

# Chapter 3

## Transient Analysis of Synchronous Machines

Day 17

# ILOs – Day17

- Use transformation matrix of generalized theory of synchronous machine to develop the expressions for transient 3-phase currents in alternators due to short circuit faults
- Also plot these transient currents

# Transient currents in synchronous generator

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- **Sudden short circuit at alternator 3-phase output terminals**
  - Expressions for armature d-axis, armature q-axis, and field currents

$$i_d(t) = \frac{v_{q0}}{X_d'} [1 - \cos \omega t]$$

$$i_q(t) = \frac{v_{q0}}{X_q} \sin \omega t$$

$$i_f(t) = I_{f0} \left[ \frac{X_d}{X_d'} - \left( \frac{X_d}{X_d'} - 1 \right) \cos \omega t \right]$$

# Transient currents in synchronous generator

- **Sudden short circuit at alternator 3-phase output terminals**
  - Take help of the transformation matrix

$$i_d(t) = \frac{v_{q0}}{X_d'} [1 - \cos \omega t]$$

$$i_q(t) = \frac{v_{q0}}{X_q} \sin \omega t$$

$$i_f(t) = I_{f0} \left[ \frac{X_d}{X_d'} - \left( \frac{X_d}{X_d'} - 1 \right) \cos \omega t \right]$$

$$\begin{bmatrix} i_a \\ i_b \\ i_c \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{matrix} a & d & q & 0 \\ b & \cos(\theta - 120^\circ) & -\sin(\theta - 120^\circ) & \frac{1}{\sqrt{2}} \\ c & \cos(\theta - 240^\circ) & -\sin(\theta - 240^\circ) & \frac{1}{\sqrt{2}} \end{matrix} \begin{bmatrix} i_d \\ i_q \\ i_0 \end{bmatrix}$$

*Refer to Chapter 1,  
Day 9: Rotating to  
Stationary axis  
transformation*

- For phase  $a$  (neglecting zero sequence current)

$$i_a = \sqrt{\frac{2}{3}} [i_d \cos \theta - i_q \sin \theta]$$

# Transient currents in synchronous generator

- **Sudden short circuit at alternator 3-phase output terminals**
  - Take help of the transformation matrix

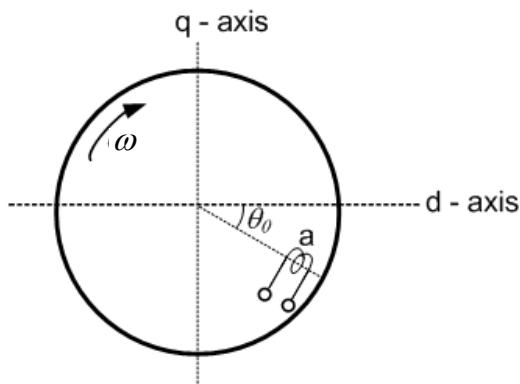
$$i_d(t) = \frac{v_{q0}}{X_d'} [1 - \cos \omega t]$$

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$$i_f(t) = I_{f0} \left[ \frac{X_d}{X_d'} - \left( \frac{X_d}{X_d'} - 1 \right) \cos \omega t \right]$$

$$i_a = \sqrt{\frac{2}{3}} [i_d \cos \theta - i_q \sin \theta]$$

- At the instant of short circuit, let the axis of phase  $a$  makes an angle  $\theta_0$  with the d-axis



# Transient currents in synchronous generator

- **Sudden short circuit at alternator 3-phase output terminals**
  - Take help of the transformation matrix

