

Hot-Wire Anemometers

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Hot-Wire Anemometers

**Constant Current
Anemometer (CCA)**

**Wire current is
maintained constant**

**Equilibrium wire temperature
is a measure of flow velocity**

**Constant Temperature
Anemometer (CTA)**

**Wire temperature is
maintained constant**

**Equilibrium wire current is a
measure of flow velocity**

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Hot-Wire Anemometers

Energy balance equation for the hot wire in equilibrium condition:

$$I^2 R_w = hA(T_w - T_f)$$

I = wire current

R_w = wire resistance

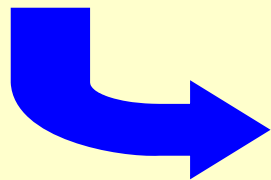
T_w = wire temperature

T_f = temperature of flowing fluid

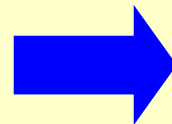
h = film coefficient of heat transfer

A = heat - transfer area

✓ h is mainly a function of flow velocity for a given fluid density.



King's Law

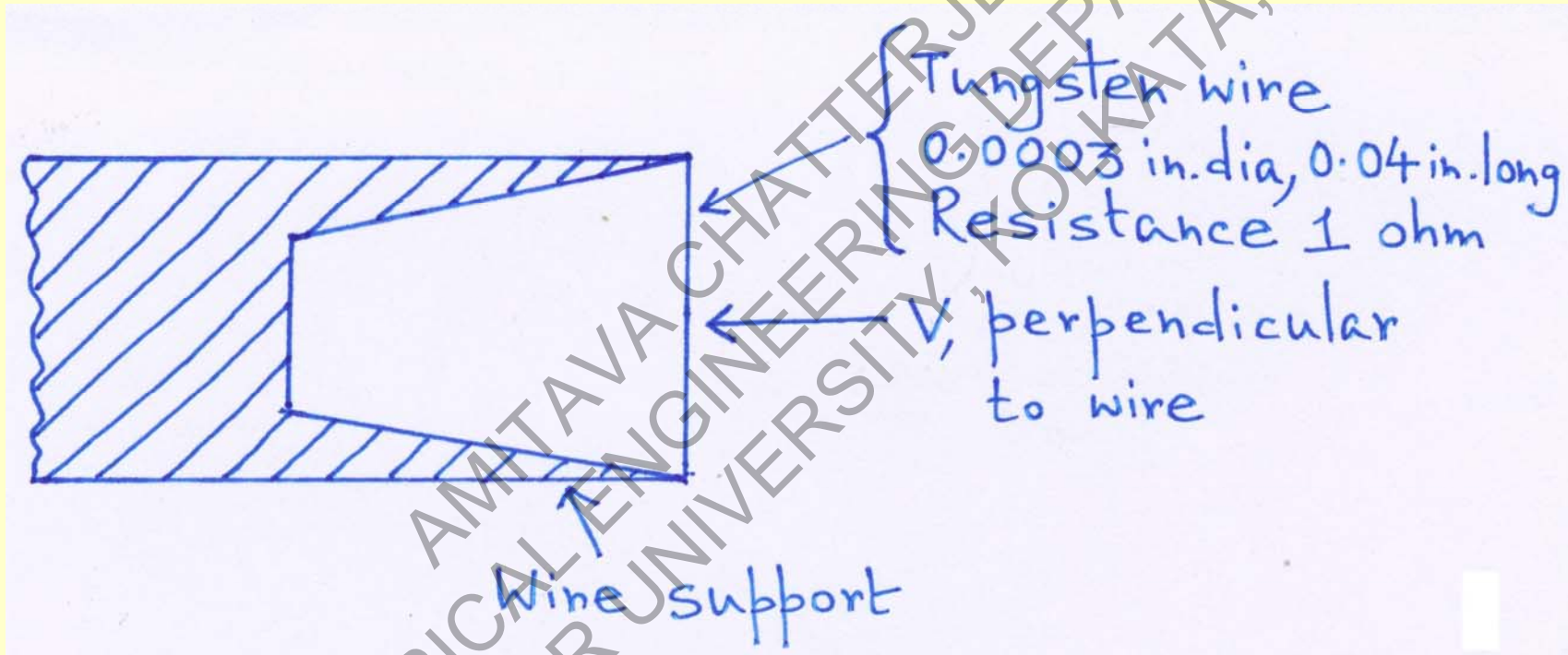


$$h = C_0 + C_1 \sqrt{V}$$

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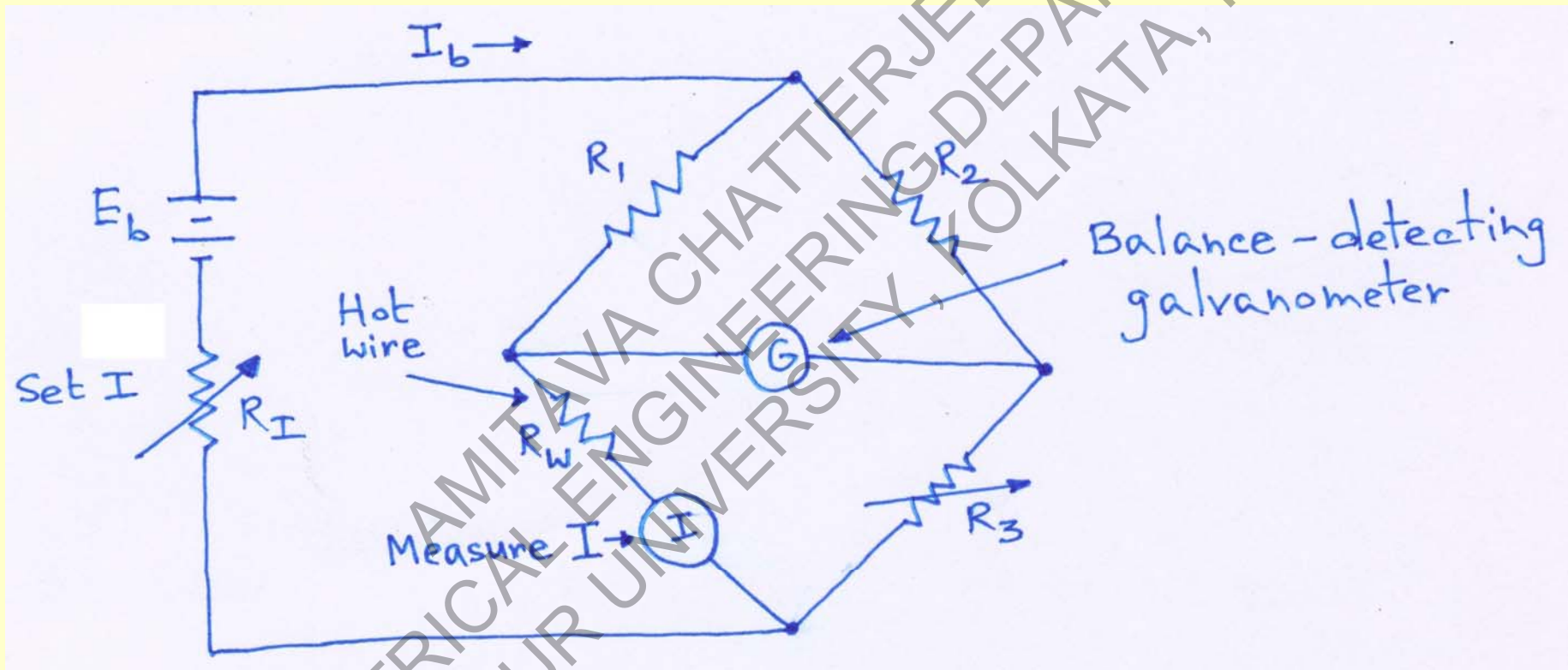
Measurement of Average velocity using CTA in "Manual Balance" Mode



