Master of Mechanical Engg 2nd Semester Examination, 2019

Design of Industrial pressure vessel

Time: Three Hours

Full Marks: 100

Answer any five

All questions carry equal marks

1. Prove that, for a thick Spherical pressure vessel which is subjected to internal pressure p_i ,

$$\sigma_r = \frac{p_i a^3}{b^3 - a^3} \left(1 - \frac{b^3}{r^3} \right) \text{ and } \sigma_i = \frac{p_i a^3}{b^3 - a^3} \left(1 + \frac{b^3}{2r^3} \right), \text{ where the terms have usual meaning.}$$

- (a) An industrial pressure vessel is to be designed based on various failure theories. Internal pressure = 150 MN/m². Internal diameter: 800 mm. Yield point stress 450 MN/m². Calculate the wall thicknesses required according to Maximum normal stress theory, Maximum shear theory. Maximum strain theory, maximum strain energy theory.
 - (b)Derive the expression of wall thickness as per maximum distortion energy theory & calculate the thickness with the help of data given in 2(a)
- A cylinder of outer radius 'a' and inner radius b is subjected to autofrettage where entire cylinder wall has been plastically penetrated. Derive the expression for the residual stress and explain graphically assuming b/a=2.
- 4. Derive the expression of thermal stress for $radial(\sigma_r)$, $tangential(\sigma_r)$ and axial stress (σ_z) developed in a cylinder [outer radius 'b' and inner radius 'a'] for a steady state logarithmic thermal gradient having inner temperature T_i (at r=a) and outer temperature being 0 (at r=b), E is the young's modulus and α is the coefficient of linear thermal expansion.
- 5. Prove that thermal stress developed in a hollow cylindrical pressure vessel for logarithmic temperature distribution is given by: $[r_e$ and r_i are inner and outer radius $a = r_e/r_i$

$$\sigma_{r} = \frac{E\alpha\Delta t}{2(1-\mu)} \left[\frac{a^{2} + \left(\frac{r_{e}}{r}\right)^{2}}{a^{2} - 1} - \frac{1 + \ln\left(\frac{r}{r_{i}}\right)}{\ln a} \right] \sigma_{r} = \frac{E\alpha\Delta t}{2(1-\mu)} \left[\frac{a^{2} - \left(\frac{r_{e}}{r}\right)^{2}}{a^{2} - 1} - \frac{\ln\left(\frac{r}{r_{i}}\right)}{\ln a} \right]$$

Draw the stress distribution for centrifugal heat flux and centripetal heat flux. Find the resultant stress distribution by superimposing the mechanical stress due to internal pressure p_i.

6. Prove that the thermal stress in a long hollow cylinder, when heated uniformly throughout its thickness is given

$$\sigma_{r} = \frac{\alpha E}{(1-\mu)r^{2}} \left[\frac{r^{2} - a^{2}}{b^{2} - a^{2}} \int_{a}^{b} Tr dr - \int_{a}^{r} Tr dr \right]$$
by
$$\sigma_{r} = \frac{\alpha E}{(1-\mu)r^{2}} \left[\frac{r^{2} + a^{2}}{b^{2} - a^{2}} \int_{a}^{b} Tr dr - \int_{a}^{r} Tr dr - Tr^{2} \right]$$

Where 'T' represents temperature distribution and other terms have the usual meaning.

 Prove that thermal stress developed in a hollow spherical pressure vessel for logarithmic temperature distribution is given by: [r_e and r_i are inner and outer radius a = r_e/r_i]

$$\sigma_t = \frac{E\alpha\Delta t}{\left(1-\mu\right)} \left[\frac{r_e}{\left(a-1\right)r} - \frac{2a}{a^2-1} \right] \text{ and } \sigma_r = 0 \quad \text{. Plot the variation of stress distribution both for centrifugal and } \sigma_t = 0$$

centripetal heat flux. Also study the combined effect of mechanical stresses and thermal stresses for σ_i . 20

8. A pipe made of C.I. [inner diameter 250 mm, 15 mm thick] is wound closely with a single layer of circular steel wire of 5 mm diameter, under a tension of 70 N/mm². Find the compressive stress in the pipe section. Also find the stresses set up in the pipe and steel wire, when water under a pressure of 3.5N/mm² is admitted into the pipe. Take Young's modulus E for castiron (C.I.) is 10⁵ N/mm² and E for steel is 2X10⁵ N/mm². Poission's ratio is 0.3.