

**BACHELOR OF ENGINEERING IN CHEMICAL ENGINEERING EXAMINATION, 2018**

(2nd Year, 2nd Semester)

**CHEMICAL ENGINEERING THERMODYNAMICS**

Time : Three hours

Full Marks : 100

(50 marks for each Part)

Use a separate Answer-Script for each Part

**PART I**

Answer any two questions

All the symbols have their usual meaning

Assume any missing data

|     |  | CO  |
|-----|--|-----|
| Q1. | <p>Water at 10 atm and 40 °C enters a boiler at a flow rate of 100kg/h. The stream exiting the boiler is at 10 atm and 300 °C.</p> <p>(5 + 20)</p> <p>(a) Sketch the path of P-V diagram?</p> <p>(b) Determine the rate of heat energy that needs to be supplied from the following data?</p> <p>The critical temperature, critical pressure and acentric factor of water is 647.3 K, 221.2 bar and 0.344.</p> <p>The equation for determining the molar volume of water is</p> $Z = 1 + \frac{BP}{RT}, \quad \frac{BP}{RT} = B_0 + \omega B_1$ $B_0 = 0.083 - \frac{0.422}{T_r^{1.6}}, \quad B_1 = 0.139 - \frac{0.172}{T_r^{4.2}}$ <p>The heat capacity in ideal gas state is <math>C_p^o \left( \frac{\text{J}}{\text{mol K}} \right) = 28.85 + 0.01205T^2</math></p> <p>The vapor pressure of water can be estimated from the following relation</p> $\log_{10}(\text{mm Hg}) = 7.97 - \frac{1668.21}{t(^{\circ}\text{C}) + 228} \quad (25)$ | CO1 |
| Q2. | <p>(A) The volume change of mixing of the system ethanol (1)/methyl butyl ether (2) at 25 °C is given by <math>\Delta V (\text{cm}^3/\text{mol}) = x_1 x_2 \{-1.026 + 0.22(x_1 - x_2)\}</math></p> <p>The pure species volume <math>V_1 = 110 \text{ cm}^3/\text{mol}</math> and <math>V_2 = 90 \text{ cm}^3/\text{mol}</math></p> <p>(a) 750 cm<sup>3</sup> of pure species of 1 is mixed with 1500 cm<sup>3</sup> of pure species 2 at 25 °C.</p> <p>(i) What would be the volume if an ideal solution is formed?</p> <p>(ii) Estimate the volume of the mixture is formed.</p> <p>(b) Derive the expression of <math>\bar{V}_1</math> and <math>\bar{V}_1^E</math>. (8+7)</p>   | CO2 |