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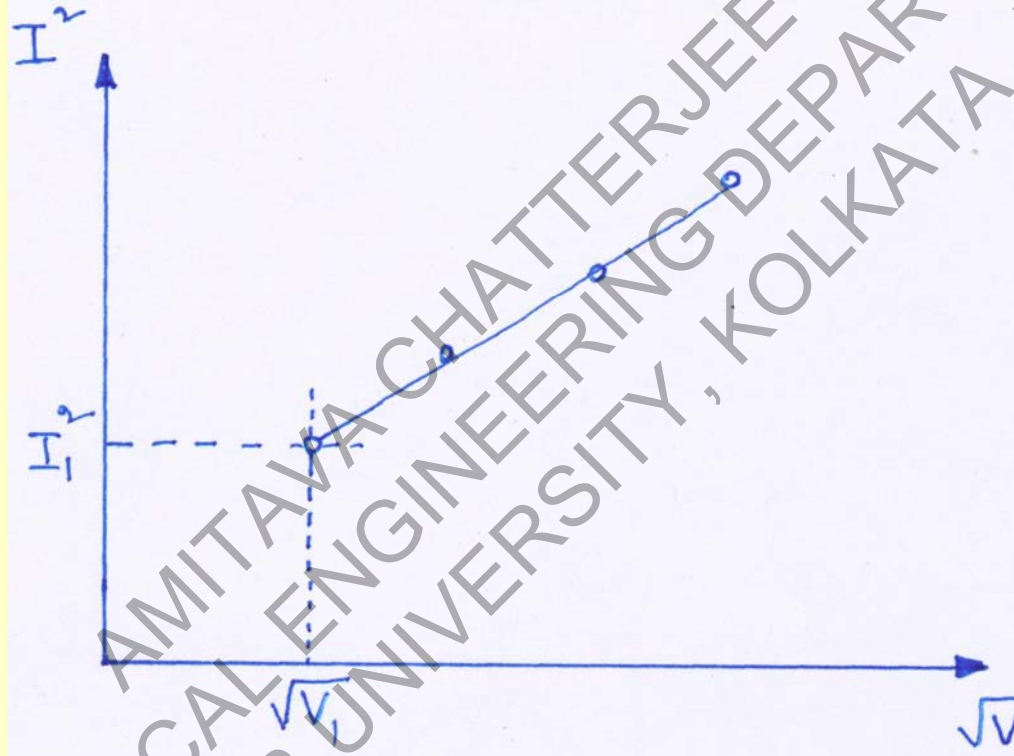
Measurement of Average velocity using CTA in "Manual Balance" Mode (contd...)



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Measurement of Average velocity using CTA in "Manual Balance" Mode (contd...)

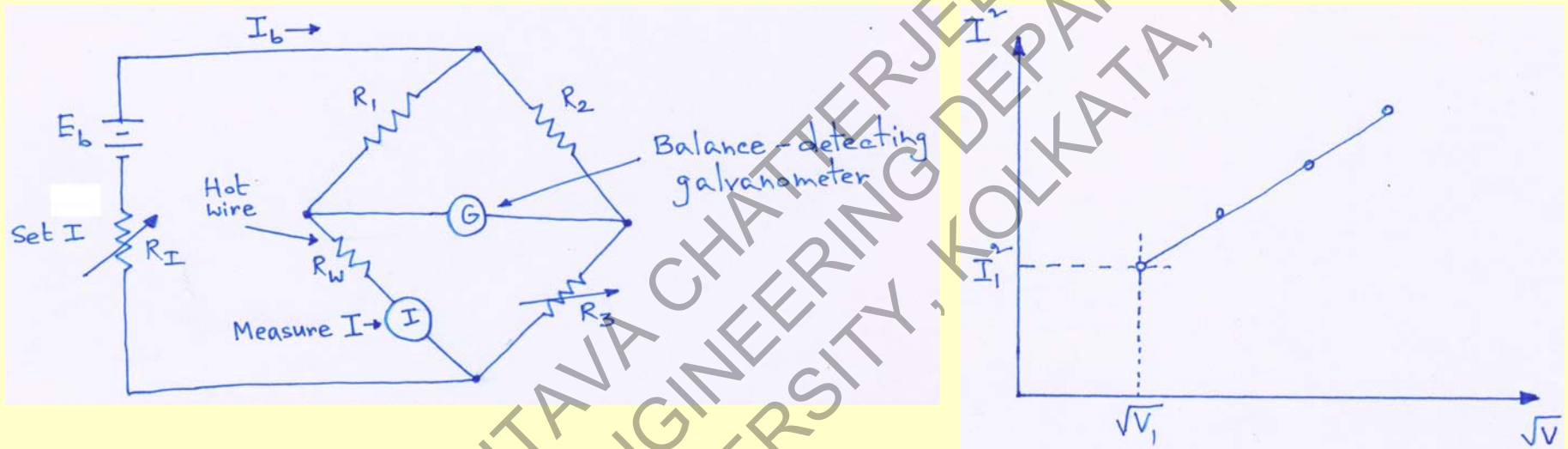


- ✓ For accurate work, a given hot-wire probe must be calibrated in the fluid in which it is to be used.

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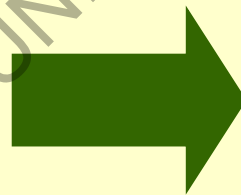
Measurement of Average Velocity using CTA in "Manual Balance" Mode (contd...)