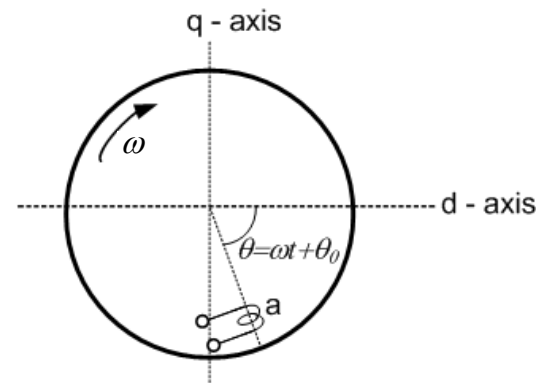
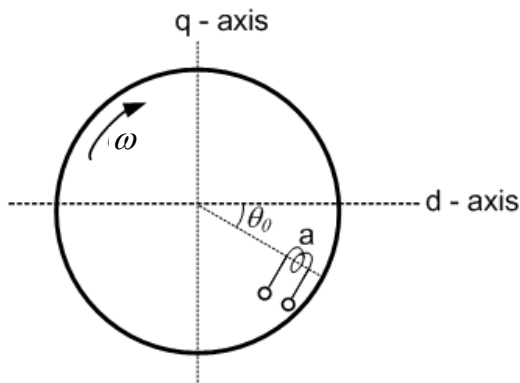
$$i_d(t) = \frac{v_{q0}}{X_d'} [1 - \cos \omega t]$$

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$$i_a = \sqrt{\frac{2}{3}} [i_d \cos \theta - i_q \sin \theta]$$

- At the instant of short circuit, let the axis of phase  $a$  makes an angle  $\theta_0$  with the  $d$ -axis
- After time  $t$  sec, the angle  $\theta$  between  $a$  phase and  $d$ -axis is given by:  $\theta = \omega t + \theta_0$



# Transient currents in synchronous generator

- **Sudden short circuit at alternator 3-phase output terminals**
  - Take help of the transformation matrix

$$i_d(t) = \frac{v_{q0}}{X_d'} [1 - \cos \omega t]$$

$$i_q(t) = \frac{v_{q0}}{X_q} \sin \omega t$$

$$i_f(t) = I_{f0} \left[ \frac{X_d}{X_d'} - \left( \frac{X_d}{X_d'} - 1 \right) \cos \omega t \right]$$

$$i_a = \sqrt{\frac{2}{3}} [i_d \cos \theta - i_q \sin \theta] \quad \theta = \omega t + \theta_0$$

Putting the values of  $i_d$ ,  $i_q$  and  $\theta$  in the expression for  $i_a$ :

$$\Rightarrow i_a = \sqrt{\frac{2}{3}} \left[ \frac{v_{q0}}{X_d'} (1 - \cos \omega t) \cos(\omega t + \theta_0) - \frac{v_{q0}}{X_q} \sin \omega t \sin(\omega t + \theta_0) \right]$$

$$\Rightarrow i_a = \sqrt{\frac{2}{3}} \left[ \frac{v_{q0}}{X_d'} \cos(\omega t + \theta_0) - \frac{v_{q0}}{X_d'} \cos \omega t \cos(\omega t + \theta_0) - \frac{v_{q0}}{X_q} \sin \omega t \sin(\omega t + \theta_0) \right]$$

# Transient currents in synchronous generator

- Sudden short circuit at alternator 3-phase output terminals

$$i_a = \sqrt{\frac{2}{3}} \left[ \frac{v_{q0}}{X_d'} \cos(\omega t + \theta_0) - \frac{v_{q0}}{X_d'} \cos \omega t \cos(\omega t + \theta_0) - \frac{v_{q0}}{X_q} \sin \omega t \sin(\omega t + \theta_0) \right]$$

- Take help of the trigonometric identities

$$\cos A \cos B = \frac{1}{2} [\cos(A - B) + \cos(A + B)]$$

$$\sin A \sin B = \frac{1}{2} [\cos(A - B) - \cos(A + B)]$$

$$i_a = \sqrt{\frac{2}{3}} \left[ \frac{v_{q0}}{X_d'} \cos(\omega t + \theta_0) - \frac{v_{q0}}{X_d'} \times \frac{1}{2} [\cos(\omega t - \omega t - \theta_0) + \cos(\omega t + \omega t + \theta_0)] \right. \\ \left. - \frac{v_{q0}}{X_q} \times \frac{1}{2} [\cos(\omega t - \omega t - \theta_0) - \cos(\omega t + \omega t + \theta_0)] \right]$$

$$\Rightarrow i_a = \sqrt{\frac{2}{3}} \left[ \frac{v_{q0}}{X_d'} \cos(\omega t + \theta_0) - \frac{v_{q0}}{X_d'} \times \frac{1}{2} [\cos \theta_0 + \cos(2\omega t + \theta_0)] \right. \\ \left. - \frac{v_{q0}}{X_q} \times \frac{1}{2} [\cos \theta_0 - \cos(2\omega t + \theta_0)] \right]$$



