

# Transformation from Rotating to Stationary Axes

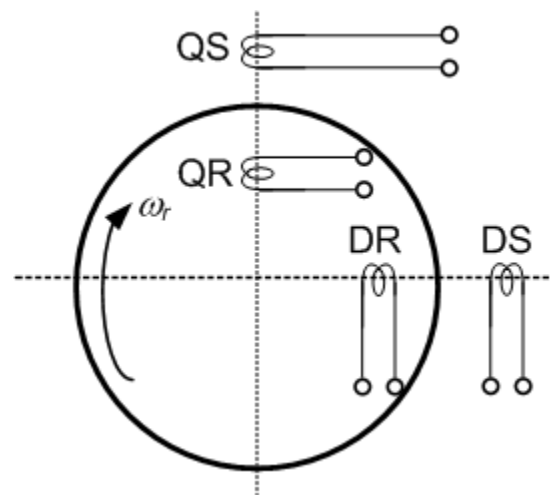
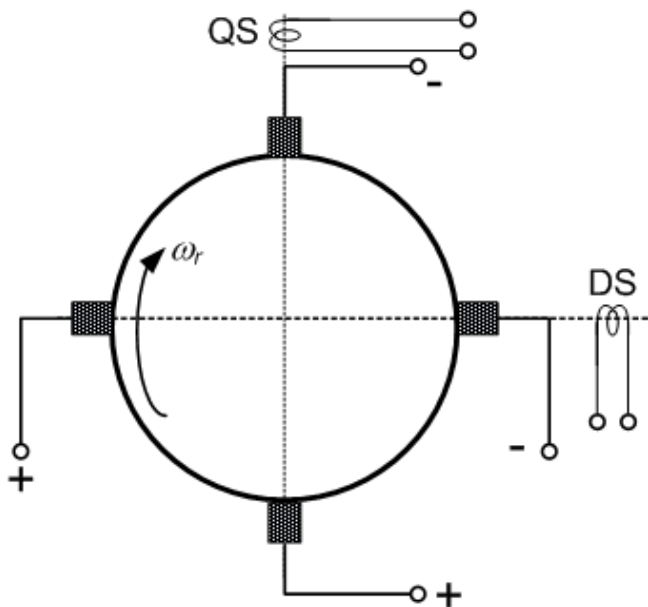
Day 9

# Why Transformation?

- **Kron's Primitive (basic) 2-pole machine**

- Two static coils in stator
- Two pseudo-stationary coils in rotor

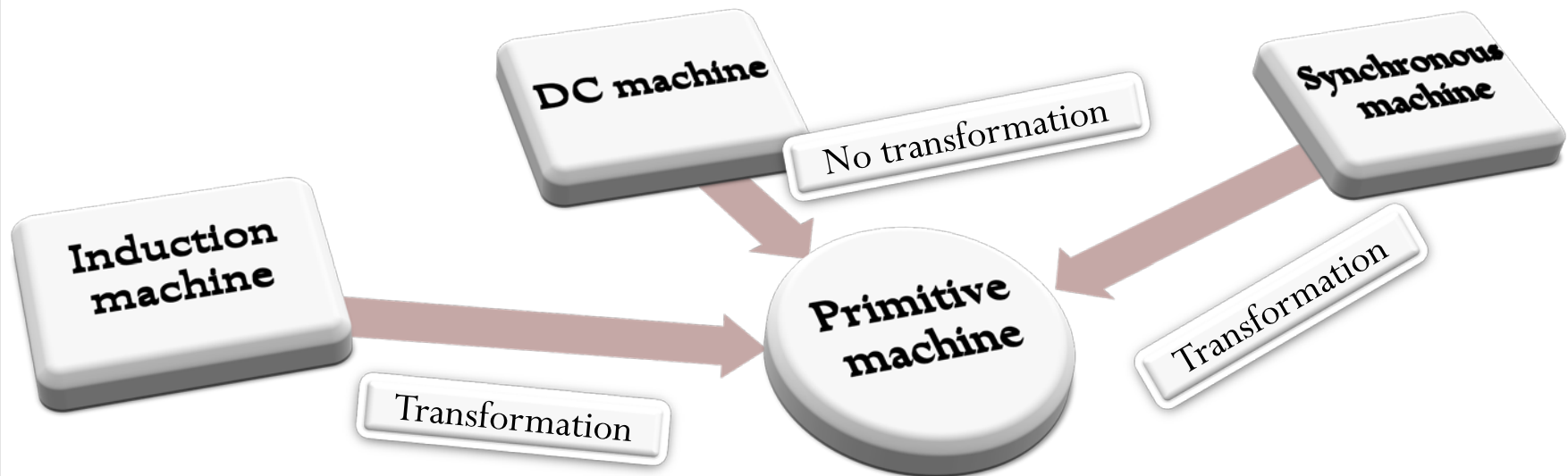
- We want to represent all rotating machines by this primitive machine structure for ease & uniformity of analysis



# What is Transformation?

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- The process of replacing one set of variables by another set of variables for equivalent representation electrical machines is called *winding transformation* or simply *transformation*.
  - Since DC machines resemble the primitive machine structure directly, no transformation is necessary
  - Polyphase machines, however, need such transformations so that they can be fit into the primitive machine model and analyzed



