

Name of the Examinations: B. PHARMACEUTICAL TECHNOLOGY THIRD YEAR
SECOND SEMESTER - 2017

Subject : PHARMACEUTICAL ENGINEERING -I Time: Three hours Full Marks:100

Answer any five questions taking at least two questions from each group.)

Group A

1(a) A continuous vacuum crystallizer is fed with a 31% $MgSO_4$ (M.W. 120.5)solution. The equilibrium temperature of magma in the crystallizer is 86°F. A product magma containing 5tons of $MgSO_4 \cdot 7H_2O$ (crystal) is obtained. The mass ratio of crystal to mother liquor is 0.224(M_c/M_L). Concentration of mother liquor is 28.5%. Determine the Feed Rate (MF) and the Rate of Evaporation (M_v)? Determine enthalpy of slurry (h_T)?

Enthalpy of vapor= 1098 BTU/lb ; Enthalpy of mother liquor (h_L)= - 43 BTU/lb ;Enthalpy of Crystal(h_C)= - 149 BTU/lb. Solve Graphically. Use mm graph paper.

(b) Describe Draft tube baffle crystallizer with (i) principle of operation , (ii) its construction, (iii) working procedure alongwith functions of each component part ,(iv) advantages and disadvantages, (v) a neat sketch. Marks 12+8

Q2.(i)Discuss on various types of 'turbine' impellers with specifications and neat sketch, and show the flow patterns of liquid in the vessel during agitation .(ii)What is vortex and how can it be prevented ? (iii) Write on calculation of power requirement in a liquid mixing tank for both unbaffled and baffled tank?

(b) Write short notes on pony mixer and ribbon blender. How do you assess uniformity of mixing of paste and mixing of solid powder. Marks (8+3+3)+(2+2+2)

Q3.(a) Derive heat transfer equations for (i) heat flow through 'flat metallic slabs in series' and (ii) heat flow through a cylindrical tube wall.

(b) Describe the construction, operation of 2-4 passes heat exchanger and write its advantages over 1-2 passes heat exchanger .Draw a neat diagram 2-4 passes heat exchanger with label. Marks (4+6)+10

B. PHARMACEUTICAL TECHNOLOGY THIRD YEAR SECOND SEMESTER -2017

PHARMACEUTICAL ENGINEERING-II

TIME: 3 h

FULL MARKS: 100

ANSWER ANY FIVE QUESTIONS TAKING ATLEAST TWO FROM EACH GROUP

GROUP-B

(Use graph paper if required)

4. A 6% aqueous solution of a high molecular weight solute has to be concentrated to 35% in a forward-feed double effect evaporator at the rate of 8000 kg.h^{-1} . The feed temperature is 40°C . Saturated steam at 4.5 kg.cm^{-2} is available for heating. A vacuum of 600 mm Hg is maintained in the second effect. Calculate the area requirements, if calandria of equal area are used. The overall heat transfer coefficients are 650 and $470 \text{ kcal.h}^{-1}\text{m}^{-2}{}^\circ\text{C}^{-1}$ in the first and the last effect respectively. The specific heat of the concentrated liquor is $0.84 \text{ kcal.kg}^{-1}{}^\circ\text{C}^{-1}$. [20 marks]

5

- a. A material is crushed in a Blake jaw crusher such that the average size of particle is reduced from 50 mm to 10 mm with the consumption of energy of 13.0 kW/(kg/s) . What would be the consumption of energy needed to crush the same material of average size 75 mm to an average size of 25 mm:
- assuming Rittinger's law applies?
 - assuming Kick's law applies?

Which of these results would be regarded as being more reliable and why?

- b. The screen analysis shown in the table-1 below, applies to a sample of crushed quartz. The density of the particle is 3000 kg/m^3 , and the shape factor are $a=1.5$, and $\Phi_s=0.6$. for the material between 4-mesh and 200 mesh in particle size, calculate a) A_w , and N_w
 b) $\overline{D_v}$ c) $\overline{D_s}$ d) $\overline{D_w}$ e) \overline{N} , for the 150/200 mesh increment. f) What fraction of the total number of particles is in the 150/200-mesh increment?

A quartz mixture having the screen analysis shown in the table-2 below is screened through a standard 10-mesh screen. The cumulative screen analysis of the overflow and underflow are also provided. Calculate the mass ratios of the overflow and underflow to feed and the overall effectiveness of the screen.

[5+8+7=20 marks]

6

- a. An evaporator is used to concentrate 5000 kg/h of a 15% solution of NaOH in water entering at 65°C to a product of 55% solids. The pressure of the saturated steam used is 25 psia and the pressure in the vapour space of the evaporator is 12 kPa. The overall heat transfer coefficient is $1600 \text{ W/m}^2 \cdot \text{K}$. Calculate the steam used, the steam economy in kg vaporized/kg steam used, and the heating surface area in km^2 .
- b. Design a liquid-liquid gravity separator which can handle a two phase liquid stream of $0.5 \text{ m}^3/\text{min}$. The feed contains 45% by volume of light phase and 55% by volume of a heavy phase. Densities of light (ρ_l) and heavy phase (ρ_h) are 900 and 1150 kg/m^3 respectively. Required settling time of light phase is 5 min while the settling time for heavy phase is 4 min.

[10+10=20 marks]

7.