# Transient currents in synchronous generator

- **Sudden short circuit at alternator 3-phase output terminals**

$$i_a = \sqrt{\frac{2}{3}} \left[ \begin{array}{l} \frac{v_{q0}}{X_d'} \cos(\omega t + \theta_0) - \frac{v_{q0}}{X_d'} \times \frac{1}{2} [\cos \theta_0 + \cos(2\omega t + \theta_0)] \\ - \frac{v_{q0}}{X_q} \times \frac{1}{2} [\cos \theta_0 - \cos(2\omega t + \theta_0)] \end{array} \right]$$

$$\Rightarrow i_a = \sqrt{\frac{2}{3}} \left[ \frac{v_{q0}}{X_d'} \cos(\omega t + \theta_0) - \frac{v_{q0}}{2} \left( \frac{1}{X_d'} + \frac{1}{X_q} \right) \cos \theta_0 - \frac{v_{q0}}{2} \left( \frac{1}{X_d'} - \frac{1}{X_q} \right) \cos(2\omega t + \theta_0) \right]$$

- From Day 16 lesson, we know that before the short circuit i.e. at  $t = 0 -$   
 $v_{d0} = 0$  and  $v_{q0} = M_d \omega I_{f0}$
- Now, d-axis voltage being zero, thus, at no-load, the entire 3-phase induced EMF ( $\sqrt{3}E_{f0}$ ) must be fully represented by the q-axis voltage in armature

$$\therefore v_{q0} = M_d \omega I_{f0} = \sqrt{3}E_{f0} \quad \text{Where } E_{f0} = \text{per phase no-load induced EMF}$$

# Transient currents in synchronous generator

- Sudden short circuit at alternator 3-phase output terminals

$$i_a = \sqrt{\frac{2}{3}} \left[ \frac{v_{q0}}{X_d'} \cos(\omega t + \theta_0) - \frac{v_{q0}}{2} \left( \frac{1}{X_d'} + \frac{1}{X_q} \right) \cos \theta_0 - \frac{v_{q0}}{2} \left( \frac{1}{X_d'} - \frac{1}{X_q} \right) \cos(2\omega t + \theta_0) \right]$$

$$v_{q0} = \sqrt{3} E_{f0}$$

$$\Rightarrow i_a = \frac{\sqrt{2} E_{f0}}{X_d'} \cos(\omega t + \theta_0) - \frac{\sqrt{2} E_{f0}}{2} \left( \frac{1}{X_d'} + \frac{1}{X_q} \right) \cos \theta_0 - \frac{\sqrt{2} E_{f0}}{2} \left( \frac{1}{X_d'} - \frac{1}{X_q} \right) \cos(2\omega t + \theta_0)$$

- The other two line currents  $i_b$  and  $i_c$  can be simply obtained by replacing  $\theta_0$  in the above equation by  $(\theta_0 - 120^\circ)$  and  $(\theta_0 - 240^\circ)$  respectively

# Transient currents in synchronous generator

- Sudden short circuit at alternator 3-phase output terminals

$$i_a = \frac{\sqrt{2}E_{f0}}{X_{d'}} \cos(\omega t + \theta_0) - \frac{\sqrt{2}E_{f0}}{2} \left( \frac{1}{X_{d'}} + \frac{1}{X_q} \right) \cos \theta_0 - \frac{\sqrt{2}E_{f0}}{2} \left( \frac{1}{X_{d'}} - \frac{1}{X_q} \right) \cos(2\omega t + \theta_0)$$