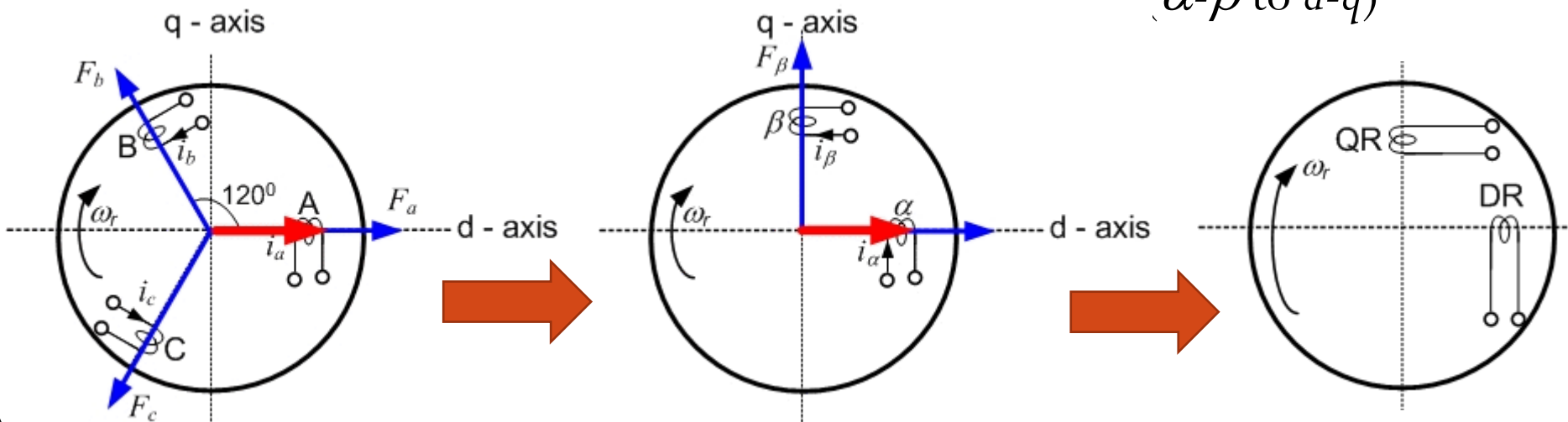
# Different Transformations in machines

Transformation from a rotating 3-phase to stationary 2-phase  
(a, b, c to d, q)

Transformation from rotating 3-phase to rotating 2-phase  
(a-b-c to  $\alpha$ - $\beta$ )



Transformation from rotating 2-phase to stationary 2-phase  
( $\alpha$ - $\beta$  to d-q)

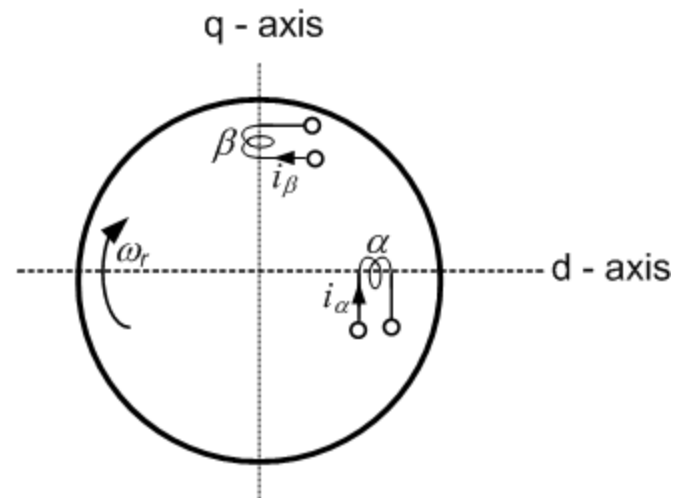
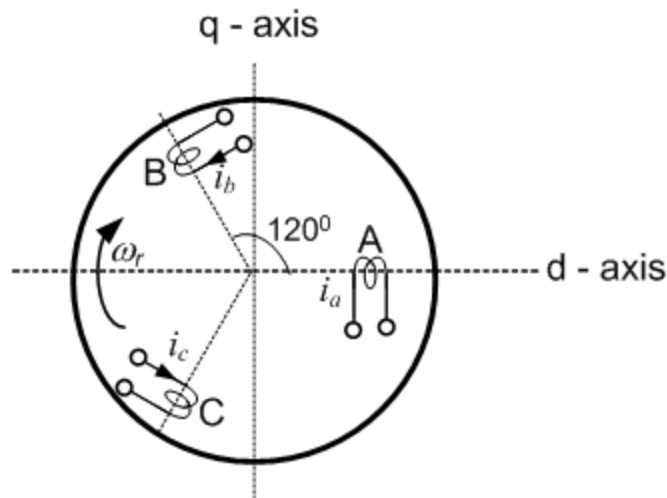


# ILOs – Day9

- Transform from 2-phase rotating axes to 2-phase stationary axes
  - Derive the transformation matrix ( $\alpha, \beta, 0$  to  $d, q, 0$ )
  - Derive the inverse transformation matrix ( $d, q, 0$  to  $\alpha, \beta, 0$ )
  
- Transform from 3-phase rotating axes to 2-phase stationary axes
  - Derive the transformation matrix ( $a, b, c$  to  $d, q, 0$ )
  - Derive the inverse transformation matrix ( $d, q, 0$  to  $a, b, c$ )

# $(\alpha, \beta, 0)$ to $(d, q, 0)$ transformation

- **Rotating to stationary axes transformation**
  - The axis of phase ' $\alpha$ ' in 2-phase machine is assumed to coincide with the axis of phase ' $A$ ' in 3-phase machine
  - Since the two rotors rotate at same speed and in the same direction, the two axes in question continue to coincide as the rotors rotate
  - Thus, the 2-phase axes  $(\alpha, \beta)$  and 3-phase axes  $(a, b, c)$  are always at rest w.r.t. each other
  - Coefficients of the transformation matrix are thus constant quantities