At the equilibrium condition:

$$I^2 = \frac{A(T_w - T_f)(C_0 + C_1\sqrt{V})}{R_w}$$

$$= C_2 + C_3\sqrt{V}$$

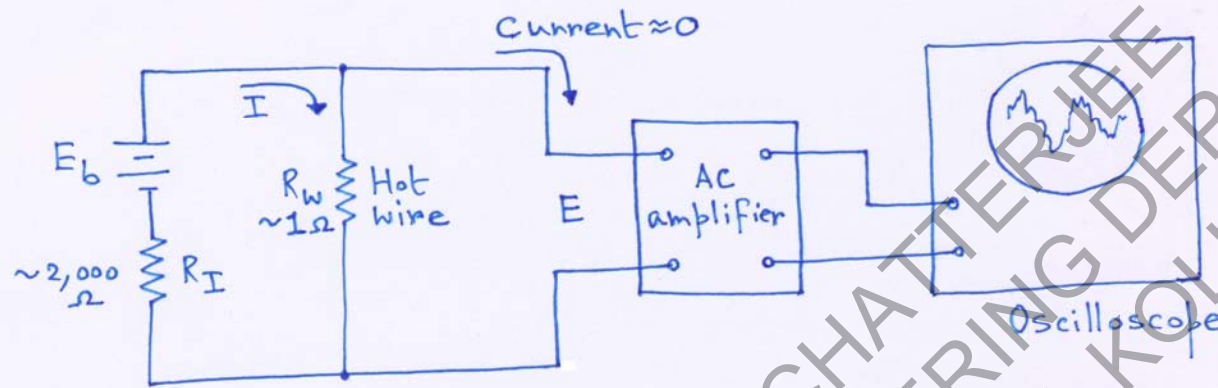


The calibration curve should be a straight line.

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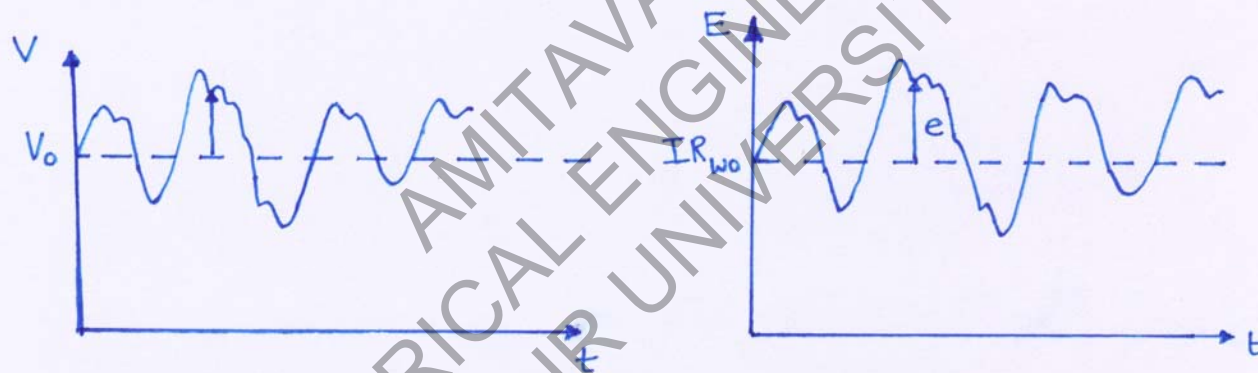
Measurement of Fluctuating Velocity using Constant Current Anemometer



$$V = V_0 + v$$

$$R_w = R_{w0} + r_w$$

$$T_w = K_{tr} (R_{w0} + r_w)$$

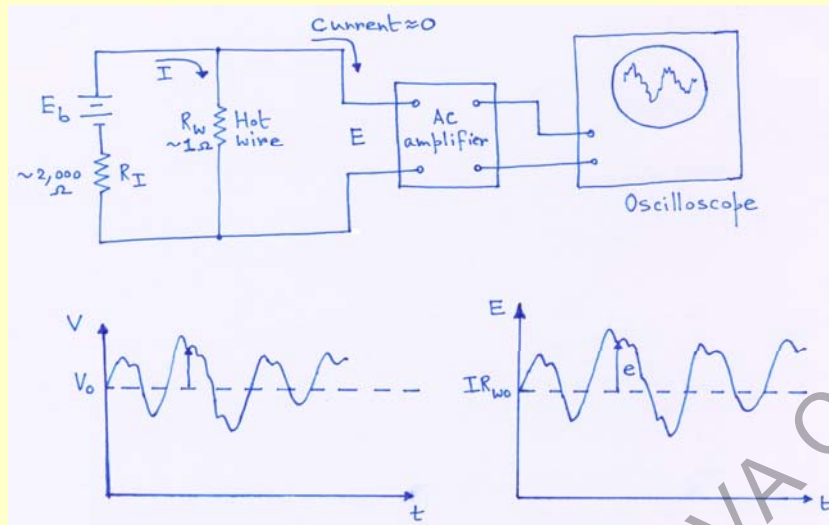


- ✓ The current can be assumed constant at I , even if R_w changes, since $R_I \gg R_w$.

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Measurement of Fluctuating Velocity using Constant Current Anemometer



Electrical energy generated – energy lost by convection = energy stored in wire

Energy lost by convection:

$$A(T_w - T_f)(C_0 + C_1\sqrt{V})dt$$

$$f(V) = f(V_0 + v) = C_0 + C_1\sqrt{V}$$

$$\approx f(V_0) + f'(V)|_{V=V_0} \cdot h \approx (C_0 + C_1\sqrt{V_0}) + \left. \frac{\partial f}{\partial V} \right|_{V=V_0} (V - V_0)$$

$$C_0 + C_1\sqrt{V} \approx (C_0 + C_1\sqrt{V_0}) + K_v v$$

$$I^2(R_{w0} + r_w)dt - A(T_w - T_f)(C_0 + C_1\sqrt{V_0} + K_v v)dt = MCdT_w$$

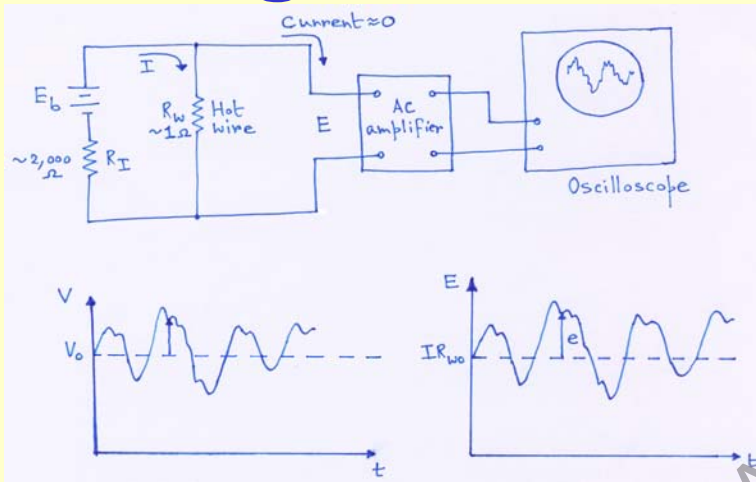
M = mass of wire

C = specific heat of wire

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$$I^2 R_{w0} + I^2 r_w - A [K_{tr} (R_{w0} + r_w) - T_f] (C_0 + C_1 \sqrt{V_0} + K_v v) = MCK_{tr} \frac{dr_w}{dt}$$

Also, $I^2 R_{w0} - A (K_{tr} R_{w0} - T_f) (C_0 + C_1 \sqrt{V_0}) = 0$

and the term containing the product $r_w v$ of two small quantities can be neglected.