Fundamental  
frequency component

DC component

2<sup>nd</sup> harmonic component

The transient line currents thus consist of:

- i) A fundamental frequency AC component (1<sup>st</sup> term)
- ii) A DC component (2<sup>nd</sup> term) – independent of time  $t$
- iii) A 2<sup>nd</sup> harmonic (double the fundamental frequency) AC component (3<sup>rd</sup> term)

Magnitude of all three components depend on the pre-fault excitation voltage  $E_{f0}$ , i.e. the pre-fault no-load induced EMF, i.e. the pre-fault field current  $I_{f0}$

# Transient currents in synchronous generator

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- **Sudden short circuit at alternator 3-phase output terminals**

$$i_a = \frac{\sqrt{2}E_{f0}}{X_d'} \cos(\omega t + \theta_0) - \frac{\sqrt{2}E_{f0}}{2} \left( \frac{1}{X_d'} + \frac{1}{X_q} \right) \cos \theta_0 - \frac{\sqrt{2}E_{f0}}{2} \left( \frac{1}{X_d'} - \frac{1}{X_q} \right) \cos(2\omega t + \theta_0)$$

## Additional observations

- a) Magnitude of the fundamental component (1<sup>st</sup> term) depends on the  $d$ -axis transient reactance  $X_d'$
- b) Magnitude of the DC component (2<sup>nd</sup> term), in addition to the  $d$ - and  $q$ -axis reactances, depends on  $\theta_0$  i.e. the instant at which the short circuit occurs
- c) Magnitude of the 2<sup>nd</sup> harmonic component (3<sup>rd</sup> term) depends on the term  $\left( \frac{1}{X_d'} - \frac{1}{X_q} \right)$  which is called *transient saliency* (due to difference in  $d$ - and  $q$ -axis reactances)

# Transient currents in synchronous generator

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- **Sudden short circuit at alternator 3-phase output terminals**

$$i_a = \frac{\sqrt{2}E_{f0}}{X_d'} \cos(\omega t + \theta_0) - \frac{\sqrt{2}E_{f0}}{2} \left( \frac{1}{X_d'} + \frac{1}{X_q} \right) \cos \theta_0 - \frac{\sqrt{2}E_{f0}}{2} \left( \frac{1}{X_d'} - \frac{1}{X_q} \right) \cos(2\omega t + \theta_0)$$

## Some more observations

If the short circuit occurs at  $\theta_0 = 90^\circ$ , i.e. at the instant when the coil axis is perpendicular to  $d$ -axis, then DC component of current ( $2^{\text{nd}}$  term) is zero

However, DC components will still be in the other two line currents  $i_b$  and  $i_c$  since they are with  $120^\circ$  and  $240^\circ$  phase displacement from  $i_a$

# Transient currents in synchronous generator

- Sudden short circuit at alternator 3-phase output terminals

$$i_d(t) = \frac{v_{q0}}{X_d'} [1 - \cos \omega t]$$

DC component

Fundamental frequency component

$$i_a = \frac{\sqrt{2}E_{f0}}{X_d'} \cos(\omega t + \theta_0) - \frac{\sqrt{2}E_{f0}}{2} \left( \frac{1}{X_d'} + \frac{1}{X_q} \right) \cos \theta_0 - \frac{\sqrt{2}E_{f0}}{2} \left( \frac{1}{X_d'} - \frac{1}{X_q} \right) \cos(2\omega t + \theta_0)$$