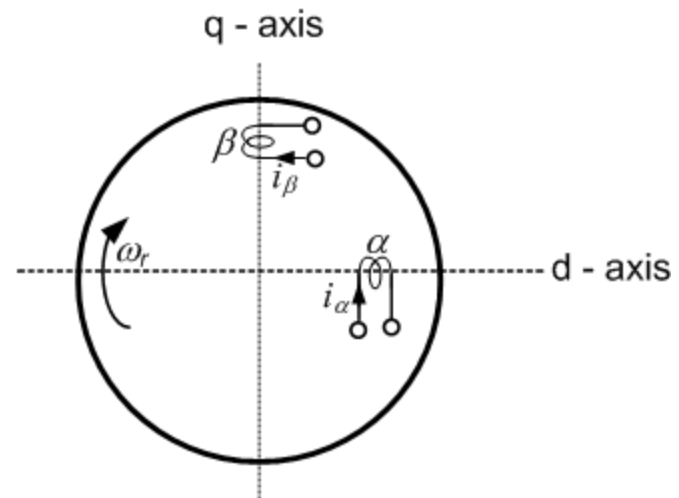
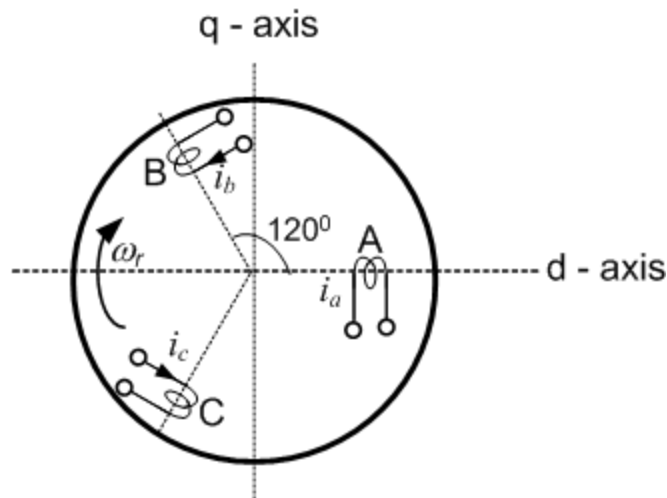


# $(\alpha, \beta, 0)$ to $(d, q, 0)$ transformation

- Rotating to stationary axes transformation

$$\begin{bmatrix} i_\alpha \\ i_\beta \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix} 1 & -\frac{1}{2} & -\frac{1}{2} \\ 0 & \frac{\sqrt{3}}{2} & -\frac{\sqrt{3}}{2} \end{bmatrix} \begin{bmatrix} i_a \\ i_b \\ i_c \end{bmatrix}$$

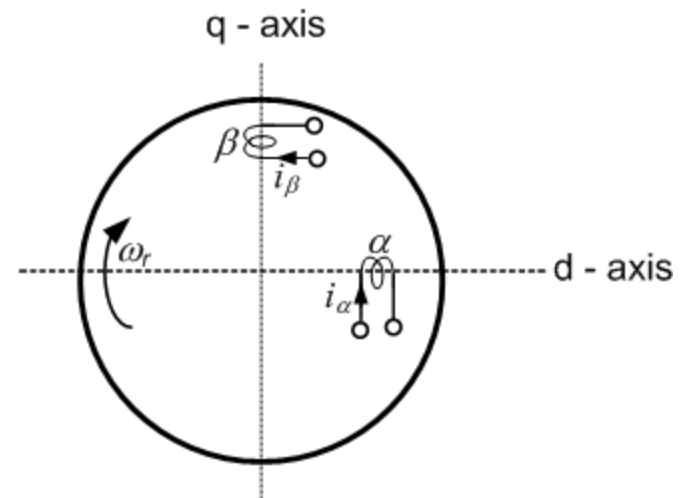
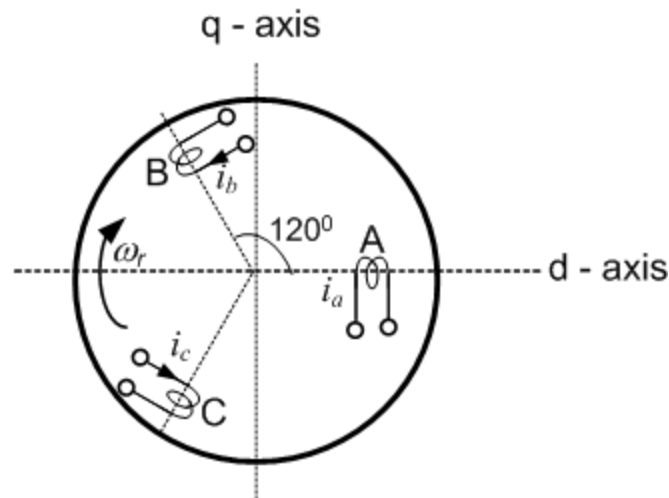
- Thus, the 2-phase axes  $(\alpha, \beta)$  and 3-phase axes  $(a, b, c)$  are always at rest w.r.t. each other
- Coefficients of the transformation matrix are thus constant quantities



# $(\alpha, \beta, 0)$ to $(d, q, 0)$ transformation

- **Rotating to stationary axes transformation**

- The 2-phase axes  $(\alpha, \beta)$  and 3-phase axes  $(a, b, c)$  are both rotating axes
- When transformation is to be done from such a rotating axis to a stationary (fixed) axis:
  - The relative position of the rotating axis varies with respect to the stationary (fixed) axis as the rotor rotates
  - The transformation matrices in such a case will contain coefficients that are function of relative positions between the rotating  $(\alpha, \beta)$  and fixed  $(d, q)$  axes