- a. Answer any three

Explain the advantages and disadvantages of the following:

- a. Cyclone Separator
- b. Wet Scrubbers
- c. Moving bar Grizzly
- d. Electrostatic Precipitators

- b. Estimate the cut diameter and overall collection efficiency of a cyclone given the particle size distribution of dust from cement kiln. Particle size distribution and other pertinent data are given below:

Average particle size in range dp, μm	1	5	10	20	30	40	50	60	>60
Wt. percent	03	20	15	20	16	10	06	03	07

Given: Gas viscosity = 0.02 Cp; Specific Gravity of the particle = 3.0, Inlet gas velocity of cyclone = 48 ft/sec, Effective number of turns within cyclone = 5, Cyclone diameter = 8 ft, Cyclone inlet width = 2 ft, $\rho_p - \rho = 187.2 \text{ lb/ft}^3$ [4x3=12 +8 =20 marks]

Supplementary Data

Table-1

Mesh	Screen opening D_p , mm	Mass fraction retained, x_i	Average particle diameter in increment, \bar{D}_p , mm	Cumulative fraction smaller than D_p
4	4.699	0.0000	—	1.0000
6	3.327	0.0251	4.013	0.9749
8	2.362	0.1250	2.845	0.8499
10	1.651	0.3207	2.007	0.5292
14	1.168	0.2570	1.409	0.2722
20	0.833	0.1590	1.001	0.1132
28	0.589	0.0538	0.711	0.0594
35	0.417	0.0210	0.503	0.0384
48	0.295	0.0102	0.356	0.0282
65	0.208	0.0077	0.252	0.0205
100	0.147	0.0058	0.178	0.0147
150	0.104	0.0041	0.126	0.0106
200	0.074	0.0031	0.089	0.0075
Pan	—	0.0075	0.037	0.0000

Table-2

Mesh	D_p , mm	Cumulative fraction smaller than D_p		
		Feed	Overflow	Underflow
4	4.699	0	0	
6	3.327	0.025	0.071	
8	2.362	0.15	0.43	0
10	1.651	0.47	0.85	0.195
14	1.168	0.73	0.97	0.58
20	0.833	0.885	0.99	0.83
28	0.589	0.94	1.00	0.91
35	0.417	0.96		0.94
65	0.208	0.98		0.975
Pan	—	1.00		1.00

Table 3 Saturated Temperature Table for Steam in SI Units

T	P _{sat}	T ₁	T ₂	T ₃	T ₄	T ₅	T ₆	T ₇	T ₈	T ₉	T ₁₀	T ₁₁	T ₁₂	T ₁₃	T ₁₄	T ₁₅
C	kPa	°C	°C	°C	°C	°C	°C									
0	0.6119	0.0006995	205.94	205.93	205.92	205.91	205.90	205.89	205.88	205.87	205.86	205.85	205.84	205.83	205.82	205.81
1	0.7096	0.0006995	179.63	179.63	179.63	179.63	179.63	179.63	179.63	179.63	179.63	179.63	179.63	179.63	179.63	179.63
4	0.8149	0.0006996	157.04	157.04	157.04	157.04	157.04	157.04	157.04	157.04	157.04	157.04	157.04	157.04	157.04	157.04
6	0.9357	0.0006996	137.59	137.59	137.59	137.59	137.59	137.59	137.59	137.59	137.59	137.59	137.59	137.59	137.59	137.59
3	1.0732	0.0006997	120.82	120.82	120.82	120.82	120.82	120.82	120.82	120.82	120.82	120.82	120.82	120.82	120.82	120.82
10	1.2282	0.0006997	106.31	106.31	106.31	106.31	106.31	106.31	106.31	106.31	106.31	106.31	106.31	106.31	106.31	106.31
12	1.4026	0.0006998	93.74	93.74	93.74	93.74	93.74	93.74	93.74	93.74	93.74	93.74	93.74	93.74	93.74	93.74
14	1.5985	0.0006999	82.33	82.33	82.33	82.33	82.33	82.33	82.33	82.33	82.33	82.33	82.33	82.33	82.33	82.33
16	1.8180	0.0006999	73.33	73.33	73.33	73.33	73.33	73.33	73.33	73.33	73.33	73.33	73.33	73.33	73.33	73.33
18	2.0635	0.0006999	65.04	65.04	65.04	65.04	65.04	65.04	65.04	65.04	65.04	65.04	65.04	65.04	65.04	65.04
20	2.3326	0.0006999	57.30	57.30	57.30	57.30	57.30	57.30	57.30	57.30	57.30	57.30	57.30	57.30	57.30	57.30
22	2.6431	0.0006999	51.47	51.47	51.47	51.47	51.47	51.47	51.47	51.47	51.47	51.47	51.47	51.47	51.47	51.47
24	2.9830	0.0006992	45.90	45.90	45.90	45.90	45.90	45.90	45.90	45.90	45.90	45.90	45.90	45.90	45.90	45.90
26	3.3464	0.0006992	41.02	41.02	41.02	41.02	41.02	41.02	41.02	41.02	41.02	41.02	41.02	41.02	41.02	41.02
28	3.7789	0.0006993	36.72	36.72	36.72	36.72	36.72	36.72	36.72	36.72	36.72	36.72	36.72	36.72	36.72	36.72
30	4.2420	0.0006994	32.92	32.92	32.92	32.92	32.92	32.92	32.92	32.92	32.92	32.92	32.92	32.92	32.92	32.92
32	4.7536	0.0006995	29.57	29.57	29.57	29.57	29.57	29.57	29.57	29.57	29.57	29.57	29.57	29.57	29.57	29.57
34	5.3181	0.0006995	26.60	26.60	26.60	26.60	26.60	26.60	26.60	26.60	26.60	26.60	26.60	26.60	26.60	26.60
36	5.9998	0.0006996	23.96	23.96	23.96	23.96	23.96	23.96	23.96	23.96	23.96	23.96	23.96	23.96	23.96	23.96
38	6.6235	0.0006997	21.62	21.62	21.62	21.62	21.62	21.62	21.62	21.62	21.62	21.62	21.62	21.62	21.62	21.62
40	7.3743	0.0006998	19.54	19.54	19.54	19.54	19.54	19.54	19.54	19.54	19.54	19.54	19.54	19.54	19.54	19.54
42	8.1975	0.0006998	17.69	17.69	17.69	17.69	17.69	17.69	17.69	17.69	17.69	17.69	17.69	17.69	17.69	17.69
44	9.0987	0.0006999	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04
46	10.084	0.0006999	14.56	14.56	14.56	14.56	14.56	14.56	14.56	14.56	14.56	14.56	14.56	14.56	14.56	14.56
48	11.1160	0.0006999	13.23	13.23	13.23	13.23	13.23	13.23	13.23	13.23	13.23	13.23	13.23	13.23	13.23	13.23
50	12.3333	0.0006999	12.05	12.05	12.05	12.05	12.05	12.05	12.05	12.05	12.05	12.05	12.05	12.05	12.05	12.05
52	13.6100	0.0006999	10.98	10.98	10.98	10.98	10.98	10.98	10.98	10.98	10.98	10.98	10.98	10.98	10.98	10.98