Fundamental frequency component

DC component

2<sup>nd</sup> harmonic component

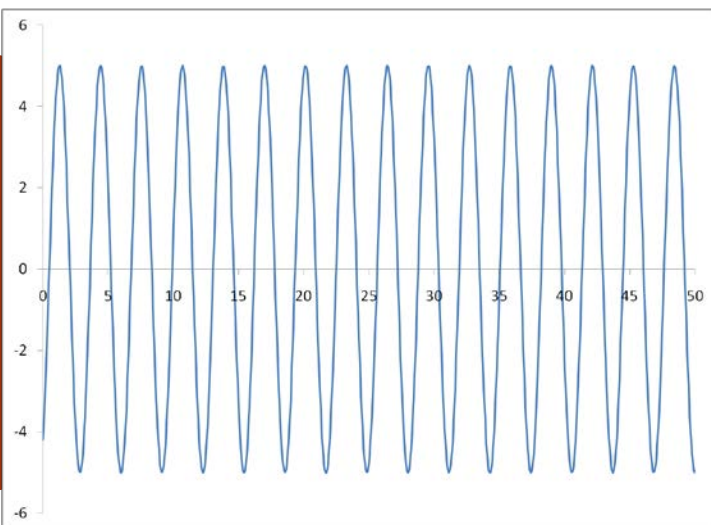
## Some interesting observations of $d$ - $q$ to $a$ - $b$ - $c$ transformation

- DC component of  $i_d(t)$  is transformed to fundamental frequency component of  $i_a(t)$
- Fundamental frequency component of  $i_d(t)$  is transformed to DC and 2<sup>nd</sup> harmonic components of  $i_a(t)$

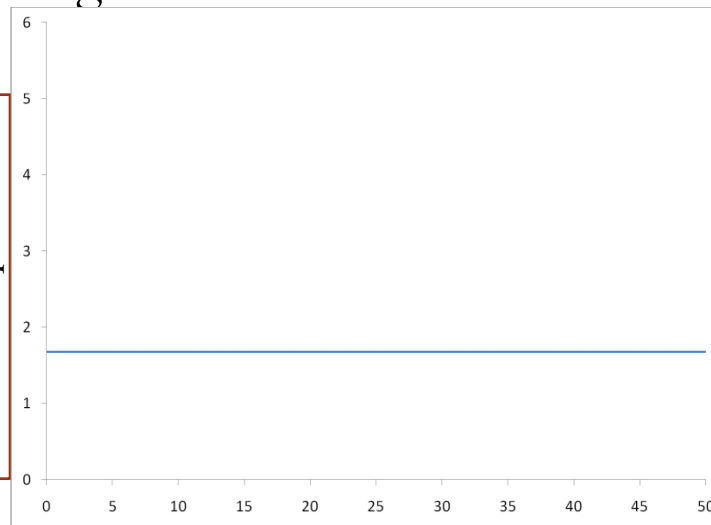
# Transient currents in synchronous generator

