

**M.E. WATER RESOURCES AND HYDRAULIC ENGG.(6- Semester Course )**  
**2<sup>nd</sup> YEAR SECOND SEMESTER - 2025**

**Groundwater Dynamics**  
**(Paper - II)**

Time: Three hours

Full Marks: 100

**Answer any five Question**

- 1.(a) In a phreatic aquifer extending over  $1 \text{ km}^2$  the water table was initially at 25 m bgl. Sometime after irrigation with depth of 20 cm of water, the water table rose to a depth of 24 m bgl. Later  $3 \times 10^5 \text{ m}^3$  of water was pumped out and the water table dropped to 26.2 m bgl. Determine (i) specific yield of the aquifer (ii) deficit in soil moisture (below field capacity) before irrigation.
- (b) Write down the limitations of Darcy's Law.
- (c) How the intrinsic permeability is related to structure coefficient, porosity function and effective grain size? Derive it with dimensional analysis.
- 8+2+10=20
2. (a) Deduce the 2D governing in polar coordinates equation for unsteady, incompressible, anisotropic, homogenous unconfined aquifer with recharge.
- (b) An artesian aquifer 25 m thick has a porosity of 20% and the bulk modulus of compression  $2.1 \text{ GN/m}^2$ . Estimate the storage coefficient of the aquifer. Assume modulus of elasticity of the soil skeleton  $= 3 \times 10^8 \text{ N/m}^2$ .
- 16+4=20
3. (a) Deduce the governing 1-D equation in polar coordinates for steady radial flow into a well for a confined, isotropic and homogenous aquifer.
- (b) During a falling head permeability test on a soil sample of 10 cm diameter and 20 cm length, the head in the stand pipe of 2 cm diameter dropped from 50 cm to 25 cm in 2 min. Determine the permeability of the sample in SI unit.
- 15+5=20

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4. (a) Show that equation which describes the transient drawdown in the piezometric head caused by a fully penetrating pumping well in a confined aquifer in unsteady-state solutions

$$s'(u) = \frac{Q}{4\pi T} W(u)$$

Where  $\int_u^\infty \frac{e^{-x}}{x} dx = W(u)$  = Well function and  $S'(u)$  = drawdown,  
T = Transmissivity, Q = discharge of well

- (b) A well is located in a 25 m confined aquifer of permeability 30 m/d and storage coefficient 0.005. If the well is being pumped at the rate of 1750 lpm, calculate the drawdown (in m) at a distance of 10 m from the well after 20 h of pumping.

14+6=20

5. (a) Why Copper-Jacob straight line method is advantageous over the Thies method? State its limitations.
- (b) The transmissivity and storativity of a confined aquifer are 1000 m<sup>2</sup>/day and 0.0001, respectively. An observation well located 500 m away from the pumping well. For a pumping period of 220 min, calculate
- the drawdown at the observation well if the discharge rate is 1000 m<sup>3</sup>/day:
  - the pumping rate required to provide a drawdown of 2 m at that well after 220 minutes.
- (c) Prove that drawdown (s) can be expressed by "Copper-Jacob Method" is

$$s = \frac{2.3Q}{4\pi T} \log \frac{2.25Tt}{r^2 S}$$

where Q is the discharge of pumping well, T and S are the Transmissivity and Storativity with time 't' and r is the radial distance between main well to observation well.

6+8+6=20

6. (a) In a test of a confined aquifer, the pumping rate was 500 m<sup>3</sup>/day. Drawdown and time data were collected at an observation well 300 m away (table given below).

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Determine the transmissivity and storativity of the aquifer using the Copper-Jacob Straight Line Method.

