

Loop eqns. for a $N \times N$ passive network:

$$Z_{11} I_1 + Z_{12} I_2 + \dots + Z_{1N} I_N = V_1$$

$$Z_{21} I_1 + Z_{22} I_2 + \dots + Z_{2N} I_N = V_2$$

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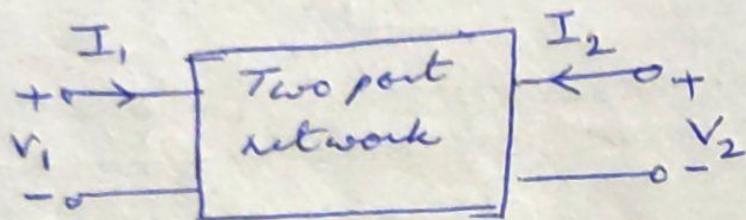
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$$Z_{N1} I_1 + Z_{N2} I_2 + \dots + Z_{NN} I_N = V_N$$

$$\Rightarrow \underline{Z} \underline{I} = \underline{V}$$

$$\begin{bmatrix} Z_{11} & Z_{12} & \dots & Z_{1N} \\ Z_{21} & Z_{22} & \dots & Z_{2N} \\ \vdots & \vdots & \ddots & \vdots \\ Z_{N1} & Z_{N2} & \dots & Z_{NN} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \\ \vdots \\ I_N \end{bmatrix} = \begin{bmatrix} V_1 \\ V_2 \\ \vdots \\ V_N \end{bmatrix}$$

$$\text{so } I_1 = \frac{\Delta_{11}}{\Delta_2} \cdot V_1 ; Z_{1n} = \frac{V_1}{I_1} = \frac{\Delta_2}{\Delta_{11}} \text{ (new)}$$



Short circuit admittance parameters y_{ij}

$$\begin{aligned} I_1 &= y_{11}V_1 + y_{12}V_2 \\ I_2 &= y_{21}V_1 + y_{22}V_2 \end{aligned} \quad \left| \Rightarrow \begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} \right| \Rightarrow \underline{I} = \underline{Y} \underline{V}$$

$$\therefore y_{11} = \frac{I_1}{V_1} \Big|_{V_2=0} ; \quad y_{12} = \underbrace{\frac{I_1}{V_2}}_{\text{i/p admittance}} \Big|_{V_1=0}, \quad y_{21} = \underbrace{\frac{I_2}{V_1}}_{\text{transfer admittances}} \Big|_{V_2=0}, \quad y_{22} = \frac{I_2}{V_2} \Big|_{V_1=0}.$$

Open circuit impedance parameters z_{ij}

$$\begin{aligned} V_1 &= z_{11}I_1 + z_{12}I_2 \\ V_2 &= z_{21}I_1 + z_{22}I_2 \end{aligned} \quad \left| \Rightarrow \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} z_{11} & z_{12} \\ z_{21} & z_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix} \right| \Rightarrow \underline{V} = \underline{Z} \underline{I}$$

$$\Rightarrow \begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = Z^{-1} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} \Rightarrow I_1 = \frac{z_{22}}{\Delta_Z} V_1 - \frac{z_{21}}{\Delta_Z} V_2 = \frac{\Delta_{11}}{\Delta_Z} V_1 - \frac{\Delta_{12}}{\Delta_Z} V_2$$

$$I_2 = \frac{-z_{12}}{\Delta_Z} V_1 + \frac{z_{11}}{\Delta_Z} V_2 = -\frac{\Delta_{21}}{\Delta_Z} V_1 + \frac{\Delta_{22}}{\Delta_Z} V_2$$

$$\text{Voltage gain } G_V = \frac{V_2}{V_1}$$

$$\text{Current gain } G_I = \frac{I_2}{I_1}$$

Input impedance $Z_{in} = \frac{V_1}{I_1}$, output impedance Z_{out} = Thevenin impedance

$$= \frac{V_2}{I_2} = Z_{22} - \frac{Z_{12}Z_{21}}{Z_{11} + Z_g} \quad \text{for generator impedance } Z_g$$