T C	P _{ext} kPa	v ₁ m ³ /kg	v ₂ m ³ /kg	b ₁ m ³ /kg	b ₂ m ³ /kg	w ₁ kJ/kg	w ₂ kJ/kg	s ₁ kJ/kg	s ₂ kJ/kg	h ₁ kJ/kg	h ₂ kJ/kg	u ₁ kJ/kg	u ₂ kJ/kg	v _{g1} m ³ /kg	v _{g2} m ³ /kg	L _f kJ/kg	L _v kJ/kg	L _{f+g} kJ/kg	L _{v+g} kJ/kg	s _{fg} kJ/kg K
54	14.660	0.001014	10.02	251.848	2599.36	2373.51	225.833	2465.04	2023.31	0.7543	0.0091	7.2547								
56	16.507	0.001015	9.159	9.158	234.032	2692.85	234.035	234.185	2451.96	2217.3	0.7798	7.9757	7.1959							
58	18.143	0.001016	8.381	8.380	242.558	2695.34	2365.78	242.540	2454.27	2211.75	0.8851	7.9428	7.1377							
60	19.916	0.001017	7.679	7.678	249.918	2695.80	2358.80	250.898	2456.87	2205.97	0.8302	7.9104	7.0802							
62	21.834	0.001018	7.044	7.043	259.281	2613.26	2153.98	259.259	2459.46	2209.20	0.8552	7.8786	7.0234							
64	23.904	0.001019	6.476	6.469	267.647	2616.70	2349.05	267.623	2462.04	2164.41	0.8801	7.8472	6.9671							
66	26.144	0.001020	5.949	5.948	276.016	2620.13	2344.11	275.890	2464.61	2188.82	0.9048	7.8163	6.9115							
68	28.557	0.001021	5.476	5.475	284.389	2623.54	2339.15	284.360	2467.16	2182.80	0.9294	7.7859	6.8564							
70	31.156	0.001023	5.047	5.046	292.765	2626.64	2334.18	292.733	2469.71	2176.97	0.9519	7.7559	6.8020							
72	33.952	0.001024	4.656	4.655	301.144	2630.32	2329.18	301.109	2472.24	2171.13	0.9782	7.7263	6.7481							
74	36.957	0.001025	4.300	4.299	309.527	2633.69	2324.16	309.489	2474.76	2165.27	1.0024	7.6972	6.6943							
76	40.184	0.001026	3.976	3.975	317.913	2637.04	2319.13	317.872	2477.27	2159.40	1.0265	7.6686	6.6421							
78	43.645	0.001028	3.680	3.679	326.303	2640.37	2314.07	326.253	2479.76	2153.51	1.0555	7.6403	6.5898							
80	47.353	0.001029	3.409	3.408	334.696	2643.60	2308.99	334.648	2482.35	2147.60	1.0743	7.6125	6.5382							
82	51.322	0.001030	3.162	3.161	345.083	2646.99	2303.90	345.040	2484.72	2141.68	1.0980	7.5850	6.4870							
84	55.567	0.001032	2.935	2.934	351.494	2650.27	2298.78	351.457	2487.17	2135.74	1.1216	7.5570	6.4564							
86	60.102	0.001033	2.727	2.726	359.899	2653.53	2293.64	359.857	2499.62	2129.73	1.1450	7.5313	6.3862							
88	64.942	0.001034	2.537	2.536	368.303	2656.78	2288.47	368.240	2492.04	2123.80	1.1684	7.5050	6.3346							
90	70.104	0.001036	2.361	1.360	376.710	2660.01	2283.39	376.648	2494.46	2117.91	1.1916	7.4790	6.2874							
92	75.603	0.001037	2.200	2.199	385.137	2663.21	2278.03	385.059	2496.86	2111.80	1.2147	7.4534	6.2387							
94	81.457	0.001039	2.052	2.051	393.558	2666.40	2272.24	393.474	2499.25	2105.77	1.2377	7.4203	6.1905							
96	87.683	0.001040	1.915	1.914	401.981	2669.57	2267.58	401.893	2501.62	2099.73	1.2685	7.4033	6.1427							
98	94.269	0.001041	1.782	1.782	410.414	2672.72	2262.36	410.316	2503.98	2093.66	1.2813	7.3767	6.0954							
100	101.325	0.001043	1.673	1.672	418.949	2675.84	2255.99	418.743	2506.32	2087.57	1.3060	7.3545	6.0485							
102	108.778	0.001045	1.566	1.565	427.280	2678.95	2251.66	427.175	2508.64	2081.47	1.3265	7.3305	6.0020							
104	116.678	0.001046	1.466	1.465	435.113	2682.03	2246.30	435.611	2510.95	2075.34	1.3510	7.3076	5.9560							
106	125.047	0.001048	1.374	1.373	444.033	2685.09	2240.91	444.052	2513.75	2069.19	1.3733	7.2837	5.9103							
108	133.905	0.001050	1.289	1.288	452.638	2688.13	2235.49	452.498	2515.52	2063.03	1.3955	7.2606	5.8651							
110	143.273	0.001051	1.210	1.209	461.369	2691.14	2230.64	460.948	2517.78	2056.83	1.4177	7.2379	5.8203							