Table: Drawdown measured at an observation well 300 m away

| Time(min) | S(m) | Time(min) | S(m) |
|-----------|------|-----------|------|
| 1.00      | 0.03 | 35.62     | 1.79 |
| 1.27      | 0.05 | 45.20     | 1.97 |
| 1.61      | 0.09 | 57.36     | 2.15 |
| 2.04      | 0.15 | 72.79     | 2.33 |
| 2.59      | 0.22 | 92.37     | 2.52 |
| 3.29      | 0.31 | 117.21    | 2.70 |
| 4.18      | 0.41 | 148.74    | 2.89 |
| 5.30      | 0.53 | 188.74    | 3.07 |
| 6.72      | 0.66 | 239.50    | 3.26 |
| 8.53      | 0.80 | 303.92    | 3.45 |
| 10.83     | 0.95 | 385.66    | 3.64 |
| 13.74     | 1.11 | 489.39    | 3.83 |
| 17.43     | 1.27 | 621.02    | 4.02 |
| 22.12     | 1.44 | 788.05    | 4.21 |
| 28.07     | 1.61 | 1000.00   | 4.39 |

Table 5.1 Values of  $W(u)$  for values of  $u$  (abridged, after Wenzel, 1942)

| $u$               | 1.0   | 2.0   | 3.0   | 4.0    | 5.0    | 6.0     | 7.0     | 8.0      | 9.0      |
|-------------------|-------|-------|-------|--------|--------|---------|---------|----------|----------|
| $\times 1$        | 0.219 | 0.049 | 0.013 | 0.0038 | 0.0011 | 0.00036 | 0.00012 | 0.000038 | 0.000012 |
| $\times 10^{-1}$  | 1.82  | 1.22  | 0.91  | 0.70   | 0.56   | 0.45    | 0.37    | 0.31     | 0.26     |
| $\times 10^{-2}$  | 4.04  | 3.35  | 2.96  | 2.68   | 2.47   | 2.30    | 2.15    | 2.03     | 1.92     |
| $\times 10^{-3}$  | 6.33  | 5.64  | 5.22  | 4.95   | 4.73   | 4.54    | 4.39    | 4.26     | 4.14     |
| $\times 10^{-4}$  | 8.63  | 7.94  | 7.53  | 7.25   | 7.02   | 6.84    | 6.69    | 6.55     | 6.44     |
| $\times 10^{-5}$  | 10.94 | 10.24 | 9.84  | 9.55   | 9.33   | 9.14    | 8.99    | 8.86     | 8.74     |
| $\times 10^{-6}$  | 13.24 | 12.55 | 12.14 | 11.85  | 11.63  | 11.45   | 11.29   | 11.16    | 11.04    |
| $\times 10^{-7}$  | 15.54 | 14.85 | 14.44 | 14.15  | 13.93  | 13.75   | 13.60   | 13.46    | 13.34    |
| $\times 10^{-8}$  | 17.84 | 17.15 | 16.74 | 16.46  | 16.23  | 16.05   | 15.90   | 15.76    | 15.65    |
| $\times 10^{-9}$  | 20.15 | 19.45 | 19.05 | 18.76  | 18.54  | 18.35   | 18.20   | 18.07    | 17.95    |
| $\times 10^{-10}$ | 22.45 | 21.76 | 21.35 | 21.06  | 20.84  | 20.66   | 20.50   | 20.37    | 20.25    |
| $\times 10^{-11}$ | 24.75 | 24.06 | 23.65 | 23.36  | 23.14  | 22.96   | 22.81   | 22.67    | 22.55    |
| $\times 10^{-12}$ | 27.05 | 26.36 | 25.96 | 25.67  | 25.44  | 25.26   | 25.11   | 24.97    | 24.86    |
| $\times 10^{-13}$ | 29.36 | 28.66 | 28.26 | 27.97  | 27.75  | 27.56   | 27.41   | 27.28    | 27.16    |
| $\times 10^{-14}$ | 31.66 | 30.97 | 30.56 | 30.27  | 30.05  | 29.87   | 29.71   | 29.58    | 29.46    |
| $\times 10^{-15}$ | 33.96 | 33.27 | 32.86 | 32.58  | 32.35  | 32.17   | 32.02   | 31.89    | 31.77    |