$$V_g = V_1 + I_1 Z_g$$

Hybrid parameters t_{ij}

$$\begin{aligned} V_1 &= h_{11} I_1 + h_{12} V_2 \quad \left| \begin{bmatrix} V_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} I_1 \\ V_2 \end{bmatrix} \right. \\ I_2 &= h_{21} I_1 + h_{22} V_2 \end{aligned}$$

$$h_{11} = \frac{V_1}{I_1} \Big|_{V_2=0} = \text{s.c. i/p impedance}; \quad h_{12} = \frac{V_1}{V_2} \Big|_{I_1=0} = \text{o/p ckt. reverse voltage gain}$$

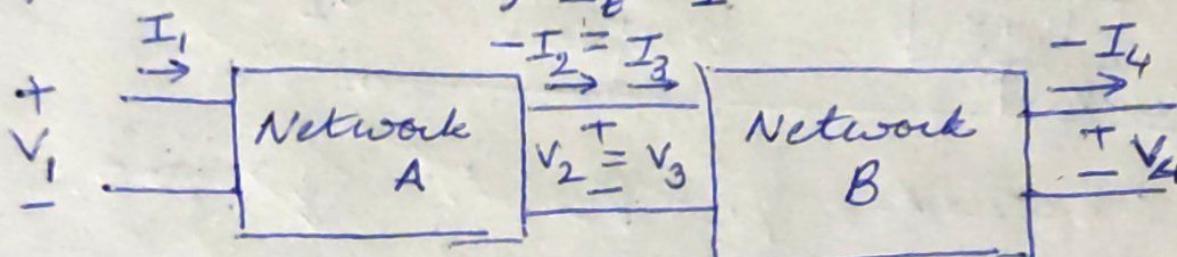
$$h_{21} = \frac{I_2}{I_1} \Big|_{V_2=0} = \text{s.c. fwd current gain}; \quad h_{22} = \frac{I_2}{V_2} \Big|_{I_1=0} = \text{o/p ckt. o/p admittance}$$

For bilateral network, $t_{12} = -t_{21}$

Transmission parameters t_{ij} ABCD parameters.

$$\begin{aligned} V_1 &= t_{11} V_2 - t_{12} I_2 \\ I_1 &= t_{21} V_2 - t_{22} I_2 \end{aligned} \Rightarrow \begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} t_{11} & t_{12} \\ t_{21} & t_{22} \end{bmatrix} \begin{bmatrix} V_2 \\ I_2 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ I_2 \end{bmatrix}$$

For reciprocal networks, $\Delta_t = 1$.

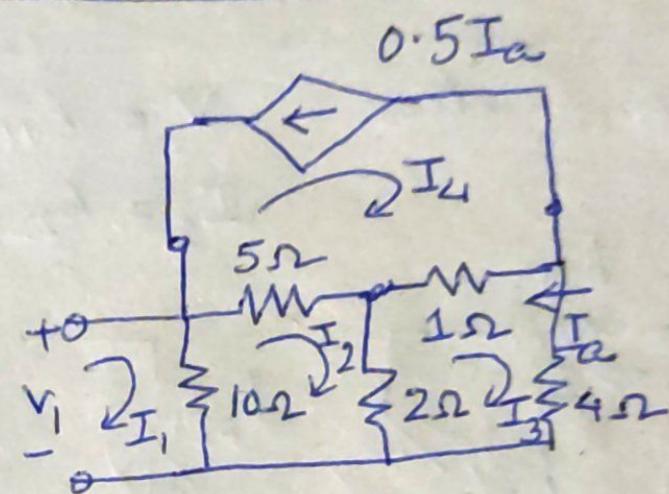
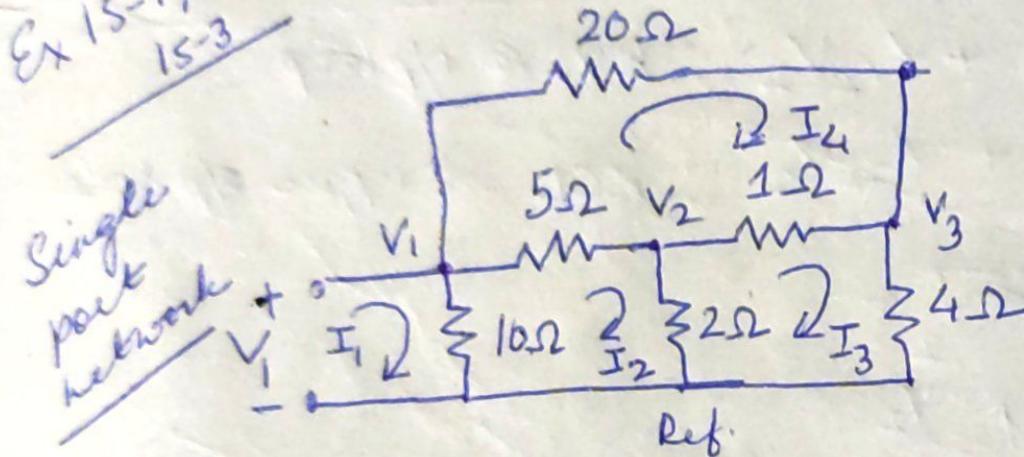