T	P _m	v _f	v _s	v _d	v _t	v _g	v _b	v _a	v _c	v _e	v _k	v _h	v _l	v _i	v _j	
C	M ₂	M ₃	M ₄	M ₅	M ₆	M ₇	M ₈	M ₉	M ₁₀	M ₁₁	M ₁₂	M ₁₃	M ₁₄	M ₁₅	M ₁₆	M ₁₇
112	1.53.173	0.001053	1.137	1.136	469.565	2694.13	2224.57	460.004	2520.93	2050.69	1.4397	7.7155	5.7758	1.10	361.962	0.00009
114	1.63.238	0.001055	1.089	1.088	478.038	2697.10	2219.98	4477.865	2525.25	2044.38	1.4616	7.1933	5.7318	128	254.377	0.00009
116	1.74.662	0.001057	1.005	1.004	466.516	2700.04	2211.52	480.312	2524.46	2038.12	1.4834	7.1715	5.6830	126	219.354	0.00007
118	1.86.297	0.001058	0.998	0.998	482.219	2705.84	2202.15	501.282	2528.81	2035.53	1.4679	7.1285	5.6117	124	225.682	0.00007
120	1.98.559	0.001059	0.997118	0.997118	546.058	2719.86	2173.80	545.769	2539.34	1993.57	1.6314	7.0254	5.5168	122	211.472	0.00007
122	2.08.520	0.001062	0.996991	0.996991	554.595	2721.57	2167.98	554.287	2541.38	1987.09	1.6543	7.0659	5.4749	120	199.334	0.00007
124	2.25.682	0.001064	0.996183	0.996183	562.140	2726.95	2187.95	494.804	2526.64	2031.84	1.5051	6.9857	5.3103	126	197.783	0.00007
126	2.42.738	0.001065	0.996219	0.996219	569.09	2730.94	2207.95	501.282	2528.81	2035.53	1.5351	6.9554	5.2698	124	191.864	0.00007
128	2.59.859	0.001066	0.996333	0.996333	577.530	2737.70	2199.71	2179.58	2537.538	2039.02	1.5199	6.9299	5.1998	122	188.411	0.00007
130	2.70.156	0.001067	0.996456	0.996456	586.495	2741.53	2191.04	501.282	2539.34	2031.25	1.5054	6.8954	5.1510	120	186.277	0.00007
132	2.86.720	0.001068	0.996579	0.996579	595.401	2747.90	2197.90	501.282	2541.38	2035.53	1.5211	6.8663	5.1113	124	184.186	0.00007
134	3.04.987	0.001069	0.996702	0.996702	604.313	2754.34	2207.95	494.804	2536.64	2031.84	1.5051	6.83718	5.0723	126	182.110	0.00007
136	3.22.317	0.001070	0.996823	0.996823	613.225	2760.94	2219.98	480.312	2541.38	2035.53	1.5211	6.8084	5.0336	124	180.022	0.00007
138	3.41.498	0.001072	0.996949	0.996949	622.138	2767.52	2220.95	501.282	2547.36	2035.53	1.5211	6.7819	4.9958	126	178.110	0.00007
140	361.962	0.00009	0.508559	0.508559	630.046	2773.10	2144.27	508.438	2549.31	1957.47	1.7171	6.9468	5.1298	122	169.000	0.00007
142	502.973	0.00009	0.509414	0.509414	640.477	2787.34	2167.36	510.928	2553.09	1962.83	1.6597	7.0865	5.0723	120	167.900	0.00007
144	537.644	0.00009	0.509544	0.509544	648.547	2792.17	2187.95	510.928	2553.09	1962.72	1.6366	6.9796	4.9190	122	165.800	0.00007
146	471.186	0.000096	0.454672	0.454672	652.170	2801.10	1934.10	1.8199	6.8515	1.8000	1.9206	6.7665	4.8438	120	163.700	0.00007
148	451.022	0.000098	0.338120	0.338120	656.783	2805.53	1934.10	1.8199	6.8515	1.8000	1.9206	6.7471	4.8066	122	161.600	0.00007
150	428.000	0.000099	0.338121	0.338121	661.322	2813.51	1934.10	1.8199	6.8515	1.8000	1.9206	6.7338	4.7690	120	158.500	0.00007
152	392.973	0.000099	0.338125	0.338125	669.928	2820.95	1940.95	1.8199	6.8515	1.8000	1.9206	6.7136	4.7338	122	156.400	0.00007
154	359.277	0.000099	0.338126	0.338126	677.783	2826.53	1940.95	1.8199	6.8515	1.8000	1.9206	6.6866	4.6962	120	154.300	0.00007
156	327.644	0.000099	0.338127	0.338127	685.783	2832.44	1940.95	1.8199	6.8515	1.8000	1.9206	6.6575	4.6674	122	152.200	0.00007
158	287.722	0.000099	0.338129	0.338129	692.546	2838.23	1940.95	1.8199	6.8515	1.8000	1.9206	6.6285	4.6386	120	150.100	0.00007
160	218.016	0.000099	0.338130	0.338130	701.271	2761.22	2061.95	700.474	2572.03	1871.56	1.9466	6.5996	4.6094	122	145.900	0.00007
162	650.092	0.000105	0.292519	0.292519	709.171	2765.34	2055.53	700.474	2572.03	1871.56	1.9466	6.5700	4.5700	120	143.800	0.00007
164	633.477	0.000107	0.278985	0.278985	716.090	2770.47	1878.68	1.9391	6.5692	1.9391	6.5692	4.5338	122	141.700	0.00007	
166	718.210	0.001110	0.266195	0.266195	723.010	2775.34	2055.53	700.474	2572.03	1871.56	1.9466	6.5596	4.5596	120	139.100	0.00007
168	754.328	0.001112	0.254102	0.254102	730.910	2775.34	2055.53	700.474	2572.03	1871.56	1.9466	6.5596	4.5596	122	137.000	0.00007

