Ref. Ex-ME/5/T/322/2019

Bachelor of Engineering(Mechanical Engg.) 2nd Sem Examination 2019 (3rd Year, 2nd Semester) Machine Design III

Time – 03 Hours Full Marks: 100

Answer any five questions All questions carry equal marks

1. A single-row deep groove ball bearing is subjected to a 30 second work cycle that consists of the following two parts:

	Part I	Part II
Duration (s)	15	15
Radial load (kN)	50	20
Axial load (kM)	20	12
Speed (rpm)	720	1440

The static and dynamic load capacities of the ball bearing are 50 and 68kN respectively. Calculate the expected life the bearing in hours.

- 2. a) A ball bearing subjected to a radial load of 2000 N is expected to have satisfactory life of 15000 h at 750 rpm with a reliability of 98%. Calculate the dynamic load carrying capacity of the bearing, so that it can be selected from a manufacture's catalogue based on 90% reliability. If there are four such bearing, each with a reliability of 98% in system, what is reliability of the complete system?
 - b) A single-row deep groove ball bearing is subjected to a radial force of 9 kN and a thrust force of 4 kN. The shaft rotates at 1200 rpm. The expected life L_{10h} of the bearing is 20,000 h. The minimum acceptable diameter of the shaft is 75 mm. Select a suitable ball bearing for this application.
- 3. It is required to design a chain drive to connect a 10 kW, 900 rpm petrol engine to a conveyor. The driving sprocket is mounted on engine shaft, the driven sprocket is mounted on conveyor shaft. The conveyor shaft should run between 230 to 250 rpm. The service conditions involve moderate shocks.
 - i. Select a proper roller chain and give a list of its dimension.
 - ii. Determine the pitch circle diameters of the driving and driven sprockets.
 - iii. Determine the number of chain links
 - iv. Specify the correct centre distance between the axes of sprockets.

- 4. It is required to design a spur gear speed reducer for a compressor running at 250 rpm driven by a 7.5kW, 1000 rpm electric motor. The centre distance 250 mm. The starting torque of the motor can be assumed to be 170% of the rated torque. The gears are made of carbon steel 50C4 (Sut = 700 N/mm²). The pressure angle is 20°. The factor of safety is 1.8 for preliminary design based on the use of velocity factor:
 - i. Design the gears and specify their dimensions.
 - ii. Assume that the gears are manufactured to meet the requirements of Grade 6 calculate the dynamic load by using Buckingham's equation.
 - iii. Calculate the effective load
 - iv. What is the actual factor of safety against bending failure?
 - v. Using the same factor of safety against pitting failure, specify suitable hardness for the gears.
- 5. The following data is given for a pair of parallel helical gears made of steel:

power transmitted = 15kW, speed of pinion = 720 rpm, number of teeth on pinion = 35 number of teeth on gear = 70, centre distance = 285 mm, normal module = 5 mm, face width = 50 mm, normal pressure angle =20°, ultimate tensile strength = 610 BHN, grade of machining = Gr. 6, service factor = 1.25, Calculate

- i) The helix angle ii) the beam strength iii) the wear strength iv) the static load v) the dynamic load by Buckingham's equation vi) the effective load vii) the effective factor of safety against bending failure; and viii) the effective factor of safety against pitting failure.
- 6. A pair of straight bevel gears is mounted on shafts, which are intersecting at right angles. The number of teeth on the pinion and gear are 30 and 45 respectively. The pressure angle is 20°. The pinion shaft is connected to an electric motor developing 20 kW rated power at 500rpm. The service factor can be taken as 1.65. the pinion and the gear are made of steel (S_{ut} = 550 N/mm²) and heat-treated to a surface hardness of 300 BHN. The gear are manufactured in such a way that the error between two meshing teeth is limited to 20μm. The module and face width are 6 mm and 50 mm respectively.

Determine the factor of safety against bending as well as pitting.

7. Write a short notes on (any four)

- i. Polygonal action of roller chain
- ii. Wiebull distribution for the design of bearing
- iii. Distinguish between helical gear and herringbone gear
- iv. Sketch of Roller chain and explain
- v. Selection of bearing from manufacturer's catalogue.