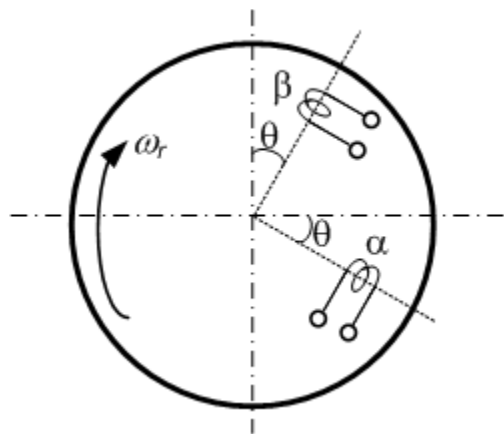


# $(\alpha, \beta, 0)$ to $(d, q, 0)$ transformation

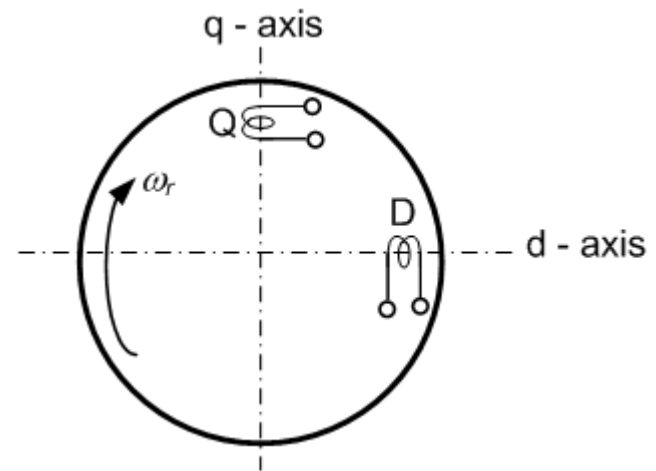
- Rotating to stationary axes transformation

- The transformation process

- The rotating coils are to be replaced by *pseudo-stationary* coils
- Zero sequence quantities are not transformed, thus the required transformation is only from  $\alpha$ - $\beta$  to  $d$ - $q$  axes
- Revolving axes on the rotor implies that they are rotating w.r.t. the stator
- Stationary axes on the rotor implies that they are fixed w.r.t. the stator (i.e. pseudo-stationary coil in rotor)



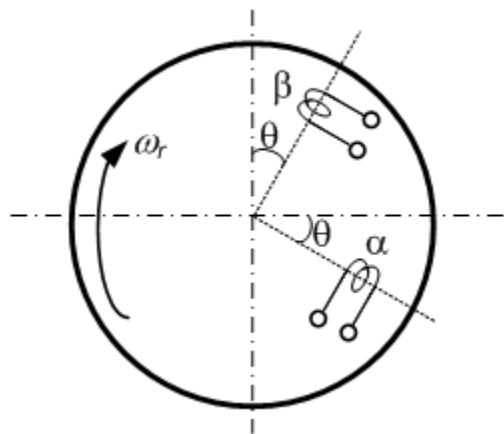
Rotating  $\alpha$ - $\beta$  axes



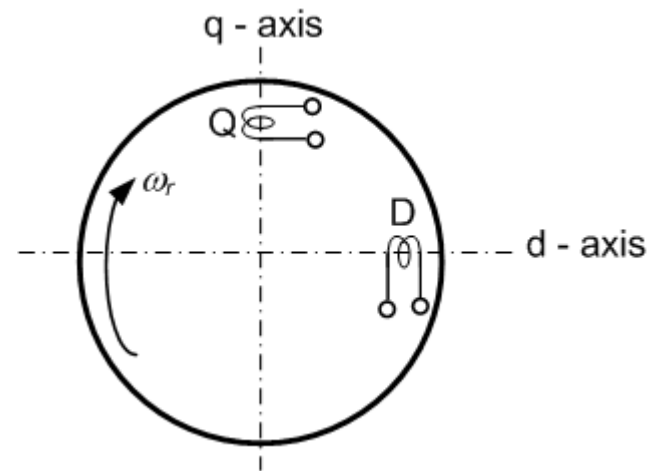
Stationary  $d$ - $q$  axes

# $(\alpha, \beta, 0)$ to $(d, q, 0)$ transformation

- Rotating to stationary axes transformation
  - The transformation process
    - Coils  $\alpha$  and  $\beta$  of the rotating winding are shown to make an angle  $\theta$  with the stationary  $d$ - $q$  axes windings
    - The angle  $\theta$  is such that at time  $t=0$ ,  $\theta=0$ , i.e. the rotating axes  $\alpha$ - $\beta$  coincide with the stationary axes  $d$ - $q$  at  $t=0$
    - At any time  $t$ , the angular displacement is  $\theta = \omega_r t$ , where  $\omega_r$  is the angular velocity