|       | <p>(B) If the equation <math>\mu_1 = G_1 + RT \ln x_1</math> is a valid expression for the chemical potential in a binary liquid system at constant T and P show that <math>\mu_2 = G_2 + RT \ln x_2</math>. (5)</p> <p>(C) The following equations have been proposed to represent activity coefficient for a system at a fixed T and P</p> $\ln \gamma_1 = Ax_2^2 + Bx_2^2(3x_1 - x_2) \quad \ln \gamma_2 = Ax_1^2 + Bx_1^2(x_1 - 3x_2)$ <p>Check whether the system satisfies Gibbs Duhem equation. (5)</p>  |       |                             |       |                             |       |                             |   |        |     |         |     |         |      |         |     |         |      |         |      |         |     |        |      |         |      |         |     |         |      |         |      |         |     |         |      |         |     |         |     |         |     |        |      |         |     |        |  |  |     |
|-------|---|-------|-----------------------------|-------|-----------------------------|-------|-----------------------------|---|--------|-----|---------|-----|---------|------|---------|-----|---------|------|---------|------|---------|-----|--------|------|---------|------|---------|-----|---------|------|---------|------|---------|-----|---------|------|---------|-----|---------|-----|---------|-----|--------|------|---------|-----|--------|--|--|-----|
| Q3.   | <p>(A) The following data are available for the molar volume of liquid mixtures of cyclohexane (1) and carbon tetrachloride at 1 atm and 60 °C</p> <table border="1"> <thead> <tr> <th><math>x_1</math></th> <th><math>V</math> (cm<sup>3</sup>/gmol)</th> <th><math>x_1</math></th> <th><math>V</math> (cm<sup>3</sup>/gmol)</th> <th><math>x_1</math></th> <th><math>V</math> (cm<sup>3</sup>/gmol)</th> </tr> </thead> <tbody> <tr> <td>0</td> <td>101.46</td> <td>0.2</td> <td>104.002</td> <td>0.9</td> <td>112.481</td> </tr> <tr> <td>0.02</td> <td>101.717</td> <td>0.3</td> <td>105.253</td> <td>0.92</td> <td>112.714</td> </tr> <tr> <td>0.04</td> <td>101.973</td> <td>0.4</td> <td>106.49</td> <td>0.94</td> <td>112.946</td> </tr> <tr> <td>0.06</td> <td>102.228</td> <td>0.5</td> <td>107.715</td> <td>0.96</td> <td>113.178</td> </tr> <tr> <td>0.08</td> <td>102.483</td> <td>0.6</td> <td>108.926</td> <td>0.98</td> <td>113.409</td> </tr> <tr> <td>0.1</td> <td>102.737</td> <td>0.7</td> <td>110.125</td> <td>1.0</td> <td>113.64</td> </tr> <tr> <td>0.15</td> <td>103.371</td> <td>0.8</td> <td>111.31</td> <td></td> <td></td> </tr> </tbody> </table> <p>(a) Use the above data to determine <math>V_1, V_2, \bar{V}_1^\infty</math> and <math>\bar{V}_2^\infty</math></p> <p>(b) Determine the value of <math>\Delta V</math> from the data at <math>x_1=0.4</math>. (10 + 5)</p> <p>(B) The solution behavior of a certain class of substances is described by the equation</p> $G = \sum_i x_i \Gamma_i + RT \sum_i x_i \ln(x_i P)$ <p>where <math>\Gamma_i</math> is a function of temperature</p> <p>Derive the formulas for (a) <math>G_i</math> (b) <math>\mu_i</math> (c) <math>S_i</math> (d) <math>V_i</math> (e) <math>\bar{S}_i</math> (10)</p> | $x_1$ | $V$ (cm <sup>3</sup> /gmol) | $x_1$ | $V$ (cm <sup>3</sup> /gmol) | $x_1$ | $V$ (cm <sup>3</sup> /gmol) | 0 | 101.46 | 0.2 | 104.002 | 0.9 | 112.481 | 0.02 | 101.717 | 0.3 | 105.253 | 0.92 | 112.714 | 0.04 | 101.973 | 0.4 | 106.49 | 0.94 | 112.946 | 0.06 | 102.228 | 0.5 | 107.715 | 0.96 | 113.178 | 0.08 | 102.483 | 0.6 | 108.926 | 0.98 | 113.409 | 0.1 | 102.737 | 0.7 | 110.125 | 1.0 | 113.64 | 0.15 | 103.371 | 0.8 | 111.31 |  |  | CO3 |
| $x_1$ | $V$ (cm <sup>3</sup> /gmol)   | $x_1$ | $V$ (cm <sup>3</sup> /gmol) | $x_1$ | $V$ (cm <sup>3</sup> /gmol) |       |                             |   |        |     |         |     |         |      |         |     |         |      |         |      |         |     |        |      |         |      |         |     |         |      |         |      |         |     |         |      |         |     |         |     |         |     |        |      |         |     |        |  |  |     |
| 0     | 101.46  | 0.2   | 104.002                     | 0.9   | 112.481                     |       |                             |   |        |     |         |     |         |      |         |     |         |      |         |      |         |     |        |      |         |      |         |     |         |      |         |      |         |     |         |      |         |     |         |     |         |     |        |      |         |     |        |  |  |     |
| 0.02  | 101.717   | 0.3   | 105.253                     | 0.92  | 112.714                     |       |                             |   |        |     |         |     |         |      |         |     |         |      |         |      |         |     |        |      |         |      |         |     |         |      |         |      |         |     |         |      |         |     |         |     |         |     |        |      |         |     |        |  |  |     |
| 0.04  | 101.973   | 0.4   | 106.49                      | 0.94  | 112.946                     |       |                             |   |        |     |         |     |         |      |         |     |         |      |         |      |         |     |        |      |         |      |         |     |         |      |         |      |         |     |         |      |         |     |         |     |         |     |        |      |         |     |        |  |  |     |
| 0.06  | 102.228   | 0.5   | 107.715                     | 0.96  | 113.178                     |       |                             |   |        |     |         |     |         |      |         |     |         |      |         |      |         |     |        |      |         |      |         |     |         |      |         |      |         |     |         |      |         |     |         |     |         |     |        |      |         |     |        |  |  |     |
| 0.08  | 102.483   | 0.6   | 108.926                     | 0.98  | 113.409                     |       |                             |   |        |     |         |     |         |      |         |     |         |      |         |      |         |     |        |      |         |      |         |     |         |      |         |      |         |     |         |      |         |     |         |     |         |     |        |      |         |     |        |  |  |     |
| 0.1   | 102.737   | 0.7   | 110.125                     | 1.0   | 113.64                      |       |                             |   |        |     |         |     |         |      |         |     |         |      |         |      |         |     |        |      |         |      |         |     |         |      |         |      |         |     |         |      |         |     |         |     |         |     |        |      |         |     |        |  |  |     |
| 0.15  | 103.371   | 0.8   | 111.31                      |       |                             |       |                             |   |        |     |         |     |         |      |         |     |         |      |         |      |         |     |        |      |         |      |         |     |         |      |         |      |         |     |         |      |         |     |         |     |         |     |        |      |         |     |        |  |  |     |