T	P _c	V _t	V _r	V _b	I _b	I _t													
C	LP _c	mJ ₂ /g																	
218	2694.01	0.0001204	0.074220	0.073025	0.980750	2891.50	1820.75	977.00	2891.50	1820.75	977.00	2891.50	1820.75	977.00	2891.50	1820.75	977.00	2891.50	1820.75
230	2795.02	0.0001203	0.071555	0.070534	0.990111	2891.30	1811.67	986.75	2891.30	1811.67	986.75	2891.30	1811.67	986.75	2891.30	1811.67	986.75	2891.30	1811.67
232	2898.94	0.0001212	0.068891	0.067777	0.999519	2892.03	1802.49	996.00	2892.03	1802.49	996.00	2892.03	1802.49	996.00	2892.03	1802.49	996.00	2892.03	1802.49
234	3005.81	0.0001216	0.066652	0.065316	100030	2892.19	1793.22	1005.32	2892.19	1793.22	1005.32	2892.19	1793.22	1005.32	2892.19	1793.22	1005.32	2892.19	1793.22
236	3115.9	0.0001214	0.064396	0.063039	1005.30	2892.30	1791.82	1001.62	2892.30	1791.82	1001.62	2892.30	1791.82	1001.62	2892.30	1791.82	1001.62	2892.30	1791.82
248	3441.61	0.0001246	0.051878	0.049612	1075.80	2892.11	1755.10	1042.75	2892.11	1755.10	1042.75	2892.11	1755.10	1042.75	2892.11	1755.10	1042.75	2892.11	1755.10
250	3594.26	0.0001246	0.051878	0.049612	1075.80	2892.11	1755.10	1042.75	2892.11	1755.10	1042.75	2892.11	1755.10	1042.75	2892.11	1755.10	1042.75	2892.11	1755.10
252	4110.40	0.0001256	0.048391	0.047135	1095.30	2892.30	1798.02	1055.43	2892.30	1798.02	1055.43	2892.30	1798.02	1055.43	2892.30	1798.02	1055.43	2892.30	1798.02
254	4250.11	0.0001256	0.048391	0.047135	1095.30	2892.30	1798.02	1055.43	2892.30	1798.02	1055.43	2892.30	1798.02	1055.43	2892.30	1798.02	1055.43	2892.30	1798.02
256	4393.44	0.0001265	0.045164	0.043959	1114.35	2892.30	1798.98	1085.58	2892.30	1798.98	1085.58	2892.30	1798.98	1085.58	2892.30	1798.98	1085.58	2892.30	1798.98
258	4540.47	0.0001270	0.045377	0.043959	1124.69	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32
260	4681.25	0.0001274	0.045377	0.043959	1124.69	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32
262	4835.82	0.0001281	0.045380	0.043960	1124.69	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32
264	5004.33	0.0001286	0.045380	0.043960	1124.69	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32
266	5166.78	0.0001291	0.045380	0.043960	1124.69	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32
268	5332.25	0.0001297	0.045380	0.043960	1124.69	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32
270	5500.71	0.0001303	0.045380	0.043960	1124.69	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32
272	5678.56	0.0001309	0.045380	0.043960	1124.69	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32
274	5857.53	0.0001315	0.045380	0.043960	1124.69	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32
276	6040.58	0.0001321	0.045380	0.043960	1124.69	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32
278	6222.47	0.0001327	0.045380	0.043960	1124.69	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32
280	6420.58	0.0001333	0.045380	0.043960	1124.69	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32
282	6617.23	0.0001340	0.045380	0.043960	1124.69	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32
284	6818.48	0.0001346	0.045380	0.043960	1124.69	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32	1074.34	2892.30	1799.32