Cascade connections

For bilateral, $\Delta_t = t_{11} t_{22} - t_{12} t_{21} = 1$

Ex 15-1, 15-2
15-3

Single
port
network



$$V_1 = 10I_1 - 10I_2$$

$$0 = -10I_1 + 17I_2 - 2I_3 - 5I_4$$

$$0 = -2I_2 + 7I_3 - I_4$$

$$0 = -5I_2 - I_3 + 26I_4$$

Mesh
equations

$$V_1 = 10I_1 - 10I_2$$

$$0 = -10I_1 + 17I_2 - 2I_3 - 5I_4$$

$$0 = -2I_2 + 7I_3 - I_4$$

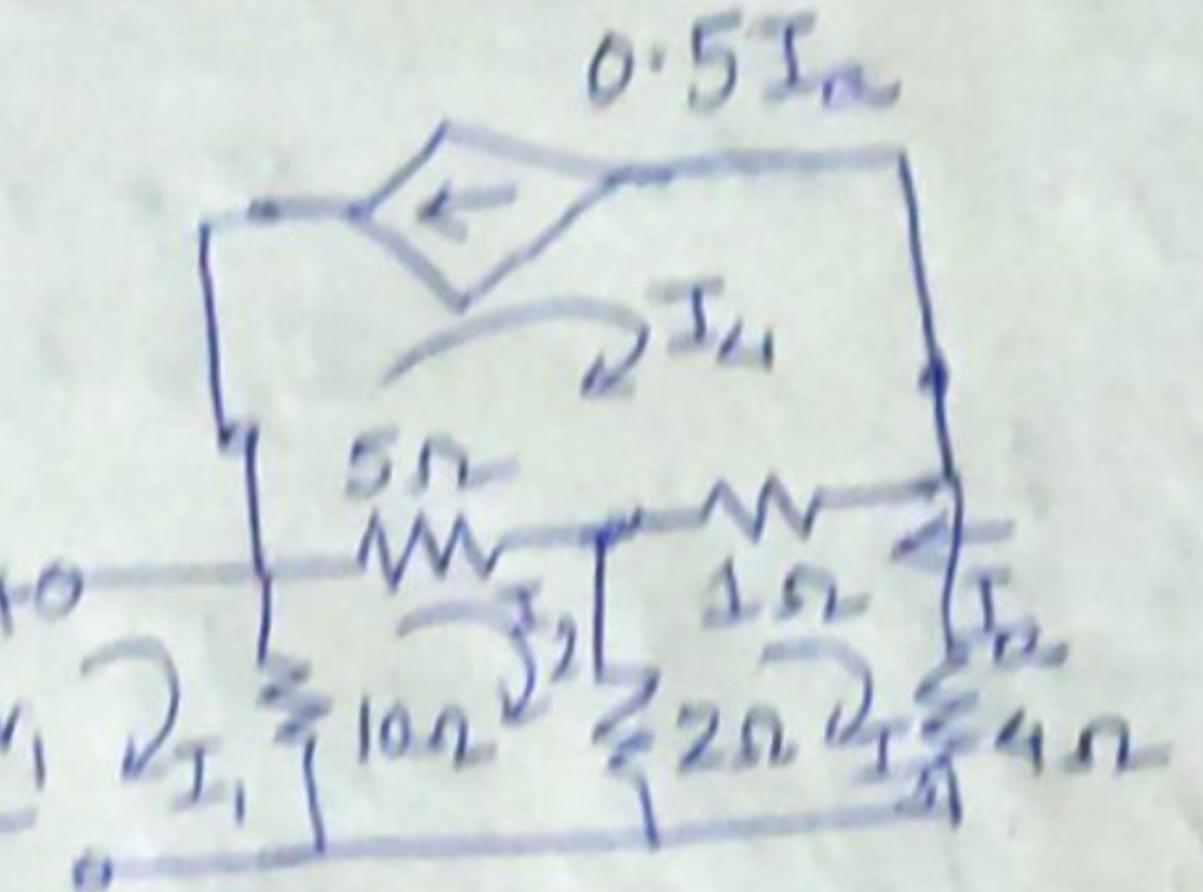
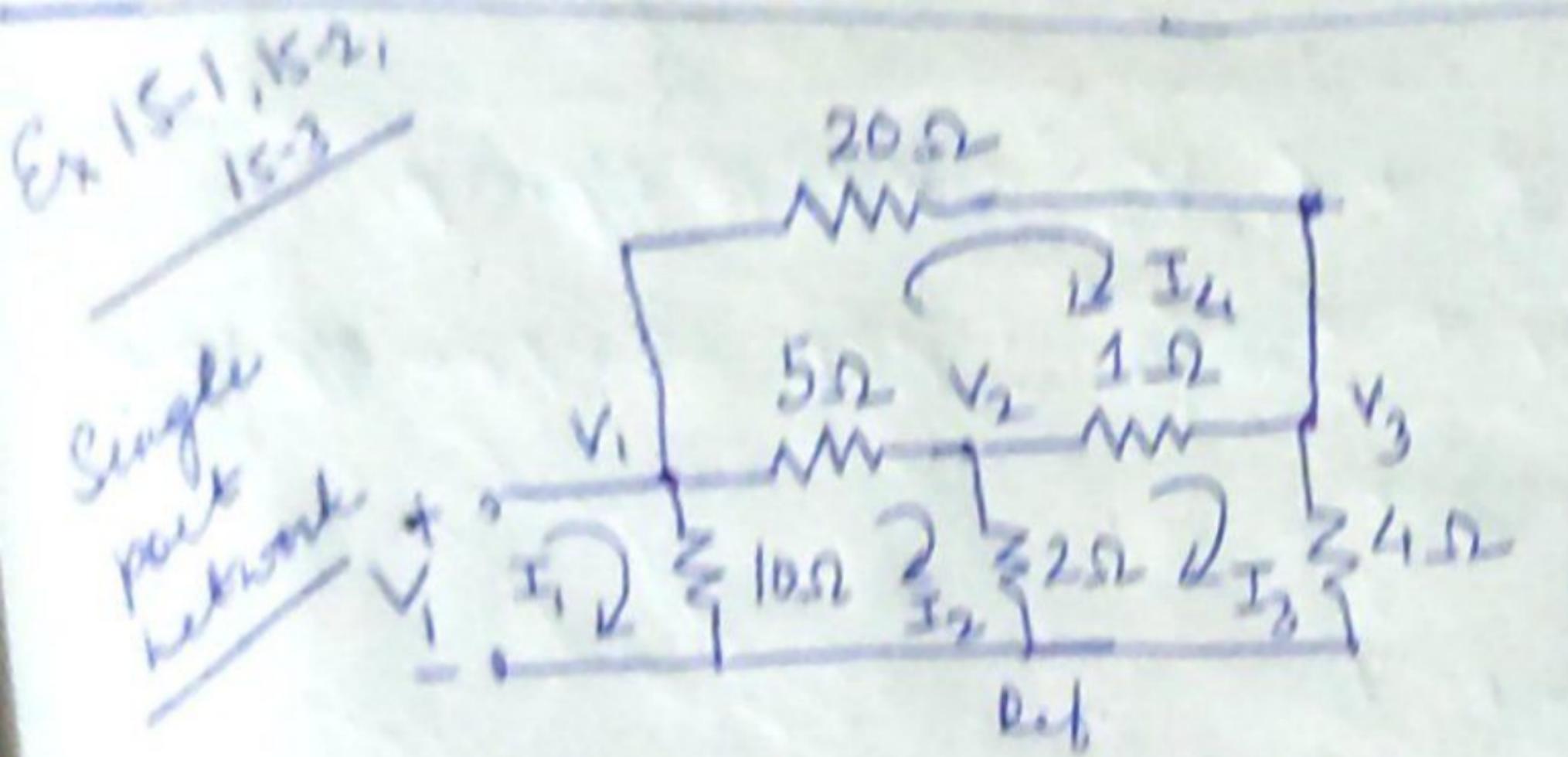
$$I_4 = -0.5I_a = -0.5(I_4 - I_3)$$