- Plot of transient line current: Resistances neglected

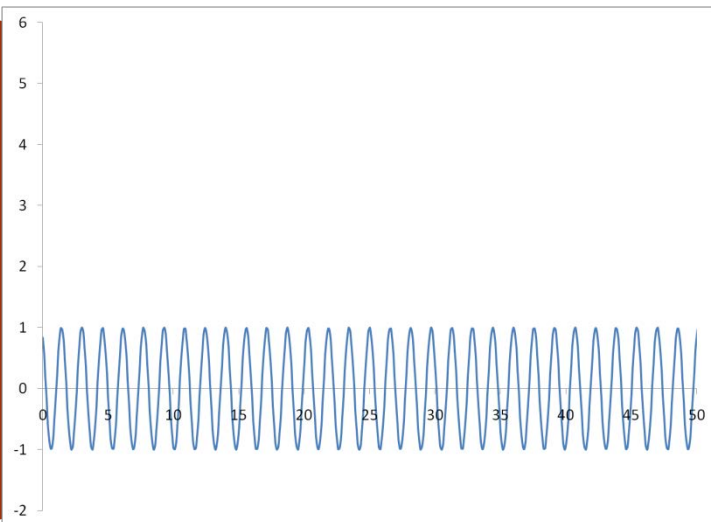
Fundamental frequency component



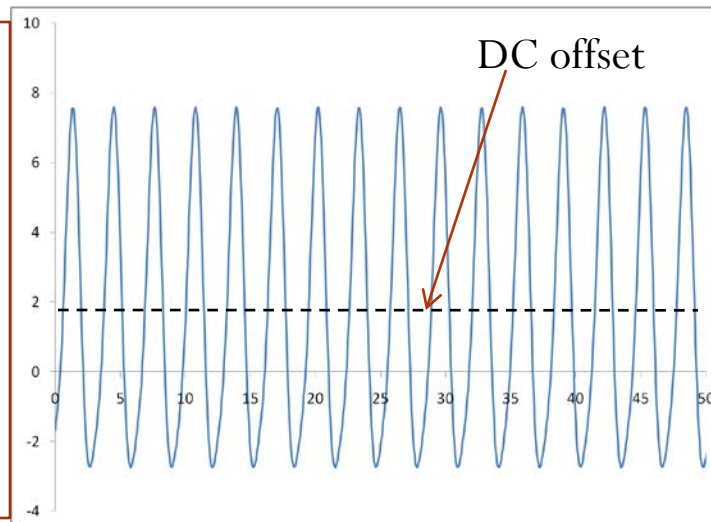
DC component



2<sup>nd</sup> harmonic component



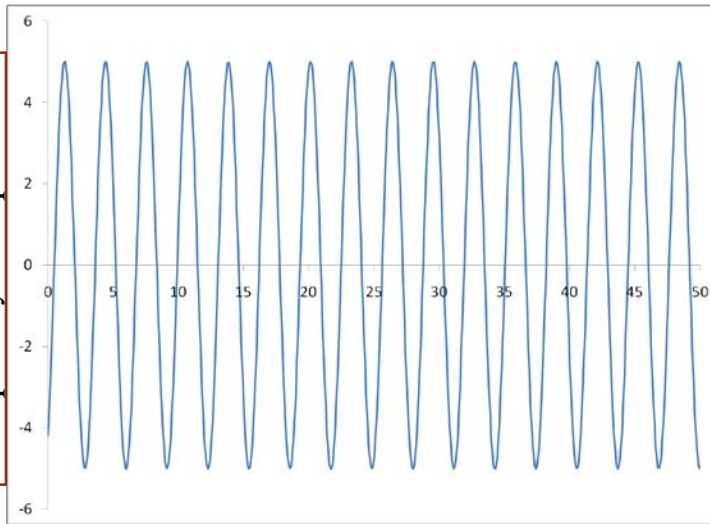
Total current  $i_a(t)$



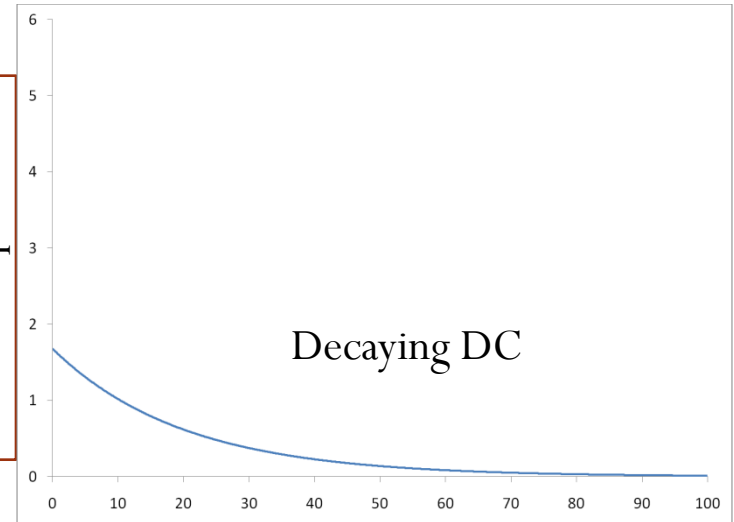
# Transient currents in synchronous generator

- Plot of transient line current: Resistances **not** neglected (DC will decay)