T C	P _{ext} MPa	v _t m ³ /kg	v _s m ³ /kg	v _g m ³ /kg	b _t m ³ /kg	b _s m ³ /kg	b _g m ³ /kg	w _t kg/kg	w _s kg/kg	w _g kg/kg	u _t kJ/kg	u _s kJ/kg	u _g kJ/kg	s _t kJ/kg K	s _s kJ/kg K	s _g kJ/kg K
285	7024.42	0.001353	0.027188	0.015935	1266.85	2782.75	1515.87	1257.88	2591.07	1333.69	3.0855	5.8125	2.7170			
288	7235.11	0.001360	0.026482	0.025042	1277.42	2781.06	1501.64	1267.38	2590.03	1322.46	3.1136	5.7977	2.6852			
290	7450.65	0.001367	0.025595	0.024178	1288.01	2779.29	1491.27	1277.83	2588.96	1311.11	3.1296	5.7810	2.6553			
291	7671.10	0.001374	0.024717	0.023343	1298.67	2777.44	1478.77	1298.13	2587.83	1299.71	3.1466	5.7681	2.6215			
294	7896.54	0.001382	0.023917	0.022515	1309.39	2775.53	1466.14	1298.48	2586.67	1288.19	3.1635	5.7532	2.5886			
296	8127.07	0.001389	0.023142	0.021753	1320.18	2773.54	1453.38	1308.89	2585.46	1276.57	3.1804	5.7382	2.5578			
298	8343.76	0.001397	0.022363	0.020996	1331.03	2771.47	1440.44	1310.35	2584.20	1264.85	3.1972	5.7231	2.5258			
300	8560.49	0.001405	0.021659	0.019263	1341.95	2769.34	1427.38	1129.87	2582.91	1253.04	3.2139	5.7079	2.4946			
302	8778.96	0.001413	0.020867	0.018554	1352.96	2767.13	1414.16	1340.45	2581.57	1241.11	3.2336	5.6927	2.4621			
304	9010.61	0.001421	0.020288	0.018867	1364.04	2764.84	1400.90	1351.10	2580.18	1229.08	3.2472	5.6773	2.4302			
306	9255.81	0.001430	0.019631	0.018201	1375.19	2762.48	1387.20	1361.81	2578.76	1216.95	3.2636	5.6619	2.3982			
308	9521.58	0.001439	0.018695	0.017556	1386.43	2759.05	1373.02	1373.02	2577.29	1204.70	3.2836	5.6463	2.3664			
310	9830.03	0.001448	0.018379	0.016931	1397.76	2757.54	1359.76	1382.44	2575.77	1192.34	3.2957	5.6307	2.3345			
312	10161.24	0.001457	0.017782	0.016325	1409.17	2754.96	1345.20	1394.36	2574.22	1179.86	3.3123	5.6150	2.3037			
314	10444.32	0.001466	0.017203	0.015737	1420.68	2752.30	1331.62	1405.36	2572.62	1167.26	3.3222	5.5991	2.2769			
316	10730.34	0.001476	0.016643	0.015157	1432.28	2749.56	1217.22	1416.44	2570.98	1154.54	3.3430	5.5832	2.2393			
318	11022.41	0.001485	0.016100	0.014614	1443.98	2746.75	1302.77	1427.61	2569.30	1141.69	3.3594	5.5671	2.2077			
320	11320.63	0.001495	0.015573	0.014078	1455.79	2743.87	1288.06	1438.66	2567.57	1122.71	3.3746	5.5510	2.1764			
322	11625.08	0.001506	0.015063	0.013537	1467.71	2740.91	1271.20	1450.10	2565.80	1115.60	3.3805	5.5347	2.1452			
324	11915.86	0.001517	0.014563	0.013632	1479.74	2737.87	1258.13	1401.04	2563.99	1102.35	3.4041	5.4983	2.1142			
326	12251.07	0.001527	0.014088	0.012561	1491.88	2734.76	1141.87	1473.17	2562.13	1088.96	3.4112	5.5018	2.0336			
328	12576.82	0.001538	0.013623	0.012684	1504.15	2731.57	1127.41	1484.11	2560.24	1075.43	3.4318	5.4851	2.0313			
330	12987.21	0.001550	0.013171	0.011622	1516.55	2728.30	1111.75	1496.55	2558.29	1061.74	3.4448	5.4684	2.0235			
332	13324.13	0.001563	0.011172	0.011172	1529.09	2724.96	1105.87	1508.41	2556.31	1047.90	3.4571	5.4515	1.9844			
340	14462.79	0.001611	0.011168	0.009457	1580.67	2710.81	1110.44	1557.05	2547.41	980.89	3.4953	5.3825	1.8372			
342	15034.68	0.001624	0.010731	0.009107	1583.96	2717.03	1113.11	1565.55	2545.74	976.19	3.5006	5.3669	1.8841			