$$\Rightarrow 0 = +0.5I_3 - 1.5I_4$$

BILATERAL
ELEMENTS

$$\Delta_2 = \begin{bmatrix} 10 & -10 & 0 & 0 \\ -10 & 17 & -2 & -5 \\ 0 & -2 & 7 & -1 \\ 0 & -5 & -1 & 26 \end{bmatrix}$$

$$\Delta_2 = \begin{bmatrix} 10 & -10 & 0 & 0 \\ -10 & 17 & -2 & -5 \\ 0 & -2 & 7 & -1 \\ 0 & 0 & 0.5 & -1.5 \end{bmatrix}$$



Nodal

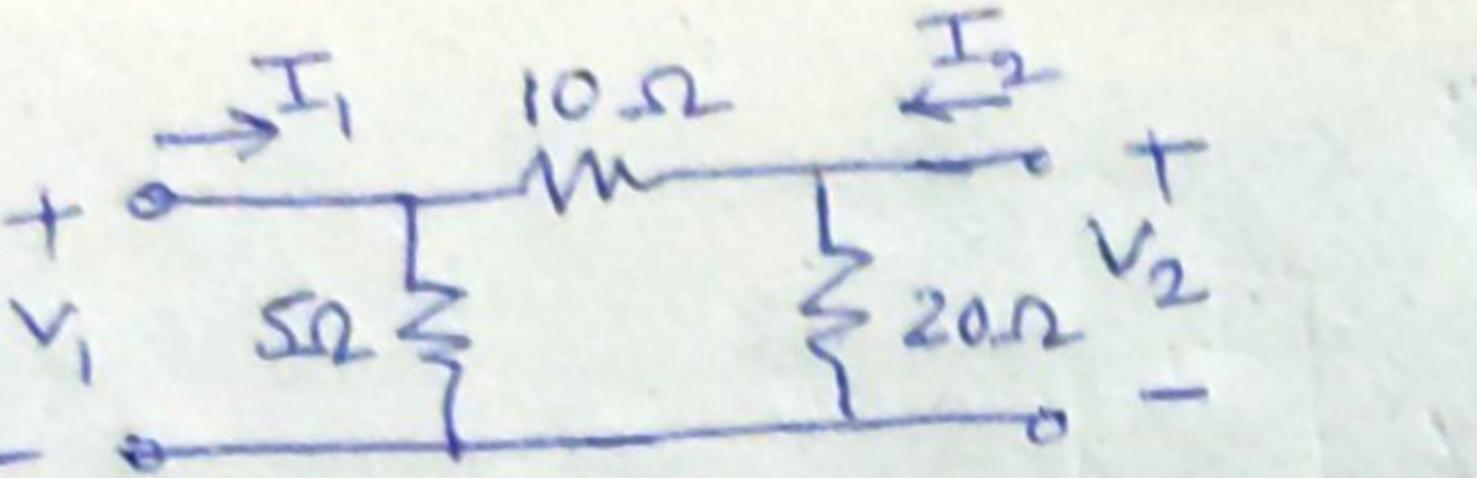
$$\begin{aligned}
 & \text{for } \Delta Y \\
 & \left. \begin{aligned}
 & v_1 \left(\frac{1}{10} + \frac{1}{5} + \frac{1}{20} \right) - 0.2v_2 - 0.05v_3 = 0 \\
 & - 0.2v_1 + v_2 \left(\frac{1}{5} + \frac{1}{2} + 1 \right) - v_3 = 0 \\
 & - 0.05v_1 - v_2 + v_3 \left(\frac{1}{20} + 1 + \frac{1}{4} \right) = 0
 \end{aligned} \right\}
 \end{aligned}$$