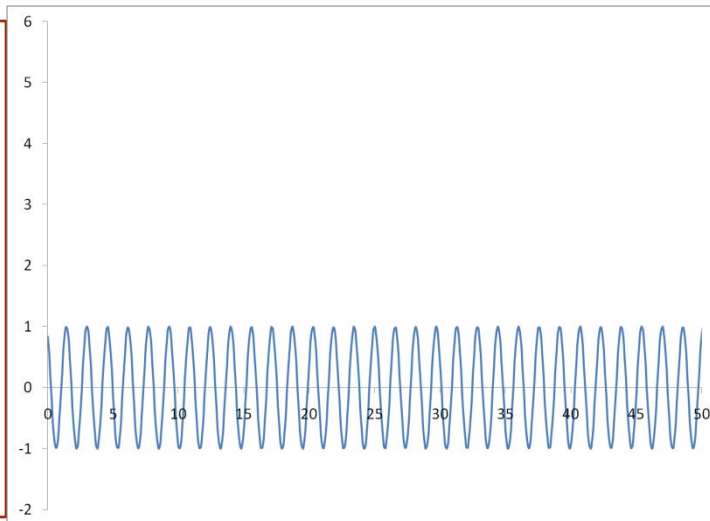
Fundamental frequency component



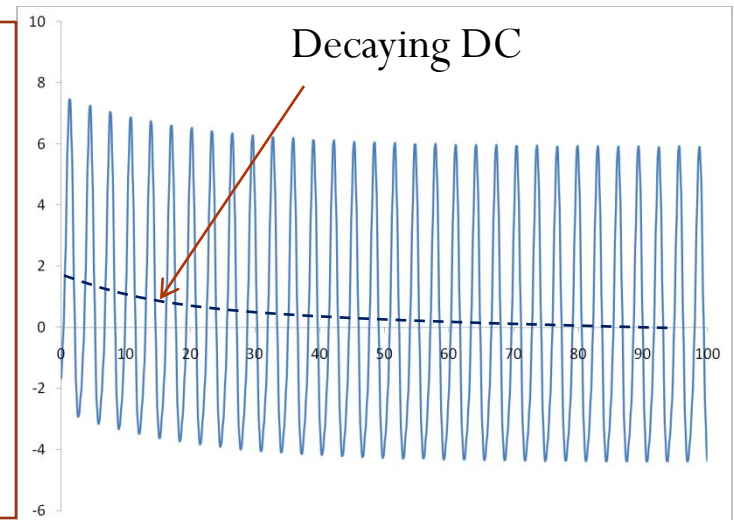
DC component



2<sup>nd</sup> harmonic component



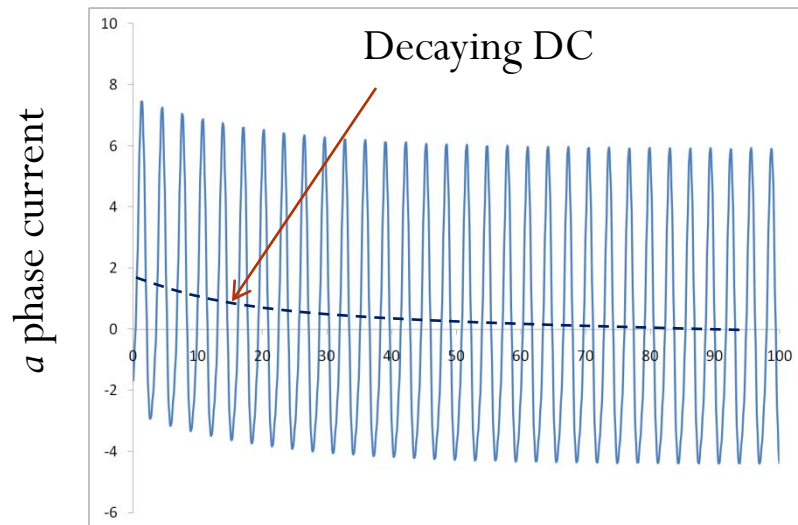
Total current  $i_a(t)$





# Transient currents in synchronous generator

- Plot of transient line current: Resistances **not** neglected (DC will decay)



*b* phase current and *c* phase currents will be displaced from *a* phase current by  $120^\circ$  and  $240^\circ$  respectively (replace  $\theta_0$  in the equation by  $(\theta_0 - 120^\circ)$  and  $(\theta_0 - 240^\circ)$  respectively)