Rotating  $\alpha$ - $\beta$  axes



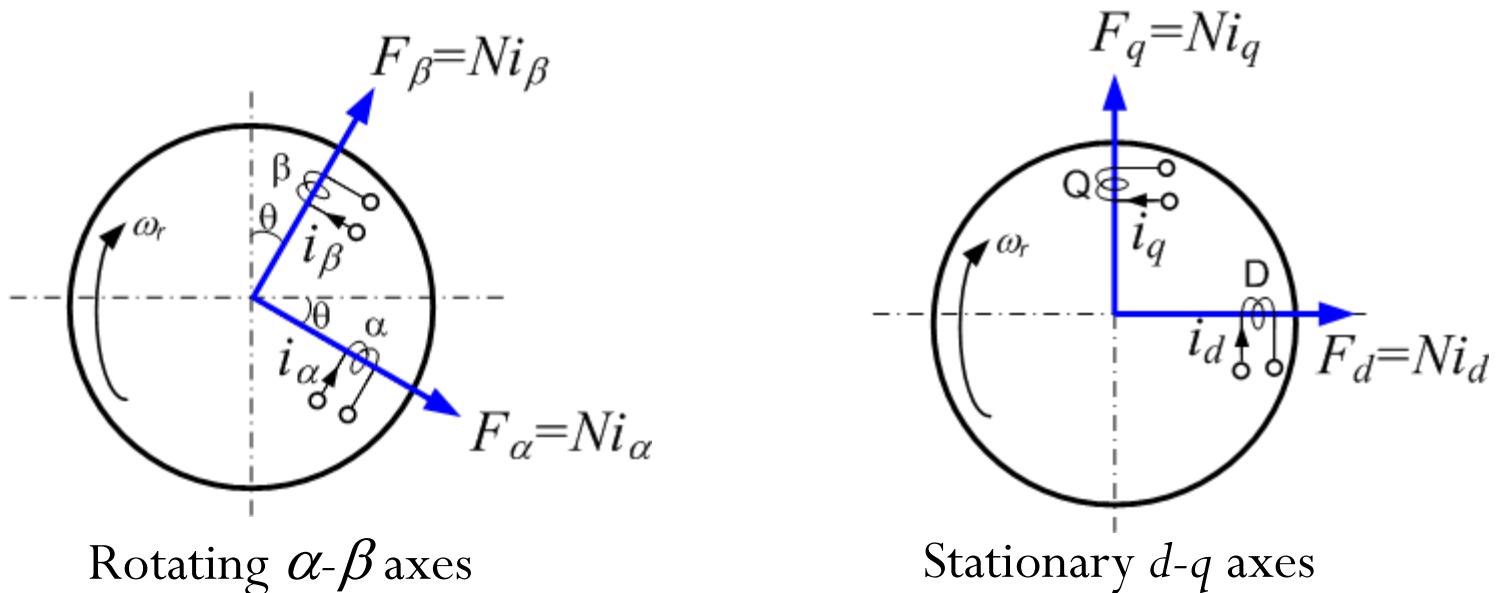
Stationary  $d$ - $q$  axes

# $(\alpha, \beta, 0)$ to $(d, q, 0)$ transformation

- Rotating to stationary axes transformation

- The transformation process

- At this instant 't', the MMF space phasors  $F_\alpha, F_\beta$  of the  $\alpha$ - $\beta$  winding and  $F_d, F_q$  of the  $d$ - $q$  winding are shown
- Assume that all the windings have same number of turns "N"



# $(\alpha, \beta, 0)$ to $(d, q, 0)$ transformation

- Rotating to stationary axes transformation

- The transformation process

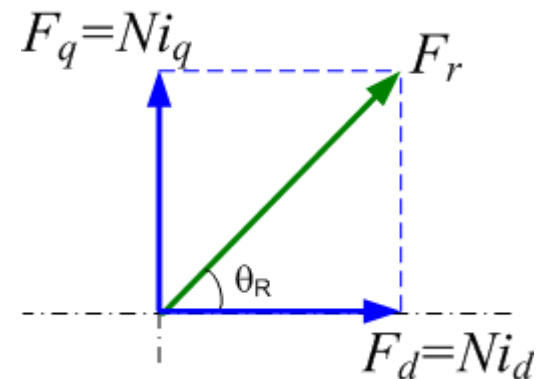
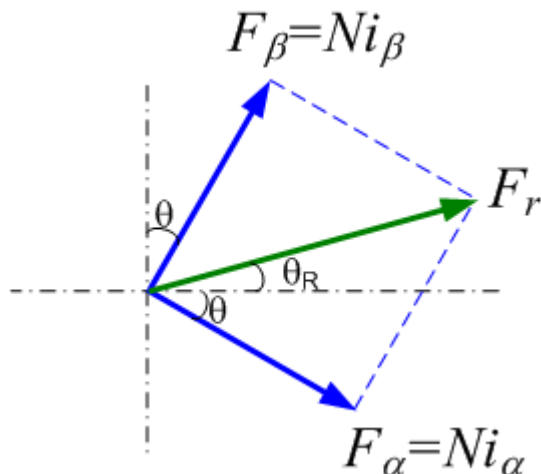
- The two MMFs and can be resolved along  $d$ - and  $q$ - axes:

$$F_d = F_\alpha \cos \theta + F_\beta \sin \theta$$

or,  $Ni_d = Ni_\alpha \cos \theta + Ni_\beta \sin \theta$

Thus,  $i_d = i_\alpha \cos \theta + i_\beta \sin \theta$

Similarly,  $i_q = -i_\alpha \sin \theta + i_\beta \cos \theta$



# $(\alpha, \beta, 0)$ to $(d, q, 0)$ transformation

- Rotating to stationary axes transformation

$$i_d = i_\alpha \cos \theta + i_\beta \sin \theta$$

$$i_q = -i_\alpha \sin \theta + i_\beta \cos \theta$$

- In matrix form:

$$\begin{bmatrix} i_d \\ i_q \end{bmatrix} = \begin{matrix} \alpha & \beta \\ d & q \end{matrix} \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} i_\alpha \\ i_\beta \end{bmatrix}$$

Let us define,  $C = \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix}$

$$\therefore C_t = \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix}$$

$$\therefore |C| = \cos^2 \theta + \sin^2 \theta = 1$$

Hence,  $C^{-1} = \frac{C_t}{|C|} = \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix}$

Thus, the inverse transformation is:

$$\begin{bmatrix} i_\alpha \\ i_\beta \end{bmatrix} = \begin{matrix} d & q \\ \alpha & \beta \end{matrix} \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} i_d \\ i_q \end{bmatrix}$$

- The MMF, flux and number of turns are same in both configurations
- Thus, induced EMF (voltage) per phase will also be same
- Hence, current and voltage will have identical transformations

# $(\alpha, \beta, 0)$ to $(d, q, 0)$ transformation

- Rotating to stationary axes transformation

- Let the currents in coils d-q axes are time-varying:  
(remember that they are at  $90^\circ$  in time & space)

$$i_d = I_m \sin(\omega t + \phi)$$

$$i_q = I_m \cos(\omega t + \phi)$$

Here  $\phi$  is any arbitrary constant phase angle

$$\begin{array}{c} \begin{array}{|c|} \hline i_d \\ \hline \end{array} \\ \begin{array}{|c|} \hline i_q \\ \hline \end{array} \end{array} = \begin{array}{cc} \alpha & \beta \\ \hline d \cos \theta & \sin \theta \\ \hline q - \sin \theta & \cos \theta \end{array} \begin{array}{|c|} \hline i_\alpha \\ \hline i_\beta \\ \hline \end{array}$$

$$\begin{array}{c} \begin{array}{|c|} \hline i_\alpha \\ \hline \end{array} \\ \begin{array}{|c|} \hline i_\beta \\ \hline \end{array} \end{array} = \begin{array}{cc} d & q \\ \hline \alpha \cos \theta & -\sin \theta \\ \hline \beta \sin \theta & \cos \theta \end{array} \begin{array}{|c|} \hline i_d \\ \hline i_q \\ \hline \end{array}$$