(b) "It is good practice to measure residual drawdowns"- Justify the statement

2+18=20

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7. (a) Briefly describe the approach and objective of groundwater modelling

(b) Briefly describe the common mistakes in groundwater modelling

(c) An R C network analog has to be constructed to simulate a confined aquifer 6 km X 4 km extent having a uniform saturated thickness of 50 m, permeability of 3 m/day, and storage coefficient 10-3. The aquifer may be divided into grid of 1km\*1 km. 1 sec. in the analog should represent 1000 days for the aquifer. Restore of 1 megaohm are available and 1 m head of water should represent 1 volt in analog. Work out the scale factor for resistance and discharge. What capacitance should be required for each block.

$$6+4+10=20$$

8. (a) Briefly describe the term "response of an unconfined aquifer to pumping."

(b) A test was conducted with an unconfined aquifer near Burdwan, Damodar River. The well was pumped at constant rate of 2040 m<sup>3</sup>/day. The drawdown measured in an observation well 10 m away are listed in below table. Aquifer thickness is 14 m. Assuming fully penetrating well calculate the hydraulic parameters for the aquifer using Neuman's straight-line method.

| Time Since Pumping (Minutes) | Drawdown (m) | Time Since Pumping (Minutes) | Drawdown (m) | Time Since Pumping (Minutes) | Drawdown (m) | Time Since Pumping (Minutes) | Drawdown (m) |
|------------------------------|--------------|------------------------------|--------------|------------------------------|--------------|------------------------------|--------------|
| 1                            | 0.07         | 40                           | 0.178        | 85                           | 0.207        | 720                          | 0.259        |
| 2                            | 0.08         | 41                           | 0.18         | 90                           | 0.21         | 840                          | 0.26         |
| 3                            | 0.09         | 42                           | 0.18         | 95                           | 0.21         | 960                          | 0.267        |
| 4                            | 0.095        | 44                           | 0.18         | 100                          | 0.21         | 1080                         | 0.269        |
| 5                            | 0.1          | 46                           | 0.185        | 105                          | 0.212        | 1200                         | 0.27         |
| 6                            | 0.11         | 48                           | 0.188        | 110                          | 0.212        | 1320                         | 0.27         |
| 7                            | 0.13         | 50                           | 0.19         | 115                          | 0.218        | 1440                         | 0.278        |
| 8                            | 0.13         | 52                           | 0.19         | 120                          | 0.218        | 1560                         | 0.28         |
| 9                            | 0.13         | 54                           | 0.193        | 130                          | 0.22         | 1680                         | 0.28         |
| 10                           | 0.13         | 56                           | 0.193        | 140                          | 0.22         | 1800                         | 0.285        |
| 12                           | 0.135        | 58                           | 0.193        | 150                          | 0.225        | 1920                         | 0.287        |
| 13                           | 0.14         | 60                           | 0.193        | 210                          | 0.238        | 2040                         | 0.29         |
| 14                           | 0.141        | 62                           | 0.199        | 240                          | 0.24         | 2160                         | 0.293        |
| 15                           | 0.145        | 64                           | 0.2          | 270                          | 0.24         | 2280                         | 0.293        |
| 16                           | 0.145        | 66                           | 0.2          | 300                          | 0.241        | 2400                         | 0.295        |
| 17                           | 0.147        | 68                           | 0.204        | 330                          | 0.243        | 2520                         | 0.299        |
| 18                           | 0.147        | 70                           | 0.205        | 360                          | 0.243        | 2640                         | 0.299        |
| 19                           | 0.149        | 75                           | 0.207        | 420                          | 0.25         | 2760                         | 0.3          |
| 20                           | 0.149        | 80                           | 0.207        | 600                          | 0.259        | 2880                         | 0.3          |

$$3+17=20$$