T	P _{ad}	v _f	v _s	v _b	b _f	b _s	b _b	e _f	e _s	e _b	x _f	x _s	x _b
C	MPa	m ³ /kg	m ³ /kg	m ³ /kg	L/kg	L/kg	L/kg	L/kg	L/kg	L/kg	kJ/kg K	kJ/kg K	kJ/kg K
344	15414.47	0.001637	0.010365	0.008728	1697.42	2703.26	1695.84	1522.19	2543.50	961.31	3.5040	5.3472	1.8433
345	15801.74	0.001651	0.010309	0.008359	1621.07	2629.38	1678.31	1594.98	2541.21	946.23	3.5040	5.3294	1.8254
348	16195.63	0.001665	0.009664	0.008000	1634.90	2695.41	1640.51	1607.93	2538.88	930.94	3.5002	5.3114	1.8111
350	16509.25	0.001679	0.009330	0.007450	1648.92	2691.36	1642.44	1621.05	2536.50	915.45	3.4915	5.2932	1.8017
352	17009.71	0.001694	0.009004	0.006711	1663.15	2687.34	1624.08	1634.34	2534.07	899.73	3.4764	5.2749	1.7985
354	17428.13	0.001709	0.008689	0.006580	1677.60	2683.03	1665.43	1647.81	2531.60	883.79	3.4578	5.2565	1.7816
356	17854.64	0.001724	0.008382	0.006358	1692.26	2678.75	988.48	1661.47	2529.09	877.61	3.4479	5.2378	1.8199
358	18289.36	0.001740	0.008084	0.006144	1707.16	2674.32	967.72	1675.33	2526.52	851.19	3.4376	5.2191	1.8315
360	18732.41	0.001756	0.007775	0.005919	1722.10	2669.94	947.64	1689.40	2523.91	834.51	3.2954	5.2002	1.9047
362	19183.91	0.001773	0.007514	0.005741	1737.69	2665.41	927.72	1703.68	2521.26	817.57	3.1918	5.1811	1.9893
364	19644.09	0.001790	0.007242	0.005452	1753.35	2660.81	907.45	1718.19	2518.55	800.36	3.0469	5.1619	2.1210
366	20112.81	0.001807	0.006977	0.005170	1769.28	2656.12	886.94	1732.93	2515.79	782.86	2.8150	5.1425	2.3276
368	20590.46	0.001825	0.006695	0.004995	1785.50	2651.35	866.35	1747.93	2512.99	765.06	2.4610	5.1230	2.6620
370	21077.08	0.001843	0.006470	0.004777	1802.03	2646.50	844.48	1763.17	2510.13	746.95	1.8582	5.1033	3.2451
372	21572.82	0.001862	0.006228	0.004528	1818.26	2641.57	822.71	1778.69	2507.22	724.53	0.5970	5.0835	4.4864
374	22077.81	0.001881	0.005993	0.004311	1836.02	2636.56	800.54	1794.49	2504.26	702.77	-19.7443	5.0635	24.8077