Voltage across R_w : $IR_w = I(R_{w0} + r_w) = E_0 + e$



$$\frac{e(s)}{v(s)} = \frac{Ir_w(s)}{v(s)} = \frac{IAK_v (K_{tr} R_{w0} - T_f)}{I^2 - AK_{tr} (C_0 + C_1 \sqrt{V_0}) - sK_{tr} MC} = \frac{K}{1 + s\tau}$$

where,

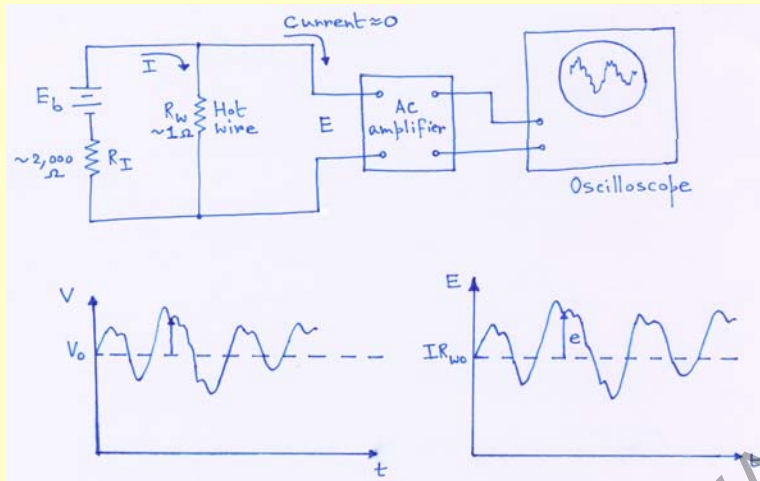
$$K = \frac{-K_v AI (K_{tr} R_{w0} - T_f)}{AK_{tr} (C_0 + C_1 \sqrt{V_0}) - I^2}$$

$$\tau = \frac{MCK_{tr}}{AK_{tr} (C_0 + C_1 \sqrt{V_0}) - I^2}$$

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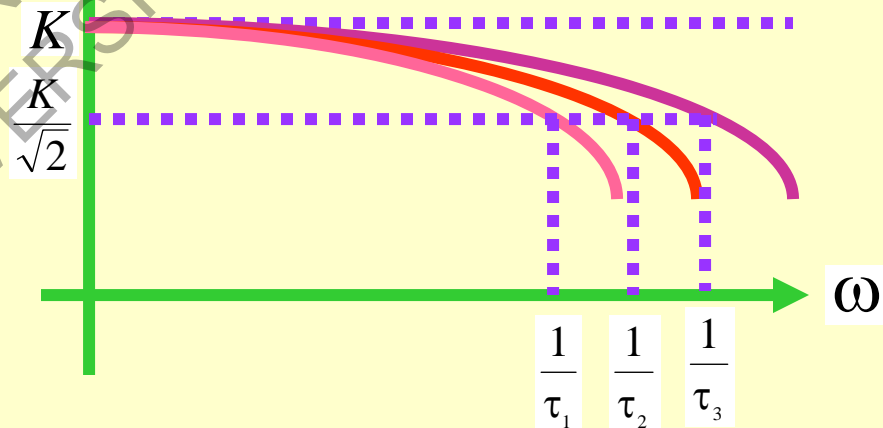


Frequency response: $\frac{e(j\omega)}{v(j\omega)} = \frac{K}{1 + j\omega\tau}$

Magnitude response: $\left| \frac{e(j\omega)}{v(j\omega)} \right| = \frac{K}{\sqrt{1 + \omega^2\tau^2}}$

$$\left| \frac{e(j\omega)}{v(j\omega)} \right|$$

$$\tau_1 > \tau_2 > \tau_3$$



τ can not be made less than 0.001 sec.

Cut off frequency:

$$\omega' = \frac{1}{0.001} = 1000$$

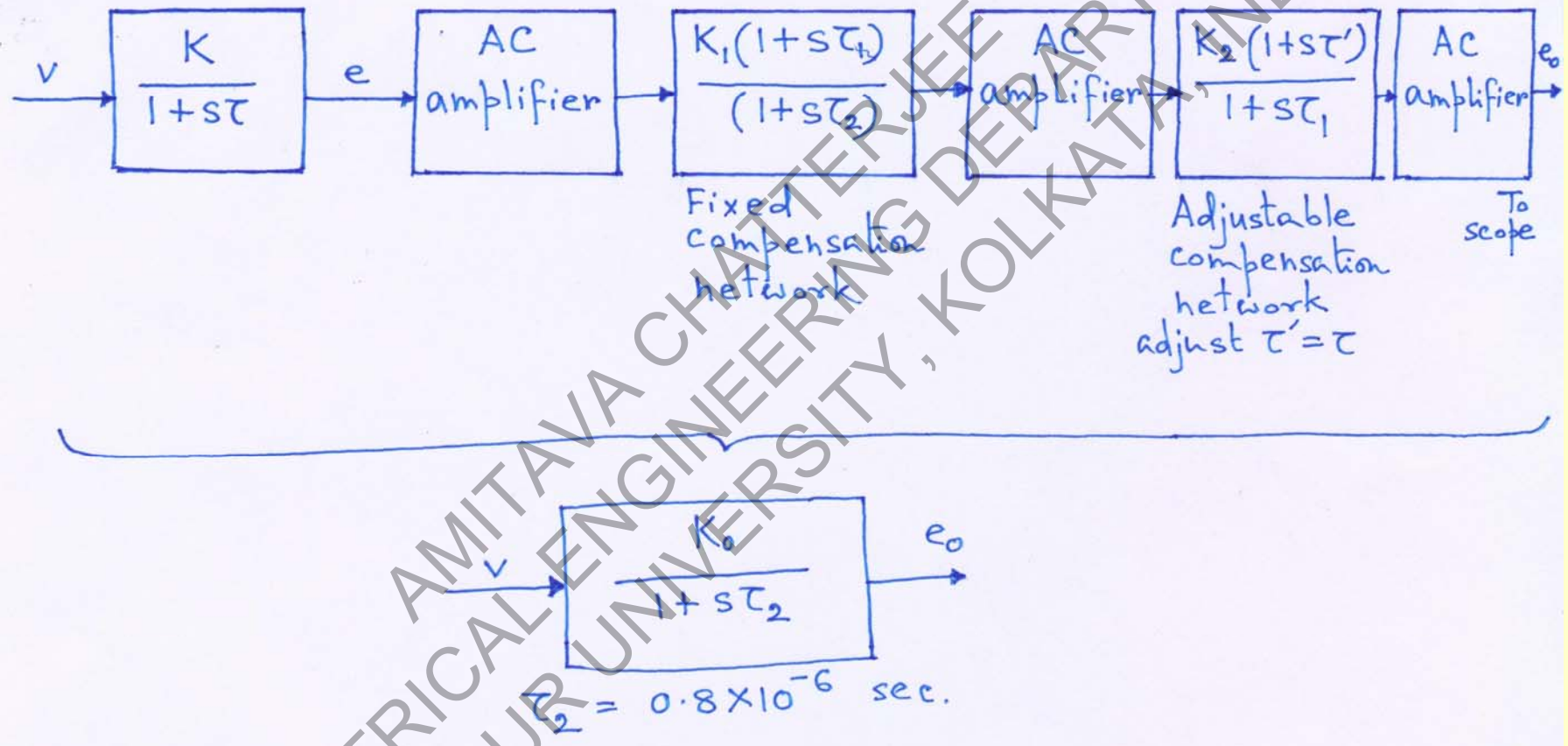
or, $f' \approx 160$ Hz.