Power rating of simple roller chain

Pinion			-		Power (kW)				
speed (rpm)	06 B	08A	08 B	10A	10 B	12A	12 B	16A	16 B
50	0.14	0.28	0.34	0.53	0,64	0.94	1.07	2.06	2.59
100	0.25	0.53	0.64	0.98	1.18	1.74	2.01	4.03	4.83
200	0.47	0.98	1.18	1.83	2.19	3.40	3,75	7.34	8.94
300	0.61	1.34	1.70	2.68	3.15	4.56	5.43	11.63	13.06
500	1.09	2.24	2.72	4.34	5.01	7.69	8.53	16.99	20.57
700	1.48	2.95	3,66	5.91	6.71	10.73	- 11.63	23.26	27.73
1000	2.03	3.94	5.09	8.05	8.97	14.32	15.65	28.63	34.89
1400	2.73	5.28	6.81	11.18	11.67	14.32	∃18.15 🕸	18.49	38.47
1800	3.44	6.98	8.10	8.05	13.03	10.44	19.85		
2000	3.80	6.26	8:67	7.16	13.49	8.50	20:57		3 m

		Service fac	ervice factor (K _s)			
Typ	e of driven load	Type of input power				
-21		IC engine with hy- draulic drive	Electric motor	IC engine with me- chanical drive		
(i)	Smooth: agitator,	1.0	1.0	1.2		
	fan, light					
	conveyor		1.2	1.4		
(ii)	Moderate shock.	1.2	1.3	1.4		
	machine tools,	and.				
	crane, heavy	A STATE OF THE STA				
	conveyor, food					
	mixer, grinder			46.4		
(iii)	Heavy shock:	3.1.4	1.4	14		
	punch press,	The Section		12.76		
	hammer mill,					
	reciprocating			(\$5.50) 100		
	conveyor, rolling					
	mill drive	i eer Haark				

Multiple	strand	factor	(K_1)
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!	Number of strands	K_L
-	1	1.0
	2 /	1.7
j	3	2.5
	· 4	3.3
	5	3.9
	. 6	4.6

Tooth correction factor (K2)

Number of teeth on the driving sprocket	<i>K</i> ₂
15	0.85
16	0.92
17	1.00
18	1.05
19	1.11
20	1.18
21	1.26
22	1.29
23	1.35
24	1.41
25	1.46
30	1.73

	Principa nsions (Basic load ratings (N)		Designation	
d	D	В	C	C_0		
70	90	10	12100	9150	61814	
	110	13	-28100	19000	16014	
	110	20	37700	24500	6014	
	125	24	61800	37500	6214	
	150	35	104000	63000	6314	
	180	42	143000	104000	6414	
75	95	10	12500	9800	61815	
	115	13	28600	20000	10615	
	115	20	39700	26000	6015	
	130	25	66300	40500	6215	
	160	37	, 112000×	72000	6315	
	190	45	153000	114000	6415	

Tolerances on the adjacent pitch

Grade	è (microns)
1	$0.80 \pm 0.06 \phi$
.2	$1.25 \pm 0.10 \phi$
3	$2.00 \pm 0.16 \phi$
4	$3.20 \pm 0.25 \ \phi$
5	$2.00\pm 5.00\pm 0.40~\phi$
. 6	$8.00 \pm 0.63 \ \phi$
7	$11.00 \pm 0.90 \phi$
8	$16.00 \pm 1.25 \phi$
9	$22.00 \pm 1.80 \ \phi$
10	$32.00 + 2.50 \phi$
11	$45.00 + 3.55 \phi$
. 12	$63.00 + 5.00 \phi$

$\left \left(\frac{F_a}{C_0} \right) \right $	$\left(\frac{F_a}{F_a}\right)$	≤ e s	$\left(\frac{F_a}{F_r}\right)$	> e	2
	X^{n}	Y .	X	Y	Project of
0.025	1	0	0.56	2.0	0.22
0.040	1	0	0.56	1.8	0.24
0.070	1	0	0.56	1.6	0.27
0.130	14.	0	0.56	1.4	0.31
0.250	1.00	0	0.56	1.2	0,37
0.500	Light	0	0.56	1.0	0.44