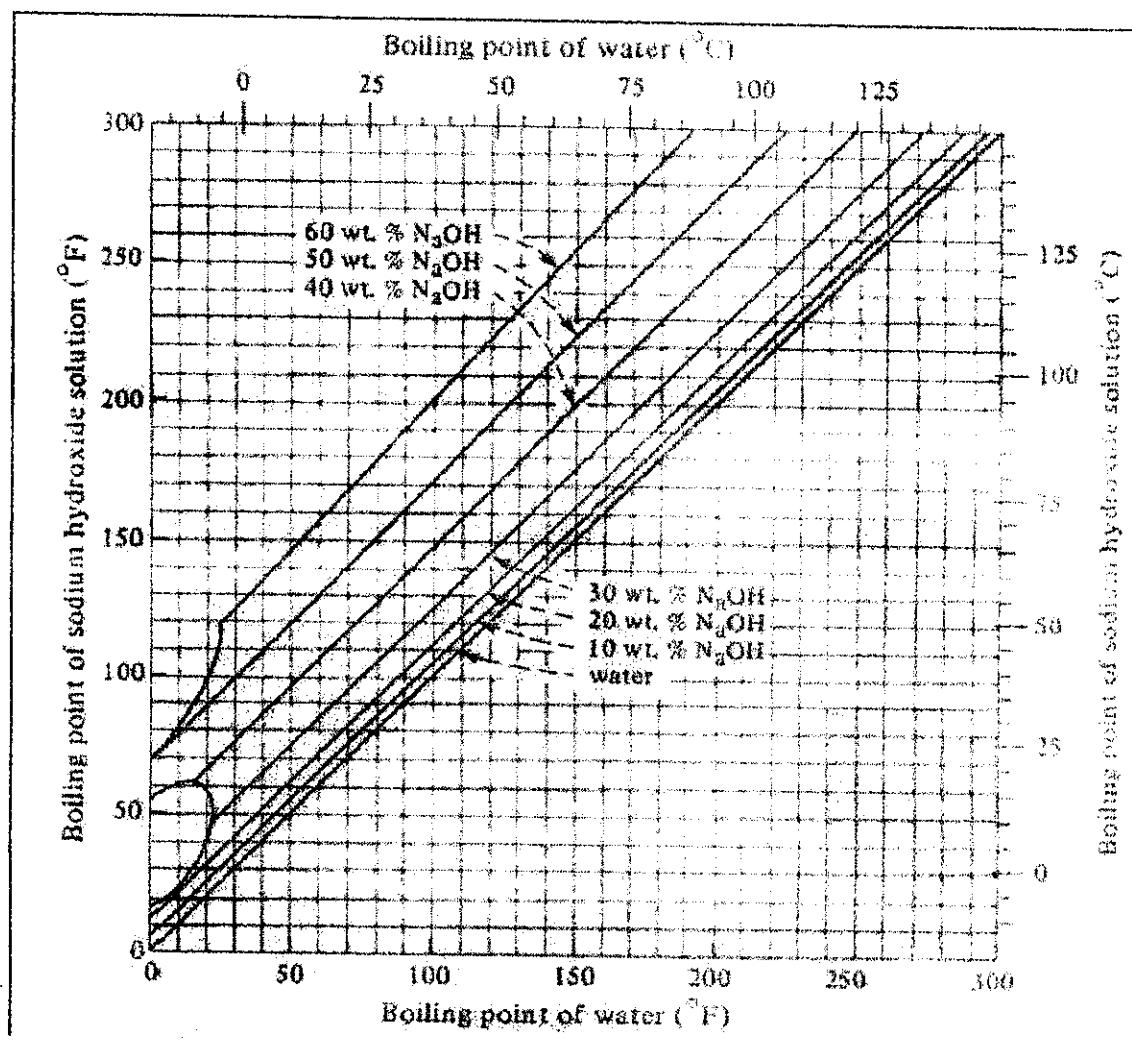


Figure. 1 Duhring lines for aqueous solutions of sodium hydroxide.

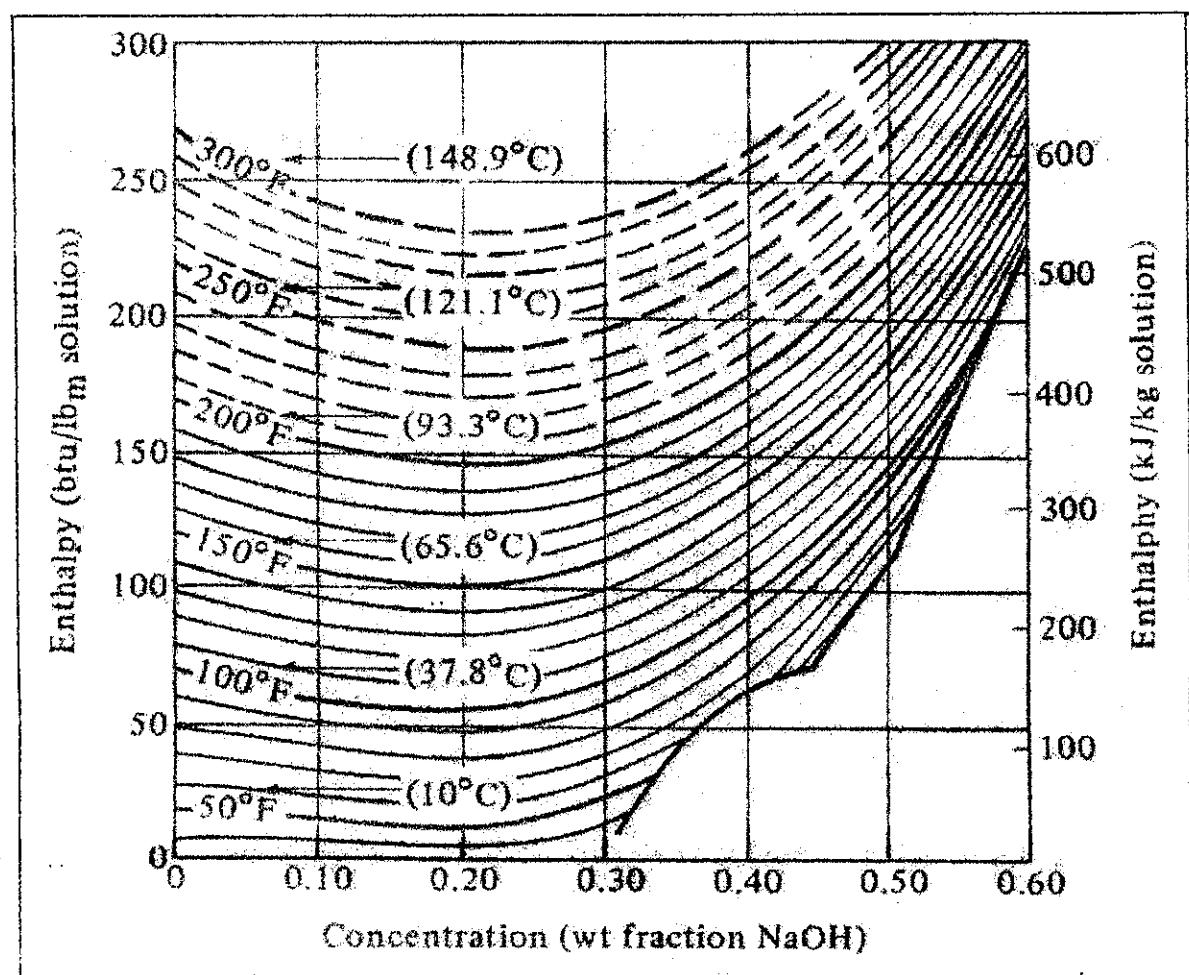


Figure.2 Enthalpy concentration chart for the system NaOH water.