✓ For turbulence studies, we have to add electrical dynamic compensation scheme.

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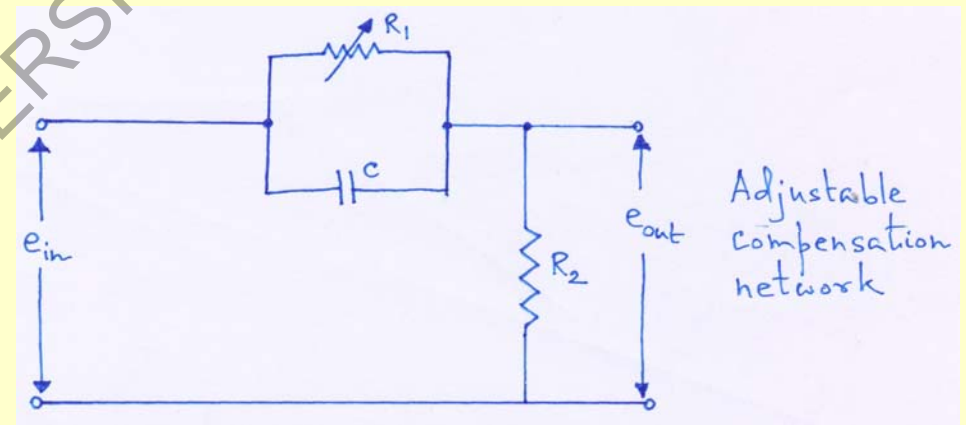
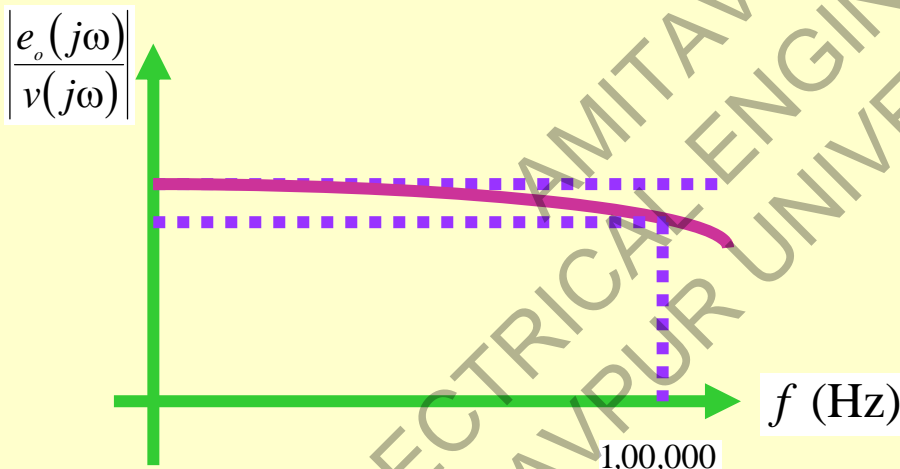
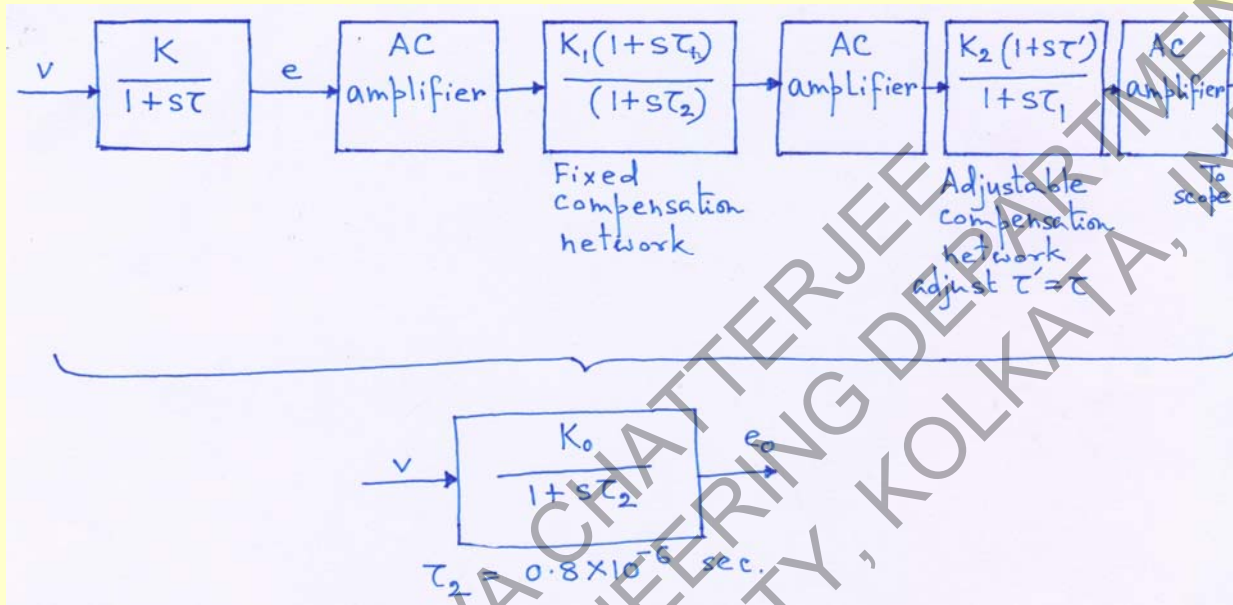
Electrical Dynamic Compensation



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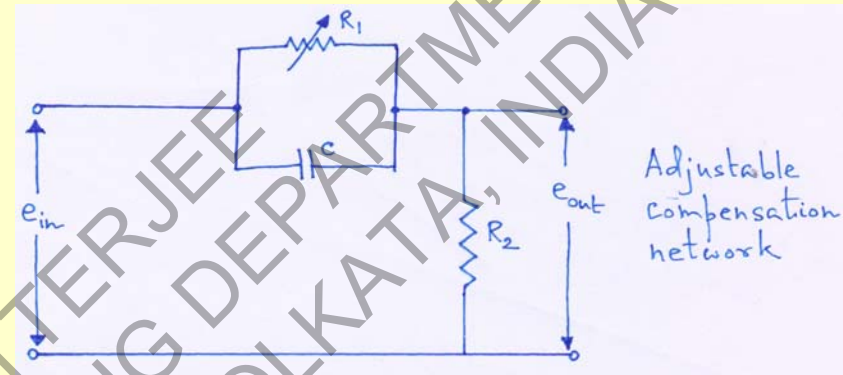
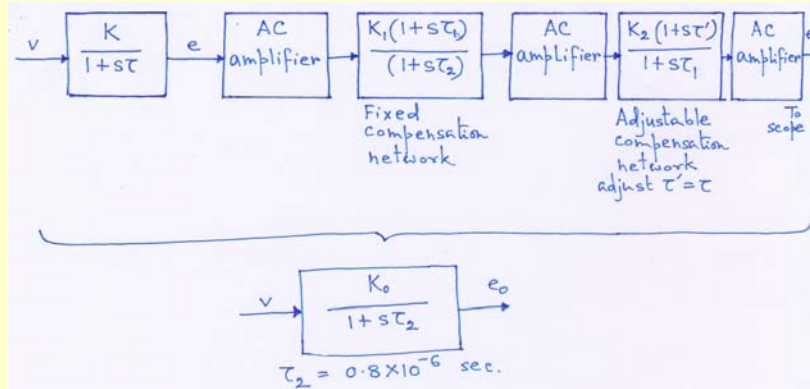
Electrical Dynamic Compensation