## B.E. CHEMICAL ENGINEERING SECOND YEAR SECOND SEMESTER EXAM 2018

## CHEMICAL ENGINEERING THERMODYNAMICS

## PART II

**Answer any 2 (two) questions**

All symbols have their usual meanings

Assume any missing data

|           |  | CO      |        |   |   |           |         |         |        |           |         |         |        |          |
|-----------|--|---------|--------|---|---|-----------|---------|---------|--------|-----------|---------|---------|--------|----------|
| Q1(A)     | <p>1. (A) A binary liquid mixture contains equimolar amounts benzene (1) and toluene (2). The activity coefficients of the two species in liquid phase are given by one constant Margule's equations. Prove that the vapour phase equilibrium mole fraction of benzene may be described by the following equation. (8)</p> $y_1 = \frac{p_1^{sat}}{(p_1^{sat} + p_2^{sat})}$   | CO2     |        |   |   |           |         |         |        |           |         |         |        |          |
| Q1(B)     | <p>(B) A binary mixture containing 40 mol% isobutane and rest n-pentane flows continuously into a flash chamber which is maintained at a constant temperature of 49°C.</p> <p>I. determine the pressure below which the flash chamber must be maintained for the liquid mixture to flash. (5)</p> <p>II. If the flash chamber is maintained at 49°C and 3.2 bar, predict</p> <p>(a) the liquid and vapour flow rates per mole of the entering feed (7)</p> <p>(b) compositions of the liquid and vapour streams. (5)</p> <p>Assume that the liquid mixture is ideal and the K values for isobutane and n-pentane at 49°C and 3.2 bar are 2.0 and 0.5 respectively. Antoine constants for isobutane and n-pentane are given below:</p> <table border="1"> <thead> <tr> <th></th> <th>A</th> <th>B</th> <th>C</th> </tr> </thead> <tbody> <tr> <td>Isobutane</td> <td>15.5381</td> <td>2032.72</td> <td>-33.15</td> </tr> <tr> <td>n-pentane</td> <td>15.8333</td> <td>2477.07</td> <td>-39.34</td> </tr> </tbody> </table> $\ln P^{sat}(\text{mm Hg}) = A - \frac{B}{T(K) + C}$ |         | A      | B | C | Isobutane | 15.5381 | 2032.72 | -33.15 | n-pentane | 15.8333 | 2477.07 | -39.34 | CO2, CO3 |
|           | A  | B       | C      |   |   |           |         |         |        |           |         |         |        |          |
| Isobutane | 15.5381  | 2032.72 | -33.15 |   |   |           |         |         |        |           |         |         |        |          |
| n-pentane | 15.8333  | 2477.07 | -39.34 |   |   |           |         |         |        |           |         |         |        |          |