The equivalent currents  $i_\alpha$  and  $i_\beta$  can now be obtained using the inverse transform matrix as (note that  $\omega t = \theta$ ):

$$\begin{aligned} i_\alpha &= i_d \cos \theta - i_q \sin \theta = I_m \sin(\omega t + \phi) \cos \theta - I_m \cos(\omega t + \phi) \sin \theta \\ &= I_m [\sin(\omega t + \phi - \theta)] = I_m [\sin(\omega t + \phi - \omega t)] \\ &= I_m \sin \phi \end{aligned}$$

$$\begin{aligned} i_\beta &= i_d \sin \theta + i_q \cos \theta = I_m \sin(\omega t + \phi) \sin \theta + I_m \cos(\omega t + \phi) \cos \theta \\ &= I_m [\cos(\omega t + \phi - \theta)] = I_m [\sin(\omega t + \phi - \omega t)] \\ &= I_m \cos \phi \end{aligned}$$

# $(\alpha, \beta, 0)$ to $(d, q, 0)$ transformation

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- **Rotating to stationary axes transformation**

- Currents in  $d$ - $q$  axes coils are time varying with  $90^\circ$  phase shift and are also at space quadrature
  - They produce a rotating MMF (RMF)
- Currents in  $\alpha$ - $\beta$  axes are constant (DC currents), but the coils are at space quadrature
  - The DC currents  $i_\alpha$   $i_\beta$  can only produce a resultant stationary MMF
  - But since the coils along  $\alpha$ - $\beta$  axes physically rotate at  $\omega_r$ , the resultant MMF also rotate physically along with the rotor at the same speed  $\omega_r$
- Thus, time varying currents  $i_d$ - $i_q$  in stationary coils  $d$ - $q$  produce exactly similar RMF, rotating at same speed and in the same direction as the DC currents  $i_\alpha$ - $i_\beta$  in the rotating coils  $\alpha$ - $\beta$  produce

$$i_d = I_m \sin(\omega t + \phi)$$

$$i_q = I_m \cos(\omega t + \phi)$$

$$i_\alpha = I_m \sin \phi$$

$$i_\beta = I_m \cos \phi$$

# $(\alpha, \beta, 0)$ to $(d, q, 0)$ transformation

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- Rotating to stationary axes transformation
  - If zero sequence currents exist:

$$\begin{array}{|c|} \hline i_d \\ \hline i_q \\ \hline i_0 \\ \hline \end{array} = \begin{array}{c} d \\ q \\ 0 \end{array} \begin{array}{|c|c|c|} \hline \alpha & \beta & 0 \\ \hline \cos \theta & \sin \theta & \\ \hline -\sin \theta & \cos \theta & \\ \hline & & 1 \\ \hline \end{array} \begin{array}{|c|} \hline i_\alpha \\ \hline i_\beta \\ \hline i_0 \\ \hline \end{array}$$



# Transformation from 3-phase to 2-phase Stationary Axes

$$(a, b, c) \rightarrow (\alpha, \beta, 0) \rightarrow (d, q, 0)$$

# $(a, b, c) \rightarrow (\alpha, \beta, 0) \rightarrow (d, q, 0)$ Transformation

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- **3-phase to 2-phase rotating axes transformation**

- $(a, b, c)$  to  $(\alpha, \beta, 0)$  transformation

$$\begin{bmatrix} i_\alpha \\ i_\beta \\ i_0 \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{matrix} \alpha \\ \beta \\ 0 \end{matrix} \begin{bmatrix} \cos 0^\circ & \cos 120^\circ & \cos 240^\circ \\ \sin 0^\circ & \sin 120^\circ & \sin 240^\circ \\ \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \end{bmatrix} \begin{bmatrix} i_a \\ i_b \\ i_c \end{bmatrix}$$

- **2-phase rotating to 2-phase stationary axes transformation**

- $(\alpha, \beta, 0)$  to  $(d, q, 0)$  transformation

$$\begin{bmatrix} i_d \\ i_q \\ i_0 \end{bmatrix} = \begin{matrix} d \\ q \\ 0 \end{matrix} \begin{bmatrix} \cos \theta & \sin \theta & \\ -\sin \theta & \cos \theta & \\ & & 1 \end{bmatrix} \begin{bmatrix} i_\alpha \\ i_\beta \\ i_0 \end{bmatrix}$$

- These two transformation matrices can be combined to obtain 3-phase to 2-phase stationary axis transformation  $(a, b, c)$  to  $(\alpha, \beta, 0)$  to  $(d, q, 0)$

# $(a, b, c) \rightarrow (\alpha, \beta, 0) \rightarrow (d, q, 0)$ Transformation

- $(a, b, c)$  to  $(\alpha, \beta, 0)$  to  $(d, q, 0)$  axes transformation

$$\begin{array}{c} i_d \\ i_q \\ i_0 \end{array} = \begin{array}{c} d \\ q \\ 0 \end{array} \begin{array}{c} \alpha \quad \beta \quad 0 \\ \cos \theta \quad \sin \theta \quad \\ -\sin \theta \quad \cos \theta \quad \\ \quad \quad \quad 1 \end{array} \sqrt{\frac{2}{3}} \begin{array}{c} a \quad b \quad c \\ \cos 0^\circ \quad \cos 120^\circ \quad \cos 240^\circ \\ \sin 0^\circ \quad \sin 120^\circ \quad \sin 240^\circ \\ \frac{1}{\sqrt{2}} \quad \frac{1}{\sqrt{2}} \quad \frac{1}{\sqrt{2}} \end{array} \begin{array}{c} i_a \\ i_b \\ i_c \end{array}$$

or,

$$\begin{array}{c} i_d \\ i_q \\ i_0 \end{array} = \sqrt{\frac{2}{3}} \begin{array}{c} d \\ q \\ 0 \end{array} \begin{array}{c} a \quad b \quad c \\ \cos \theta \quad \cos(\theta - 120^\circ) \quad \cos(\theta - 240^\circ) \\ -\sin \theta \quad -\sin(\theta - 120^\circ) \quad -\sin(\theta - 240^\circ) \\ \frac{1}{\sqrt{2}} \quad \frac{1}{\sqrt{2}} \quad \frac{1}{\sqrt{2}} \end{array} \begin{array}{c} i_a \\ i_b \\ i_c \end{array}$$