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Electrical Dynamic Compensation



Transfer Function of the Compensation Network:

$$\frac{e_{out}(s)}{e_{in}(s)} = \frac{R_2}{R_2 + \left(R_1 \times \frac{1}{sC} \right) \left(R_1 + \frac{1}{sC} \right)}$$



$$\frac{e_{out}(s)}{e_{in}(s)} = K \left(\frac{1 + s\tau_{11}}{1 + s\tau_{22}} \right)$$

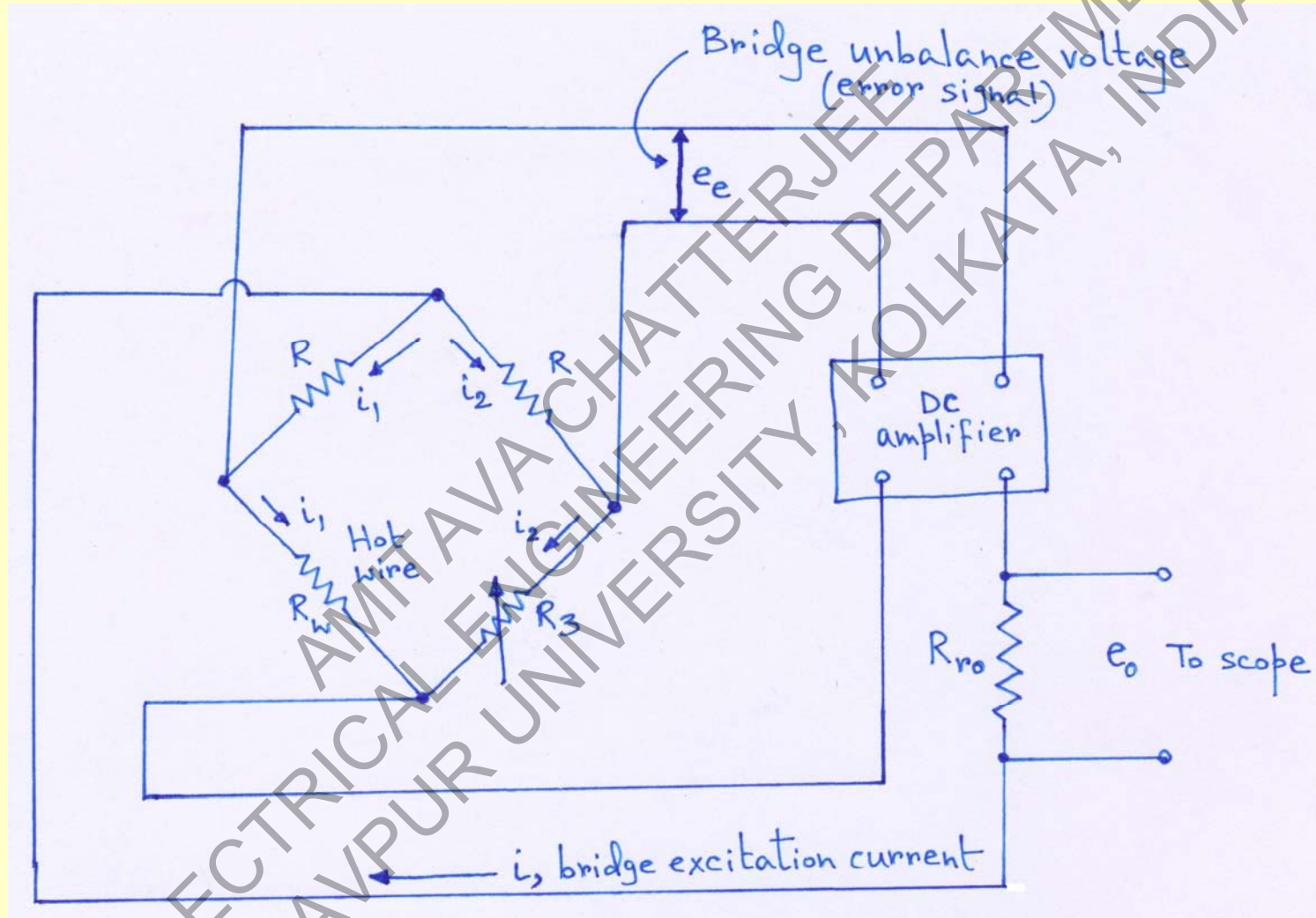
where:

$$K = \frac{R_2}{R_1 + R_2}, \tau_{11} = CR_1, \tau_{22} = C \frac{R_1 R_2}{R_1 + R_2}$$

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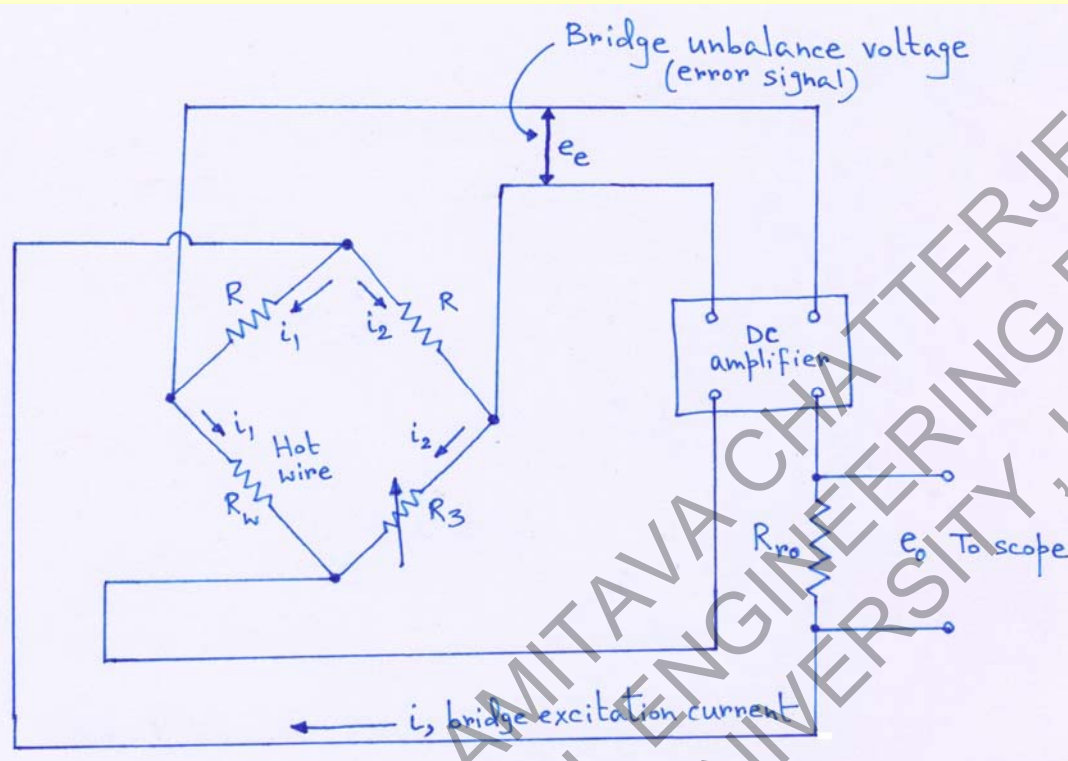
Measurement of Fluctuating Velocity using Constant Temperature Anemometer