$$\Delta Y = \begin{bmatrix} 0.35 & -0.2 & -0.05 \\ -0.2 & 1.7 & -1 \\ -0.05 & -1 & 1.3 \end{bmatrix}; Y_{in} = \frac{\Delta Y}{\Delta_{11}}$$

Ex 155

Two
port
network

Y



$$\Rightarrow I_1 = 0.3V_1 - 0.1V_2$$

$$I_2 = -0.1V_1 + 0.15V_2$$

$$I_1 = V_1 \left(\frac{1}{5} + \frac{1}{10} \right) - 0.1V_2$$

$$I_2 = -0.1V_1 + V_2 \left(\frac{1}{10} + \frac{1}{20} \right)$$

$$\Rightarrow [Y] = \begin{bmatrix} 0.3 & -0.1 \\ -0.1 & 0.15 \end{bmatrix}$$

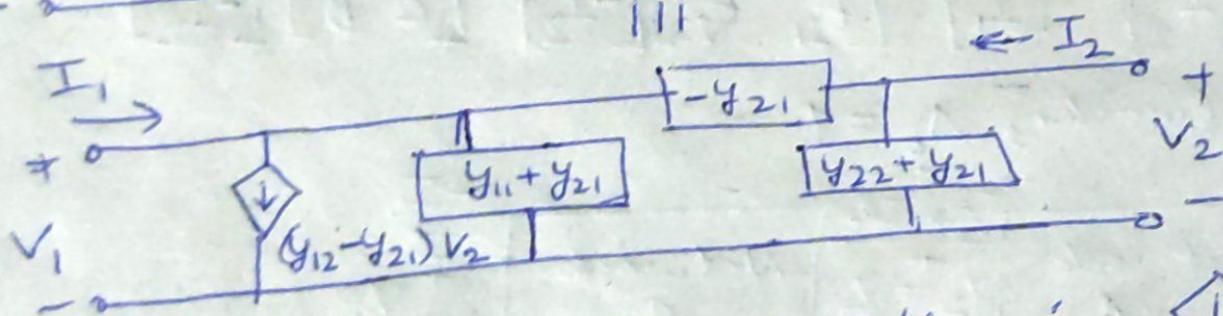
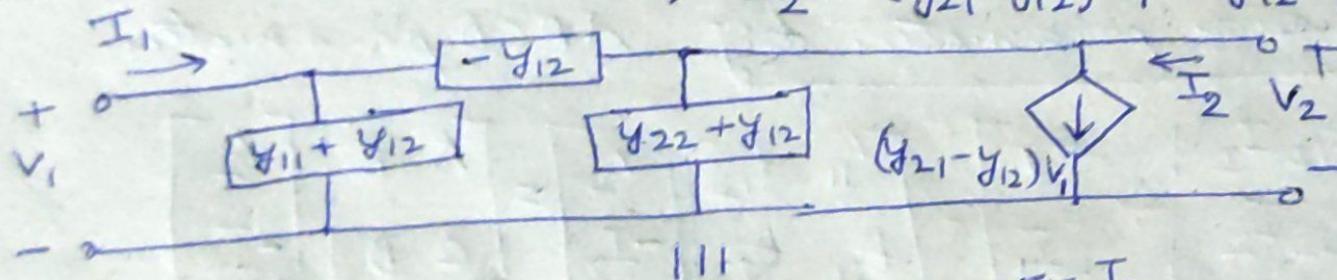
$$I_1 = y_{11}V_1 + y_{12}V_2$$