| Q2(A)  | <p>2. (A) Prove that for a gas phase reaction at low pressure, the equilibrium constants, <math>K_p</math> and <math>K_y</math> are related by the following expression (5)</p> $K_p = K_y P^{\sum \nu_i}$ <p><math>K_p</math> and <math>K_y</math> are the reaction equilibrium constants expressed in terms of species partial pressures and mole fractions and <math>\nu_i</math>'s are the stoichiometric coefficients</p>  | CO2                           |                               |                               |                                  |        |        |                                  |        |        |  |       |        |     |
|--|---|-------------------------------|-------------------------------|-------------------------------|----------------------------------|--------|--------|----------------------------------|--------|--------|--|-------|--------|-----|
| Q2(B)  | <p>(B) Calculate the pressure required for 50% dissociation of phosphorus pentachloride to phosphorous trichloride and chlorine at 250°C (8)</p> <table border="1" data-bbox="441 779 1128 926"> <thead> <tr> <th></th> <th><math>\Delta H_f^\circ</math> (kcal/mol)</th> <th><math>\Delta G_f^\circ</math> (kcal/mol)</th> </tr> </thead> <tbody> <tr> <td><math>\text{PCl}_5(\text{g})</math></td> <td>-91</td> <td>-73.2</td> </tr> <tr> <td><math>\text{PCl}_3(\text{g})</math></td> <td>-70</td> <td>-65.2</td> </tr> </tbody> </table>  |                               | $\Delta H_f^\circ$ (kcal/mol) | $\Delta G_f^\circ$ (kcal/mol) | $\text{PCl}_5(\text{g})$         | -91    | -73.2  | $\text{PCl}_3(\text{g})$         | -70    | -65.2  | CO2,CO1  |       |        |     |
|  | $\Delta H_f^\circ$ (kcal/mol)   | $\Delta G_f^\circ$ (kcal/mol) |                               |                               |                                  |        |        |                                  |        |        |  |       |        |     |
| $\text{PCl}_5(\text{g})$                             | -91   | -73.2                         |                               |                               |                                  |        |        |                                  |        |        |  |       |        |     |
| $\text{PCl}_3(\text{g})$                             | -70   | -65.2                         |                               |                               |                                  |        |        |                                  |        |        |  |       |        |     |
| Q2(C)  | <p>(C) A feed mixture containing equimolar amounts of ethylene and benzene enters a continuous alkylation reactor to form ethylbenzene. The reaction may be represented as follows:</p> $\text{C}_6\text{H}_6(\text{g}) + \text{C}_2\text{H}_4(\text{g}) \rightleftharpoons \text{C}_6\text{H}_5\text{C}_2\text{H}_5(\text{g})$ <p>The reactor is maintained at a constant temperature of 325°C. Calculate</p> <p>(i) the pressure at which the reactor must be operated to achieve an equilibrium conversion of 92.6 mol% of benzene (8)</p> <p>(ii) Amount of heat that must be removed continuously to maintain the reactor at a constant temperature of 325°C. (4)</p> <table border="1" data-bbox="441 1541 1128 1738"> <thead> <tr> <th></th> <th><math>\Delta H_f^\circ</math> (kcal/mol)</th> <th><math>\Delta G_f^\circ</math> (kcal/mol)</th> </tr> </thead> <tbody> <tr> <td><math>\text{C}_6\text{H}_6(\text{g})</math></td> <td>19.820</td> <td>30.989</td> </tr> <tr> <td><math>\text{C}_2\text{H}_4(\text{g})</math></td> <td>12.496</td> <td>16.282</td> </tr> <tr> <td><math>\text{C}_6\text{H}_5\text{C}_2\text{H}_5(\text{g})</math></td> <td>7.120</td> <td>31.208</td> </tr> </tbody> </table> |                               | $\Delta H_f^\circ$ (kcal/mol) | $\Delta G_f^\circ$ (kcal/mol) | $\text{C}_6\text{H}_6(\text{g})$ | 19.820 | 30.989 | $\text{C}_2\text{H}_4(\text{g})$ | 12.496 | 16.282 | $\text{C}_6\text{H}_5\text{C}_2\text{H}_5(\text{g})$ | 7.120 | 31.208 | CO2 |
|  | $\Delta H_f^\circ$ (kcal/mol)   | $\Delta G_f^\circ$ (kcal/mol) |                               |                               |                                  |        |        |                                  |        |        |  |       |        |     |
| $\text{C}_6\text{H}_6(\text{g})$                     | 19.820  | 30.989                        |                               |                               |                                  |        |        |                                  |        |        |  |       |        |     |
| $\text{C}_2\text{H}_4(\text{g})$                     | 12.496  | 16.282                        |                               |                               |                                  |        |        |                                  |        |        |  |       |        |     |
| $\text{C}_6\text{H}_5\text{C}_2\text{H}_5(\text{g})$ | 7.120   | 31.208                        |                               |                               |                                  |        |        |                                  |        |        |  |       |        |     |

|       |  |     |
|-------|--|-----|
|       |  |     |
| Q3(C) | <p>(C) Calculate the fugacity of water at 40°C and 80 bar pressure. Vapour pressure and saturated molar volume of water at 50°C are 7.384kPa and <math>18.018 \times 10^{-3} \text{ m}^3/\text{kmol}</math> respectively. List your assumptions. (7)</p>   | CO3 |
| Q3(D) | <p>(D) Estimate the fugacity of methane in an equimolar mixture of nitrogen (1) and methane(2) at -70°C and 20 bar. Experimental values of virial coefficients are given below: (5)</p> <p><math>B_{11} = -35.2</math>    <math>B_{22} = -105.0</math>    <math>B_{12} = -59.8 \text{ cm}^3/\text{mol}</math></p> $\ln \phi_1 = \frac{P}{RT} (B_{11} + y_2^2 \delta_{12}) \qquad \ln \phi_2 = \frac{P}{RT} (B_{22} + y_1^2 \delta_{12})$ $\delta_{12} = 2B_{12} - B_{11} - B_{22}$ | CO3 |