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Measurement of Fluctuating Velocity using Constant Temperature Anemometer



✓ Here, the bridge balancing operation is made automatic by employing a feedback arrangement.

Fluctuating components of current:

$$i_1 = \frac{R + R_3}{2R + R_w + R_3} i;$$

$$i_2 = \frac{R + R_w}{2R + R_w + R_3} i;$$

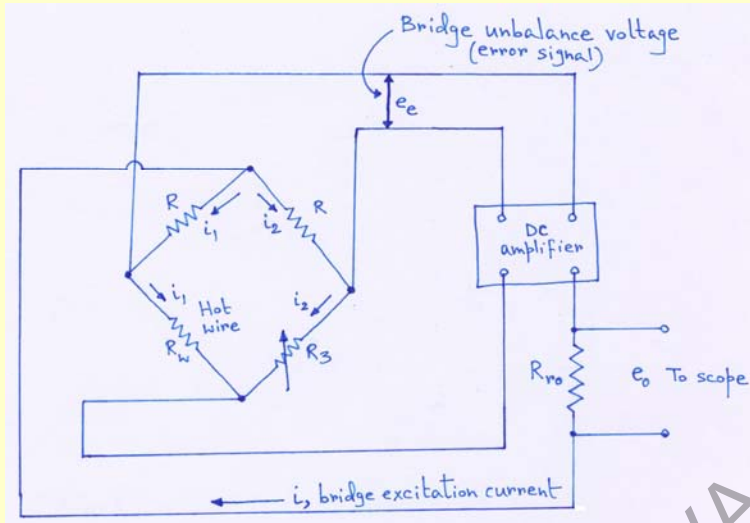
Energy balance equation: Electrical energy generated – energy lost by convection = energy stored in wire

$$(I_m + i_1)^2 (R_{w0} + r_w) - A [K_{cr} (R_{w0} + r_w) - T_f] (C_0 + C_1 \sqrt{V_0}) = MCK_{cr} \frac{dr_w}{dt} \quad (\text{velocity} = V_0 = \text{constant})$$

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Energy balance equation:

$$(I_m + i_1)^2 (R_{w0} + r_w) - A [K_{cr} (R_{w0} + r_w) - T_f] (C_0 + C_1 \sqrt{V_0}) = MCK_{cr} \frac{dr_w}{dt}$$

Initial steady condition:

$$I_m^2 R_{w0} = A (K_{cr} R_{w0} - T_f) (C_0 + C_1 \sqrt{V_0})$$

and the terms containing product of two small quantities are neglected, i.e.:

$$2I_m i_1 r_w \text{ and } i_1^2 (R_{w0} + r_w)$$

$$\frac{r_w(s)}{i_1(s)} = \frac{K_i}{1 + s\tau} = \frac{K_e / I_m}{1 + s\tau};$$

$$K_i = \frac{2I_m R_{w0}}{AK_{cr} (C_0 + C_1 \sqrt{V_0}) - I_m^2};$$

$$\tau = \frac{MCK_{cr}}{AK_{cr} (C_0 + C_1 \sqrt{V_0}) - I_m^2};$$

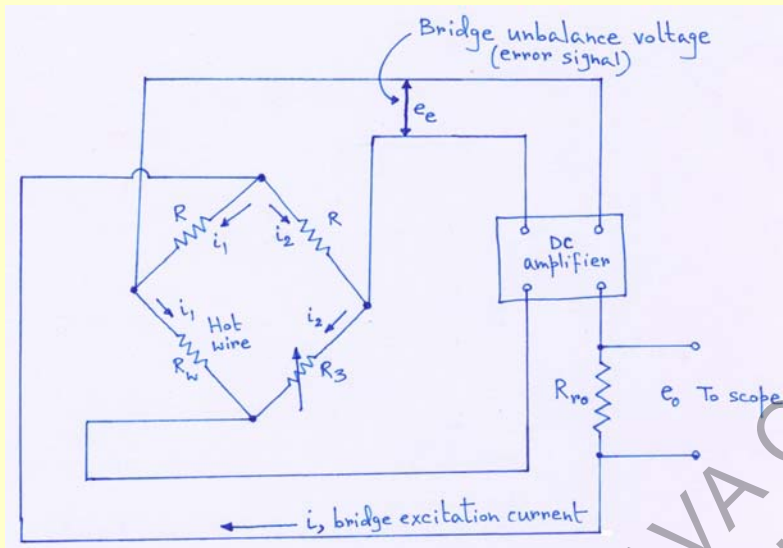
The effect of velocity on r_w :

$$\frac{r_w(s)}{v(s)} = \frac{K}{1 + s\tau} \left(\because \frac{e(s)}{v(s)} = \frac{I_m r_w(s)}{v(s)} = \frac{K}{1 + s\tau} \right)$$

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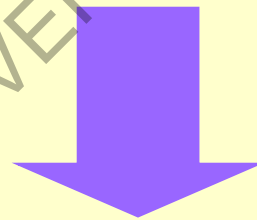
From theory of superposition, the total effect of i_1 and v on r_w :

$$(s\tau + 1)r_w(s) = \frac{Kv(s) + K_e i_1(s)}{I_m}$$

Now, a change in r_w causes a bridge unbalance voltage change as:

$$e_e(s) = \frac{I_m R_w}{R + R_{w0}} r_w(s) = -K_b r_w(s)$$

From d.c. amplifier: $i(s) = K_a e_e(s)$

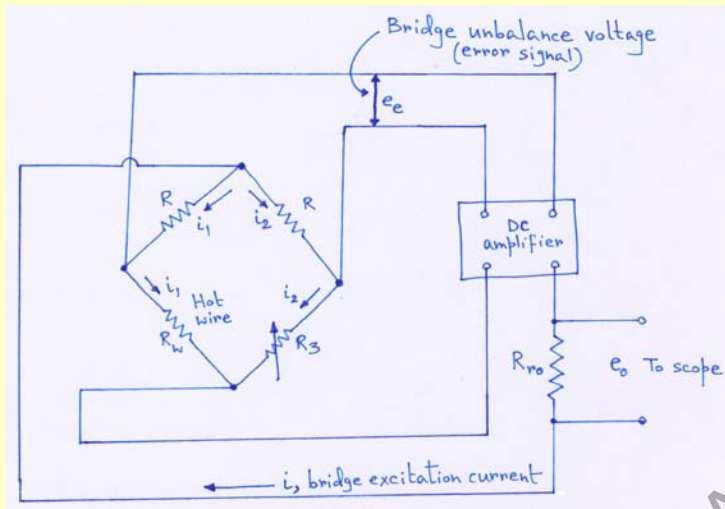


- ✓ Using these relations, a block diagram representation can be developed.