*Refer appendix for  
3x3 matrix  
multiplication*

Thus, the new current  $(i_d, i_q, i_0)$  in stationary axes can be expressed in terms of actual 3-phase currents  $(i_a, i_b, i_c)$

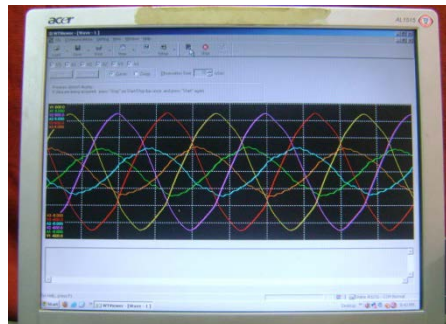
# $(a, b, c) \rightarrow (\alpha, \beta, 0) \rightarrow (d, q, 0)$ Transformation

- In case the 3-phase motor is star connected without any neutral wire (as is most commonly the case in induction motors), the zero sequence current  $i_0$  is absent, and the 3<sup>rd</sup> row will disappear from the transformation matrix:

$$\text{or, } \begin{bmatrix} i_d \\ i_q \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{matrix} d \\ q \end{matrix} \begin{array}{|c|c|c|} \hline a & b & c \\ \hline \cos \theta & \cos(\theta - 120^\circ) & \cos(\theta - 240^\circ) \\ \hline -\sin \theta & -\sin(\theta - 120^\circ) & -\sin(\theta - 240^\circ) \\ \hline \end{array} \begin{bmatrix} i_a \\ i_b \\ i_c \end{bmatrix}$$

- This gives us a transformation from ROTATING 3-phase  $(i_a, i_b, i_c)$  to STATIONARY 2-phase  $(i_d, i_q)$  transformation in stationary axes
- This technique is often used by researchers for MCSA (Motor Current Signature Analysis) for condition monitoring and fault diagnosis of induction motors

# (a, b, c) $\rightarrow$ (d, q) Transformation



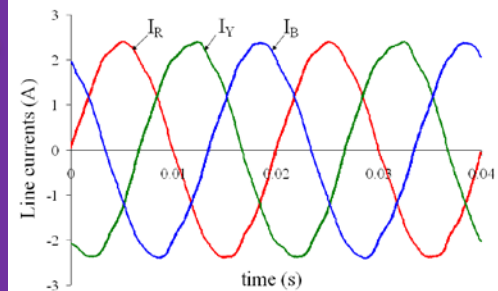
Captured 3-ph Current Signals



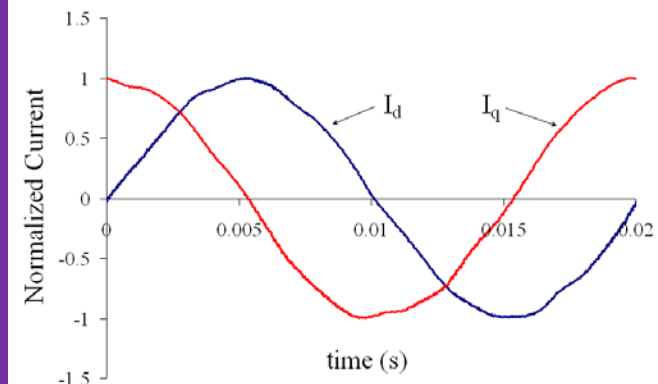
Conducted Experiments

S. Das, C. Koley, **P. Purkait**, and S. Chakravorti, "Performance of a Load-Immune Classifier for Robust Identification of Minor Faults in Induction Motor Stator Winding", Accepted for Publication in **IEEE Transactions on Dielectrics and Electrical Insulation**, 2013.

3-phase line currents



3-ph to 2-ph transformation



# Inverse Transformation

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- **(d, q, 0) to (a, b, c) axes transformation**
  - Expressing 3-phase currents ( $i_a, i_b, i_c$ ) in terms of the equivalent stationary axes currents ( $i_d, i_q, i_0$ )

$$\begin{bmatrix} i_a \\ i_b \\ i_c \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{array}{c} a \\ b \\ c \end{array} \begin{array}{|c|c|c|} \hline d & q & 0 \\ \hline \cos \theta & -\sin \theta & \frac{1}{\sqrt{2}} \\ \hline \cos(\theta - 120^\circ) & -\sin(\theta - 120^\circ) & \frac{1}{\sqrt{2}} \\ \hline \cos(\theta - 240^\circ) & -\sin(\theta - 240^\circ) & \frac{1}{\sqrt{2}} \\ \hline \end{array} \begin{array}{|c|} \hline i_d \\ \hline i_q \\ \hline i_0 \\ \hline \end{array}$$

# $(a, b, c) \rightarrow (d, q, 0)$ Transformation

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- Similar transformation could be achieved for phase **voltages** as well
- Like  $i_a, i_b, i_c$  are related to  $i_d, i_q$
- Similarly,  $v_a, v_b, v_c$  are related to  $v_d, v_q$
- These relationships between the 3-phase variables  $(a, b, c)$  and 2-phase variables  $(d, q)$  are called **Park's Transformation**
- The 3-phase coils  $(a, b, c)$  and the 2-phase coils  $(\alpha, \beta)$  are phase windings on the rotor that actually rotate along with the armature
  - Rotating w.r.t stator, but static w.r.t rotor
- On the other hand, the  $(d, q)$  coils are stationary w.r.t the stator
  - These are pseudo-stationary coils and hence involve the variable angular position term  $\theta$  in the transformation matrix

