathrm{kg}$ kerosene and kg nicotine / kg water, respectively.

## B.E. FOOD TECHNOLOGY AND BIO-CHEMICAL ENGINEERING

## THIRD YEAR SECOND SEMESTER EXAM 2018

## Mass Transfer Operation I

Time: 3 hrs.
Full Marks: 100
Part-II (Marks 50 )

1. Answer any one from the following (a) and (b)
a. (i) State Fick's first law of diffusion and find the dimension of diffusivity.
(ii) Find the relation between the diffusivities of the components in a binary mixture.
(iii) In a gas system molecular diffusion is slow process, however you can make it faster-how?

$$
(2+1)+5+2
$$

b. Derive mathematical expression of rate of diffusion of a gaseous component with respect to its partial pressure difference at two different points in a two-component gas mixture for one diffusing another non-diffusing system.
2. Answer any two from the following (a) , (b) and (c)
a. Oxygen is diffusing through non-diffusing carbon monoxide under steady state condition. The total ambient pressure $10^{5} \mathrm{~N} / \mathrm{m}^{2}$ and the temperature is $0^{\circ} \mathrm{C}$. The partial pressure of oxygen at two planes 3 mm apart is 14,000 and $7000 \mathrm{~N} / \mathrm{m}^{2}$, respectively. The diffusivity for the mixture is $1.9 \times 10^{-5} \mathrm{~m}^{2} / \mathrm{sec}$. Calculate the rate of diffusion of oxygen in kmole $/ \mathrm{sec}-\mathrm{m}^{2}$.
b. Hydrochloric acid (A) concentration at the opposite walls of a static film (4. mm thick) of non diffusing water (B) are $12 \%$ and $4 \%$ (by wt.), respectively. The diffusivity of the acid in the binary mixture of water and acid is $2.5 \times 10^{-9} / \mathrm{sec}$ at $20^{\circ} \mathrm{C}$. Density of $12 \%$ and $4 \%$ acid solution are $1050 \mathrm{~kg} / \mathrm{m}^{3}$ and $1020 \mathrm{~kg} / \mathrm{m}^{3}$, respectively. Calculate the diffusion flux of the acid at $20^{\circ} \mathrm{C}$. 12.5
c. Hydrogen gas at 2 std . atm. pressure, $25^{\circ} \mathrm{Cf}$ lows through a pipe made of unvulcanized rubber, with ID and OD 25 and 50 mm , respectively. The solubility of the hydrogen is reported to be $0.053 \mathrm{~cm}^{3}(\mathrm{STP}) / \mathrm{cm}^{3}$.atm. and the diffusivity of hydrogen through the rubber to be $1.8 \times 10^{-6} \mathrm{~cm}^{2} / \mathrm{s}$. Estimate the rate of loss of hydrogen (in gms ) by diffusion per meter of pipe length per hour. 12.5
3. Answer any one from the following (a) and (b)
a. (i) Calculate the permeability coefficient of an amorphous PET film to $\mathrm{O}_{2}$ at $23^{\circ} \mathrm{C}$ given that the OTR through a $2.54 \times 10^{-3} \mathrm{~cm}$ thick film with air on one side and inert gas on the other is 8.8 x $10^{-9} \mathrm{~mL} \mathrm{~cm}^{-2} \mathrm{~s}^{-1} . \mathrm{O}_{2}$ partial pressure difference across the film is 0.21 atm
(ii) Find out the unit of permeability in SI system.
b. A carbonated beverage is packaged in a PET bottle with oxygen permeability of $0.30 \times 10^{-11}$ $\mathrm{ml}(\mathrm{STP}) . \mathrm{cm} / \mathrm{cm}^{2} . \mathrm{sec} . \mathrm{cmHg}$. The surface area of the bottle is $720 \mathrm{~cm}^{2}$ and thickness of the wall is 0.046 cm and holds 1 litre of beverage. Calculate the shelf life of the beverage in the bottle. Assume that air contains $21 \%$ oxygen and density of oxygen is $1.40 \times 10^{-3} \mathrm{gm} / \mathrm{ml}$. The maximum limit of quantity of oxygen in the beverage at its acceptable form is 5 ppm .