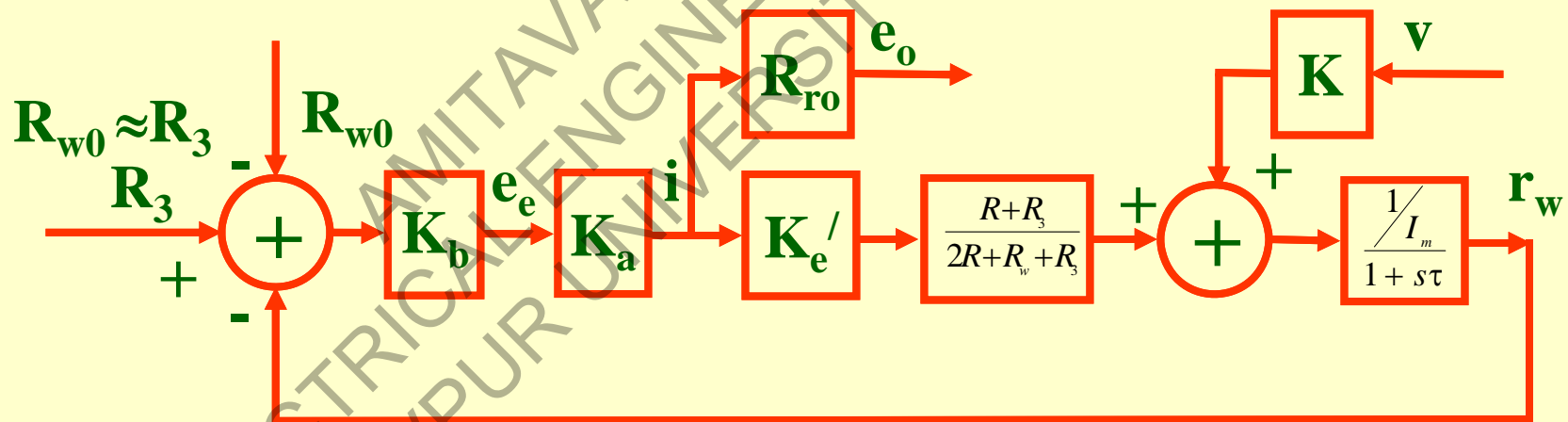
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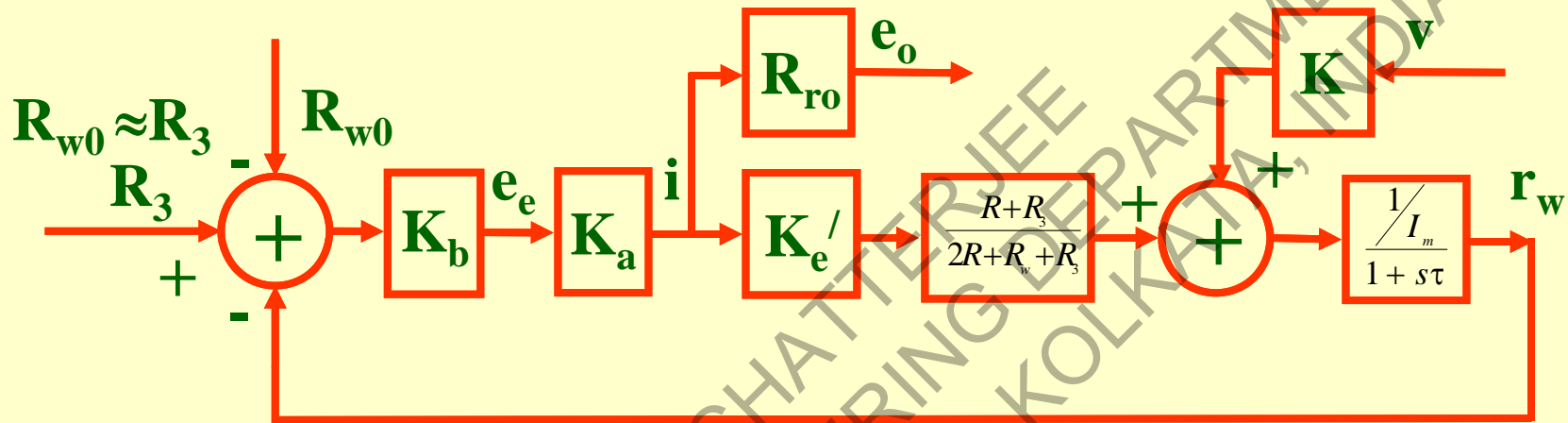
Block Diagram Representation:



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$$\frac{e_o(s)}{v(s)} = \frac{K_{ct}}{1 + s\tau_{ct}}; \quad K_{ct} = - \frac{\left(\frac{KK_b K_a R_{ro}}{I_m} \right)}{\left[1 + K_e' \left(\frac{R + R_3}{2R + R_w + R_3} \right) \cdot \frac{K_b K_a}{I_m} \right]}; \quad \tau_{ct} = \frac{\tau}{\left[1 + K_e' \left(\frac{R + R_3}{2R + R_w + R_3} \right) \cdot \frac{K_b K_a}{I_m} \right]}$$

✓ K_{ct} and τ_{ct} can be taken as constants. This is because the term containing the factor $\left(\frac{R + R_3}{2R + R_w + R_3} \right)$ also contains K_a , which is very high. The fluctuations in K_w are quite small and hence the factor $\left(\frac{R + R_3}{2R + R_w + R_3} \right)$ can be taken as (1/2).

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Comparison of CCAs and CTAs

- ✓ The feedback type CTAs provide preferable solutions, compared to CCAs.
 - ✓ In the CCAs, current must be set high enough, to heat the wire considerably above the fluid temperature.
- 
- ✓ A sudden drop in flow velocity may cause the hot wire to burn out.
 - ✓ The CTAs naturally overcome this problem, as the feedback arrangement automatically sets the wire current to maintain a safe and desired wire temperature, for every velocity.
 - ✓ The time constant of the CTAs, τ_{ct} , is always much less than τ , since an amplifier with a high gain K_a is used.

Thank You

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