$$I_2 = y_{21}V_1 + y_{22}V_2$$

$$I_2 = y_{12}V_1 + y_{22}V_2 + (y_{21} - y_{12})V_1$$

for bilateral network form.

$$\Rightarrow I_2 - (y_{21} - y_{12})V_1 = y_{12}V_1 + y_{22}V_2$$



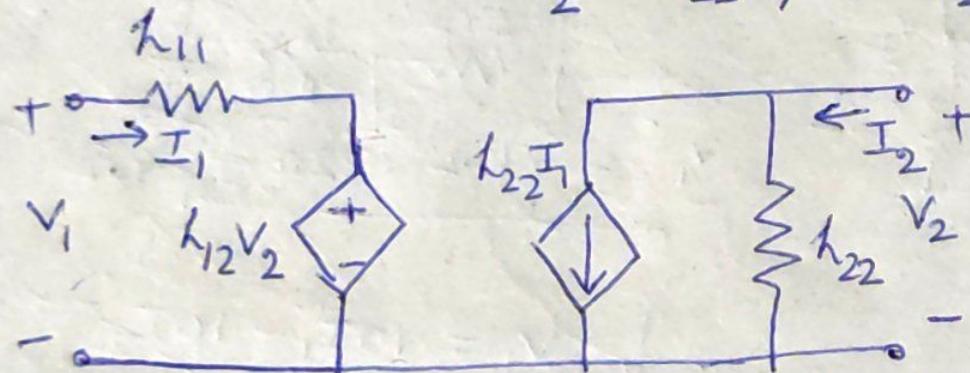
For bilateral network, $y_{12} = y_{21} \therefore \square \rightarrow 0$.

Also $\nabla \rightarrow Y$ conversion possible.

For h-parameters

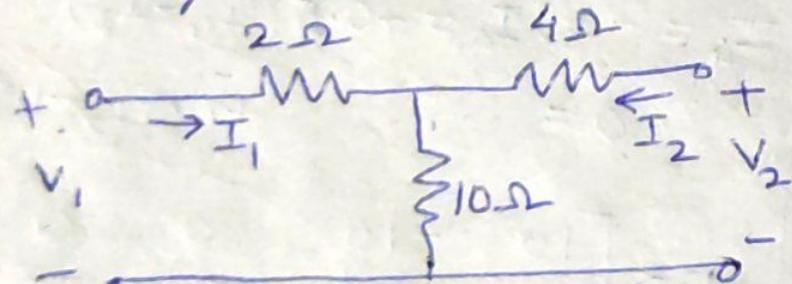
$$V_1 = R_{11} I_1 + h_{12} V_2 \quad : \text{KVL @ i/p loop}$$

$$I_2 = h_{21} I_1 + h_{22} V_2 \quad : \text{KCL at upper o/p node}$$



transistor equivalent circuit

For t-parameters



$$V_1 = t_{11} V_2 - t_{12} I_2$$

$$I_1 = t_{21} V_{12} - t_{22} I_2$$

$$V_1 = 12 I_1 + 10 I_2$$

$$V_2 = 10 I_1 + 14 I_2 \rightarrow I_1 = \frac{1}{12} V_1 - \frac{1}{14} I_2$$

$$t_{11} = 1.2 V_1 - 6.8 I_2$$

$$t_{12}$$