# (a, b, c) $\rightarrow$ (d, q, 0) Transformation

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- **Physical concept of Park's Transformation (rotating 3-phase to stationary 2-phase)**

- Assume that the 3-phase currents  $i_a, i_b, i_c$  are given by:

$$i_a = I_m \cos(\omega t + \alpha)$$

$$i_b = I_m \cos(\omega t + \alpha - 120^\circ)$$

$$i_c = I_m \cos(\omega t + \alpha - 240^\circ)$$

- Here  $I_m$  is the maximum value of armature current and  $\alpha$  is the time phase angle of  $i_a$  w.r.t the time origin at  $t=0$

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Park's transformation matrices

$$\begin{bmatrix} i_d \\ i_q \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{matrix} d \\ q \end{matrix} \begin{array}{|c|c|c|} \hline a & b & c \\ \hline \cos \theta & \cos(\theta - 120^\circ) & \cos(\theta - 240^\circ) \\ \hline -\sin \theta & -\sin(\theta - 120^\circ) & -\sin(\theta - 240^\circ) \\ \hline \end{array} \begin{bmatrix} i_a \\ i_b \\ i_c \end{bmatrix}$$



# (a, b, c) → (d, q, 0) Transformation

- Physical concept of Park's Transformation (rotating 3-phase to stationary 2-phase)**

- Using Park's transformation:

$$i_d = \sqrt{\frac{2}{3}} [i_a \cos \theta + i_b \cos(\theta - 120^\circ) + i_c \cos(\theta - 240^\circ)]$$

Substituting  $\theta = \omega t$ :

$$\begin{aligned} i_d &= \sqrt{\frac{2}{3}} I_m [\cos \omega t \cos(\omega t + \alpha) + \cos(\omega t - 120^\circ) \cos(\omega t + \alpha - 120^\circ) + \cos(\omega t - 240^\circ) \cos(\omega t + \alpha - 240^\circ)] \\ &= \sqrt{\frac{2}{3}} I_m \frac{1}{2} [\cos(2\omega t + \alpha) + \cos \alpha + \cos(2\omega t + \alpha - 240^\circ) + \cos \alpha + \cos(2\omega t + \alpha - 480^\circ) + \cos \alpha] \\ &= \sqrt{\frac{2}{3}} I_m \frac{1}{2} [\cos(2\omega t + \alpha) + \cos(2\omega t + \alpha - 240^\circ) + \cos(2\omega t + \alpha - 120^\circ) + 3 \cos \alpha] \end{aligned}$$

$$i_a = I_m \cos(\omega t + \alpha)$$

$$i_b = I_m \cos(\omega t + \alpha - 120^\circ)$$

$$i_c = I_m \cos(\omega t + \alpha - 240^\circ)$$

$$\cos A \cos B = \frac{1}{2} \cos(A - B) + \frac{1}{2} \cos(A + B)$$

Park's transformation matrices

$$\begin{bmatrix} i_d \\ i_q \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{matrix} d \\ q \end{matrix} \begin{array}{|c|c|c|} \hline a & b & c \\ \hline \cos \theta & \cos(\theta - 120^\circ) & \cos(\theta - 240^\circ) \\ \hline -\sin \theta & -\sin(\theta - 120^\circ) & -\sin(\theta - 240^\circ) \\ \hline \end{array} \begin{matrix} i_a \\ i_b \\ i_c \end{matrix}$$

# (a, b, c) → (d, q, 0) Transformation

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- **Physical concept of Park's Transformation (rotating 3-phase to stationary 2-phase)**

$$i_d = \sqrt{\frac{2}{3}} I_m \frac{1}{2} [\cos(2\omega t + \alpha) + \cos(2\omega t + \alpha - 240^\circ) + \cos(2\omega t + \alpha - 120^\circ) + 3\cos\alpha]$$
$$i_a = I_m \cos(\omega t + \alpha)$$
$$i_b = I_m \cos(\omega t + \alpha - 120^\circ)$$
$$i_c = I_m \cos(\omega t + \alpha - 240^\circ)$$

For a balanced 3-phase system:

$$\cos(2\omega t + \alpha) + \cos(2\omega t + \alpha - 240^\circ) + \cos(2\omega t + \alpha - 120^\circ) = 0$$

$$\text{Thus: } i_d = \sqrt{\frac{2}{3}} I_m \frac{1}{2} [3\cos\alpha] = \sqrt{\frac{2}{3}} I_m \frac{3}{2} \cos\alpha = \sqrt{\frac{3}{2}} I_m \cos\alpha$$

Similarly, it can be shown that:

$$i_q = \sqrt{\frac{3}{2}} I_m \sin\alpha$$

- The two currents  $i_d$  and  $i_q$  are thus not time-varying, i.e. they are DC currents
- But still they produce RMF due to physical rotation of the rotor
- This RMF has the same speed and direction as that produced by the three time varying currents  $i_a$ ,  $i_b$ , and  $i_c$

# Stator winding Transformation

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- In addition to rotor, the stator may also have 1-phase, 2-phase, or 3-phase winding
  - If the stator has a 1-phase winding, it is taken along  $d$ -axis
  - If the stator has 2-phase windings, they are taken along  $d$ - $q$  axes
  - If the stator has 3-phase windings, transformations need to be done to convert from 3-phase axes  $(a, b, c)$  to  $(\alpha, \beta)$  or  $(d, q)$  axes
- Since the stator coil axes are always stationary w.r.t. the stator and its winding, coefficients of the transformation matrix are always constant